

PERFORMANCE QUALITY SERVICE TRUST

NEW PRODUCTS FROM NPC



L10

The Model L10 pump line is newly designed to meet the stringent requirements of the API (oil and gas) and snow making markets. This pump consists of low flow and high head per stage that incorporates a low NPSH first stage impeller, required for both API and snow making. Design conditions – 300-400 GPM @ 50'TDH (1800 RPM) and 600-800 GPM @ 200'TDH (3600 RPM).

H16

Our new Model H16 pump line completes our product line, between our 14" & 18" pump models. This is a high efficiency pump, with a capacity range of 3,500 to 5,500 GPM @ 100'TDH, and is designed for the municipal, industrial, and agricultural markets.





STAINLESS STEEL CAST IMPELLERS AND BEARING RETAINERS

We have added Stainless Steel (304 and 316SS) cast impellers and bearing retainers to our product line. Available off the shelf for immediate shipment, many of our customers have a need for this product and we want to ensure we have the product in stock, should their need arise.

STAYING AHEAD OF THE CURVE



MAIN OFFICE



<u>ARIZONA</u>

7706 N. 71st Avenue Glendale, AZ 85303-1703 (623) 979-3560 • Fax (623) 979-2177 (800) 966-5240



FACTORY BRANCH LOCATIONS

CALIFORNIA

2830 San Antonio Drive Fowler, CA 93625 (559) 834-5437 • Fax (559) 834-5727 (800) 868-9755

FLORIDA

195 E. 3rd Street Zolfo Springs, FL 33890 (863) 735-8222 • Fax (863) 735-8202 (800) 994-3045

<u>MISSISSIPPI</u>

11176 Green Valley Drive Olive Branch, MS 38654 (662) 895-1110 • Fax (662) 895-5083 (866) 668-4914

<u>TEXAS</u>

LUBBOCK

4229 Adrian Street Lubbock, TX 79415 (806) 745-5396 • Fax (806) 745-6668 (800) 745-5393

HOUSTON

109 North Richey Pasadena, TX 77506 (713) 641-6818 • Fax (713) 641-4569 (800) 231-0590

Email: info@natlpump.com

www.nationalpumpcompany.com



National Keeps You Pumping Around The World

At National Pump, pump technology is our business. From principals and engineers to sales and service personnel, our key staff members have more than three centuries of combined industry experience. We want to help you achieve your goals and objectives, and we're big enough to meet your needs, yet small enough to provide the one-to-one service you deserve.

At every stage of our work, from research and development to design, production and testing, we use up-to-the-minute technologies and the most modern equipment available to ensure that every National Pump meets the highest possible standards of efficiency and reliability. Using conventional or special materials, we manufacture pumps for specific needs and conditions.

From gold mines to golf courses to grain fields, our pumps are hard at work around the world. Serving commercial, industrial, municipal, power, residential, mining, oil and gas and agricultural irrigation needs, each National Pump produced is an individual pumping system designed to do a specific pumping job. Precisely matched drivers, discharge heads, impellers, bowls and column /shaft assemblies deliver consistent pumping capacity.

We offer a full range of vertical turbine and submersible pumps, water or oil lubricated, of threaded or flanged construction, with capacities to 20,000 GPM and pressures up to 2,000 PSI. All pump models are in stock as standard materials, and they can be customized at the service center level. We also manufacture custom pumps, using special alloys and coatings to suit your specific needs. We have multiple patterns in order to meet special alloy requirements in a timely manner.

Even more important is the service we provide. We will be happy to provide pre-design information to help you develop the most efficient pumping system for your customer's needs. Whatever your application, we know that having equipment down causes unacceptable delays so each of our offices is a complete service / warehouse / assembly / finishing center.

Our branches are strategically located throughout the United States and staffed by experienced managers who are all technical experts, ready to help solve your problems on the phone or on site. No matter what brand of pump you have, when you need service, you get it now - not a two month delay while parts are ordered, or a several-day wait for a visit from service personnel.

Before you design your next pumping system, talk with a National Pump expert and take advantage of the knowledge and experience we have to offer. We're convinced you won't find better quality or service anywhere!

Creating Quality Pump Systems and Satisfied Customers Visit us on the web at: www.nationalpumpcompany.com



REVISED OCTOBER 2022



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NATIONAL PUMP COMPANY

Subject to the terms and conditions set forth below, NATIONAL PUMP COMPANY ("National") warrants that its manufactured equipment is free from defects in workmanship and materials USING ITS SPECIFICATIONS AS A STANDARD. This warranty does not extend to anyone except the first purchaser to whom the goods are shipped from National.

National's obligation under this warranty is expressly limited to replacing or repairing, free of charge, F.O.B. point of manufacture, any defective part or parts of its manufactured equipment; however, NATIONAL SHALL HAVE NO SUCH LIABILITY EXCEPT WHERE IT IS SHOWN TO THE SATISFACTION OF NATIONAL THAT THE DAMAGE OR CLAIM RESULTED FROM BREACH OF THIS WARRANTY. All parts claimed defective must be delivered to National at its factory or any factory branch, freight or express thereon PREPAID.

Every claim under this warranty SHALL BE DEEMED WAIVED UNLESS MADE IN WRITING AND RECEIVED BY NATIONAL WITHIN THIRTY (30) DAYS OF THE DATE THE DEFECT WAS DISCOVERED OR SHALL HAVE BEEN DISCOVERED, and within one year of the date of installation. The installation date must be within six months of the date the pump was purchased from National.

This Warranty does not cover those parts of the manufactured equipment which are not manufactured by National except to extend to the purchaser the same warranty, if any which is given to National by the manufacturers of said parts.

National makes no other representation of warranty of any kind, express or implied, in fact or in law, including without limitation, the warranty of merchantability or the warranty of fitness for a particular purchase, other than the limited warranty set forth herein. In no event shall National be liable for any consequential or incidental damages resulting directly or indirectly from the use or loss of use of the manufactured equipment. National shall not be liable for any alleged negligence, breach of warranty, strict liability, or any other theory other than the limited liability set forth herein.

THIS WARRANTY CONTAINS THE ENTIRE WARRANTY RELATING TO THE MANUFACTURED GOODS OF NATIONAL, AND NO CONDUCT, ORAL STATEMENTS OR REPRESENTATIONS NOT CONTAINED IN THIS WARRANTY SHALL HAVE ANY FORCE OR EFFECT OR BE DEEMED A WAIVER THEREOF, THIS WARRANTY SHALL NOT BE MODIFIED IN ANY WAY EXCEPT IF IN WRITING AND SIGNED BY AN AUTHORIZED REPRESENTATIVE OF NATIONAL.

This Warranty, and any liability of National hereunder, shall be governed by, construed, and enforced in accordance with the laws of the State of Ohio.

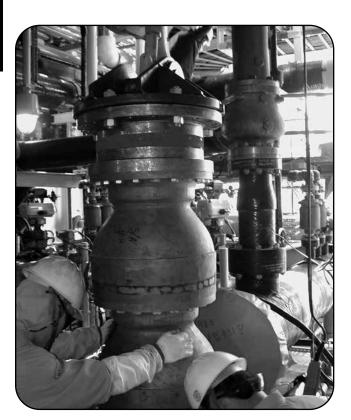


STANDARD TERMS AND CONDITIONS OF SALE

- 1. **ACCEPTANCE OF ORDERS:** All orders are subject to acceptance by an Officer of the Company and orders and deliveries are subject to the Company's regular credit policy. The Company reserves the right to refuse any order based on a quotation containing a gross error.
- 2. **PRICES:** List prices and discount schedules are to be maintained at all times. Prices are for merchandise F.O.B. shipping points, freight collect or prepaid, and added to the invoice. Prices, discounts, quotations, and specifications are subject to change without notice and will be applied as in effect at time of shipment.
- 3. **TERMS:** All quotations are subject to National Pump Co., standard terms and conditions. Payment terms require credit department approval at our main office, Glendale, AZ. Interest at the maximum legal rate will be charged on all overdue amounts.
- 4. **TAXES:** Taxes imposed by any Federal, State, County, or Municipal law on the sale will be added to the invoice, unless a fully executed tax exemption certificate is received with the order.
- 5. **ORDER CHANGES:** No changes in orders will be accepted from the Purchaser except by special written arrangement with the executive office of National.
- 6. **RETURN OF GOODS:** Written permission from the factory must be obtained before returning any merchandise. All transportation charges must be borne by the Customer. New material of current design accepted by the Company for credit is subject to a restocking charge of at least 15 percent.
- 7. **CLAIMS:** All goods shall be deemed delivered to purchaser at the time they are placed in the hands of carrier and consigned to purchaser.
- 8. **ROUTING:** If routing of shipment is specified on Customer's order, it will be followed whenever practical.
- 9. **SUBSTITUTION:** The Company reserves the right to substitute materials and modify specification to the extent required in order to comply with any Government law or regulation.
- 10. **MINIMUM ORDER AMOUNT:** The minimum order amount to be charged on customer account is \$50.00. All orders for less than this amount will be billed at the minimum of \$50.00 not including tax or freight charges.



API / OIL AND GAS INSTALLATIONS





Materials of Construction:	All nickel aluminum bronze construction / Kmonel shaft and hardware.
Pump Model:	K20MC - 3 stage – submersible pump M10LC - 2 stage – submersible pump
Design Conditions:	2 @ 5600 GPM @ 345 Feet TDH with 84% Eff. 650 HP 1 @ 900 GPM @ 345 Feet TDH with 80% Eff. 125 HP
Liquid Pumped:	Sea Water
Comments:	These submersible pumps were for process water on an oil platform in the South China Sea, off the coast of South Korea for KNOC (Korea National Oil Company). Quantity of $2 - 650$ HP Submersibles and $1 - 125$ HP Submersible. All pumps were complete with NI AI. bronze flanged column pipe and surface plate.



API / OIL AND GAS INSTALLATIONS

AZORES AFB, PORTUGAL

Pumping JP-8 Fuel Transfer Pumps 48 GPM 146' GPM M6LC – 10 Stage

BAGRAM AFB, AFGANISTAN

Pumping JP-8 & Diesel Fueling Pumps 50 GPM @ 5 HP 300 GPM @ 30 HP 600 GPM @ 50 HP 900 GPM @ 150 HP M6MC, M8HC, J11MC, M12HC

CAMP EDWARDS, KOREA

Pumping JP-8 Fueling Pumps 300 GPM @ 230' TDH M9HC – 8 Stage

CAMP CASEY, KOREA

Pumping JP-8 Fueling Pumps 200 GPM @ 92' TDH M8MC – 4 Stage

CAMP PAGE, KOREA

Pumping JP-8 Fueling Pumps 301 GPM @ 407' TDH M10LC - 8 Stage

<u>CANNON AFB – CURRY, COLORADO</u>

Pumping JP-8 Fueling Pumps 50 GPM @ 129' TDH M6LC - 9 Stage

CB&I, YEMEN LNG, MARIB, YEMEN

Pumping LPG Transfer Pumps 448 GPM @ 1974' TDH M8MC – 25 Stage

<u>CHEVRON / TEXACO</u>

Pumping Sea Water Submersible Pumps 500 GPM @ 375' TDH M8MC – 4 Stage

GRANDFORKS AFB

Pumping JP-8 Fuel Transfer Pumps 300 GPM @ 250' TDH M8MC - 9 Stage

HUSKY OIL COMP., CANADA

Pumping Crude Oil Fuel Transfer Pumps 150 M3/H @183 M M12LC – 9 Stage

KUSAN, KOREA

Pumping JP-8 Fueling Pumps 400 GPM @ 108' TDH M8MC– 1 Stage 600 GPM @ 210' TDH M8MC – 2 Stage

KWANGJU, KOREA

Pumping JP-8 Fuel Transfer Pumps 300 GPM @ 206' TDH M8XLC – 2 Stage 300 GPM @ 75' TDH M8HC – 3 Stage 300 GPM @ 50' M8HC – 2 Stage 300 GPM - 224' TDH M8XLC – 2 Stage

MCAS - BEAUFORT, S.C.

Pumping JP-8 Fuel Transfer Pumps 300 GPM @ 160' TDH E6XHC – 4 Stage 600 GPM @ 425' TDH M8MC – 4 Stage

<u>MCAS MIRAMAR – MIRAMAR, CA</u>

Pumping JP-8 Fuel Transfer Pumps 50 GPM @ 172' TDH M6MC – 12 Stage

S&BENGINEERS/

PL PROPYLENE LLC

Pumping Hydrocarbon Condensate Condensate Pumps 429 GPM @ 194' TDH M8XHC – 7 Stage

SOTO CANO, HONDURAS

Pumping Jet Fuel Fuel Transfer Pumps 300 GPM @ 204' TDH M8HC – 6 Stages 50 GPM @ 60' TDH M6MC – 4 Stages

PLAINS PIPELINE

Pumping Crude Oil Crude Oil Transfer Pumps 12,613 GPM @ 315' TDH 1250 HP H24XHC – 4 Stages

TEMA OIL REFINERY

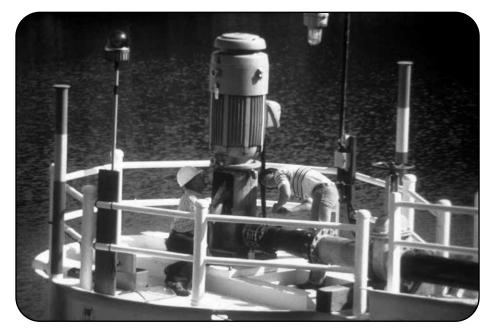
Pumping LPG Loading Pump 120 M3/HR @ 92.9 Meters J11MC – 7 Stage

WRIGHT PATTERSON AFB

Pumping JP-8 Flight Line Transfer Pumps Transferring jet fuel 600 GPM @ 419' TDH M10HC –8 Stage



MINING



Materials of Construction:	Complete 316 S.S. can booster and two 316 S.S. barge mounted pumps using carbon graphite bearings, and 316 S.S. mechanical seals.
Pump Model:	Barge Pump – 4 stage M14MC bowl assembly Barge Pump – 6 stage M14MC bowl assembly Can Booster – 7 stage M14MC bowl assembly
Design Conditions:	1000 G.P.M. @ 370' T.D.H. – 150 H.P. VSS Mill and Chem. TEFC motor. 1000 G.P.M. @ 580'T.D.H. – 250 H.P. VSS Mill and Chem. TEFC motor. 1000 G.P.M. @ 640'T.D.H. – 250 H.P. VSS Mill and Chem. TEFC motor.
Liquid Pumped:	Less than 10% H2 SO4 (sulfuric acid) and water solution. Specific Gravity – 1.02
Comments:	Reclaimed water utilized by the mine for the extraction of minerals (in particular copper) from the solution at the leaching process of the copper plants. The initial pump was floated on a fiberglass barge on a lake at the mine site to begin this process. This offshore pump was attached to the initial booster pump on shore via a flexible polypropylene pipe, boosting this mine solution to the 2nd booster pump, up the mountain and to the mine site for processing.



GENERAL INFORMATION

MINING INSTALLATIONS

GETTY OIL MINING COMPANY

SAN MATEO, CALIFORNIA

Mercur Gold Project Pumping process water In-Line Booster Pumps 620 GPM @ 920' TDH 300 GPM @ 1,010' TDH 300 GPM @ 1,550' TDH

BECHTEL POWER CORPORATION

SAN FRANCISCO, CALIFORNIA For Amselco Minerals, Inc.

Pumping sodium hydroxide Process Pumps 1396 GPM @ 375' TDH 1008 GPM @ 80' TDH 180 GPM @ 250' M14MC – 4 Stage M11MC – 2 Stage M8XLC – 10 Stage

NORANDA LAKESHORE MINES

ARIZONA

Pumping acid mine water All 316 S.S. bowl assembly 1000 GPM @380' TDH M12MC – 5 Stage

CYPRUS-BAGDAD COPPER COMPANY

BAGDAD, ARIZONA

Pumping acid mine water Canned Booster Pumps 1500 GPM @ 350' TDH 4 Units

KENNECOTT CHINO MINES

HURLEY, NEW MEXICO

Pumping mine water 500 to 1000 GPM @ 500' to 800' TDH 6 Units

INSPIRATION CONSOLIDATED COPPER COMPANY, INC.

CLAYPOOL, ARIZONA

Pumping acid mine water All 316 S.S. barge mounted and canned booster pumps 1000 GPM @ 580' TDH 1000 GPM @ 370' TDH 1000 GPM @ 640' TDH

MAGMA NEVADA MINING COMPANY

RUTH, NEVADA Iron constructed pumps for water 2550 GPM @ 230' TDH H14MC – 3 Stage 2500 GPM @ 160' TDH H14MC – 2 Stage

PEA RIDGE IRON ORE COMPANY

SULLIVAN, MISSOURI Pumping river water Booster Pumps 1200 GPM @ 690' TDH SE12MC – 11 Stage

NEVADA GOLD MINING

WINNEMUCCA, NEVADA Pumping mine water Iron constructed pumps 3100 GPM @ 300' TDH H12XHC – 4 Stage

CHAMCO INDUSTRIES

VANCOUVER, B.C., CANADA Pumping mine process water

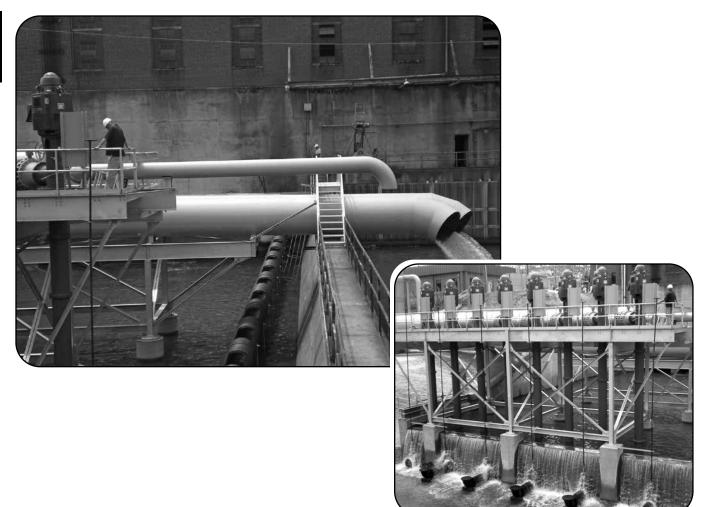
316 S.S. booster pumps

CODELCO MINES

CHILE, S.A. Pumping mine production water Well Pumps H14XHC – 3 Stage J8XHC – 4 Stage



POWER



Materials of Construction:Standard Cast Iron / Bronze18" Fab Discharge Head / Flanged Column

Pump Model:2 Stage H24MC Bowl AssemblyQuantity – 8

Design Conditions: 12

12500 G.P.M @ 80' T.D.H. 300 HP @ 1200 R.P.M.

Liquid Pumped: River Water

Comments: The eight pumps are used to pump water from the river, up through the cooling towers. This process keeps the core, where the electricity is made, cool. The water is then released back into the river at the same temperature it was originally, when it was pumped out of the river.



POWER INSTALLATIONS

DETROIT EDISON POWER PLANT

ST. CLAIR POWER PLANT

General service pumps 6,000 GPM @ 200' TDH J24HC – 2 Stage

PACIFIC GAS AND ELECTRIC

ANAHEIM, CALIFORNIA

All 316 S.S. With a TPL of 19' 2400 GPM @ 250' TDH H14MC – 4 Stage

SALT RIVER POWER PROJECT

PHOENIX, AZ

Water Supply Pumps Various well pumps ranging from 500 GPM to 4,000 GPM

SAVANNAH RIVER PROJECT

SAVANNAH, GEORGIA

Pumping produce water M12MC zinc less bronze construction with wear rings – 6 Stage "O" Rings 316 S.S. Shaft and Hardware 1000 GPM @ 385' TDH

TUCSON ELECTRIC POWER

SPRINGERVILLE, ARIZONA Generating Station Pumping well water from storage reservoir to power plant 2000 GPM @ 900' TDH 1500 GPM @ 1250' TDH H14MC – 13 Stage 3500 GPM @ 600' TDH H14XHC – 8 Stage



MUNICIPAL



Materials of Construction:	Standard Cast Iron / Zincless Bronze Impellers 18" Fab Discharge Head / Flanged Column
Pump Model:	8,680 G.P.M @ 232' TDH
Design Conditions:	2 @ 5600 GPM @ 345 Feet TDH with 84% Eff. 650 HP 1 @ 900 GPM @ 345 Feet TDH with 80% Eff. 125 HP
Liquid Pumped:	Finished Water
Comments:	More pumping capacity was needed at a finished water pumping station. The pumps were required to supply water to system storage tanks as well as keep up with the demand of the distribution system. The requirements were well met with three 600 hp vertical turbine pumps, pumping 8,680 gpm @ 232 ft.



MUNICIPAL INSTALLATIONS

AUBURN WATER DISTRICT

TRUCKEE, CALIFORNIA

1000 GPM @ 540' TDH E12MC – 9 Stage 500 GPM @ 730' TDH M10HC – 12 Stage

CITIZENS UTILITIES

SUN CITY, ARIZONA

Deep well submersible pumps for produce water 1000 GPM @ 639' TDH SM12HC – 9 Stage 1200 GPM @ 573' TDH SM12HC – 9 Stage

CITY OF CAPE CORAL

FLORIDA

316 S.S. / 304 S.S. submersible pumps for reverse osmosis plant 175 GPM @ 150' TDH 750 GPM @ 230' TDH

CITY OF CHANDLER

ARIZONA

Deep well turbine pump for water production 4000 GPM @ 300' TDH E18LC – 3 Stage

<u>CITY OF CONWAY</u>

SOUTH CAROLINA

For Pumping Potable Water 5,600 GPM @ 40' TDH H24MC – 1 Stage

<u>CITY OF INDIO</u>

CALIFORNIA

Well Pump Design Conditions: 300 GPM @ 240' TDH H14MC – 4 Stage Jockey Pump Design Conditions: 800 GPM @ 158' TDH E12XMC – 3 Stage Can Booster Pump Design Conditions: 2000 GPM @ 138' H12HC – 4 Stage

<u>CITY OF SCOTTSDALE</u>

ARIZONA

Water Treatment Plant Deep Well Pump Design Conditions: 2500 GPM @ 640' TDH H14MC - 9 Stage Coated Water Passages & 316 S.S. Can / Barrel Pump Design Conditions: 1800 GPM @ 50' TDH H12HC - 3 Stage Coated Water Passages & 316 S.S. Water Supply from the Central Arizona Project Canal to the City of Scottsdale's three (3) booster stations Ten (10) Raw Water Pumps 1500 GPM @ 388' TDH M14MC - 4 Stage

DEL WEBB

SUN CITY, ARIZONA

Deep well submersible for produce water 1200 GPM @ 550' TDH SE12MC – 10 Stage 1200 GPM @ 528' TDH SE12MC – 8 Stage

DEPT. OF WATER RESOURCES

HAWAII

Deep Well Turbine Pump 500 GPM @ 1405' M10LC – 27 Stage All Ductile Iron Construction

DOWELL SCHLUMBERGER MUNICIPAL WATER SUPPLY UNITS AUSTRALIA

Pumping Water Service Water Supply Pumps 4000 GPM @ 345' 900 HP 3600 RPM H12HC – 4 Stage All Nickel Aluminum Bronze Tungsten Carbide Shaft Journals, Bearings and K-Monel Shaft

EL PASO WATER UTILITIES TEXAS

For Municipal Water Supply Deep Well Pumps 1400 GPM @ 480' TDH M14MC – 5 Stage

SHEA SUNBELT PLEASANT POINT CAN BOOSTER PUMPS FOR MUNICIPAL PROJECT

1750 GPM @ 115' TDH 600 GPM @ 115' TDH 1750 GPM @ 215' TDH 700 GPM @ 215 TDH Vertical Turbine Deep Well Supply Pump 550 GPM @ 500' TDH J11HC – 9 Stage

SUN CITY WATER COMPANY

SUN CITY, ARIZONA

Deep Well Submersible for produce water 1000 GPM @ 639' TDH SM12HC – 9 Stage 1200 GPM @ 573' TDH SE12MC - 9Stage



INDUSTRIAL / COMMERCIAL



Materials of Construction:	Cast Iron Bowls, bronze impellers, stainless steel fitted, steel fabricated discharge head.
Pump Model:	M10LC – 14 Stage
Design Conditions:	400 GPM @ 750' TDH
Liquid Pumped:	Water From Coal Mine
Comments:	The pump was designed to pump mine water back to the prep plant to wash the coal after it went through the prep plant.



INDUSTRIAL / COMMERCIAL INSTALLATIONS

ARGO INDUSTRIAL

BELLEVUE, WASHINGTON

For Ice Harbor Project Office, Corps of Engineers "Ice Harbor Dam" 2000 GPM @ 80' TDH M14XHC

ARIZONA BOILER WORKS

FLAGSTAFF, ARIZONA

Boiler Pump 350 GPM @ 46' TDH M8MC – 2 Stage

ARIZONA CORRECTIONAL CENTER

LITCHFIELD PARK, ARIZONA 1000 GPM @ 42' TDH

M11MC – 1 Stage

ARMY COMMAND CENTER

FORT MCPHEARSON, GEORGIA HVAC Lineshaft Turbine Pumps

BROWN & ROOT, INC.

HOUSTON, TX For salt water supply for mud pumps on off shore production platform H14MC – 2 Stage

250 HP Ragd Close-Coupled

BUREAU OF RECLAMATION

YUMA, ARIZONA

Submersible well pump, all bronze construction with 304 S.S. motor adapter 3250 GPM @ 43' TDH SH14MC – 1 Stage Plueger 50 HP A-1 Construction

BUSCH GARDENS

TAMPA, FL Congo River Rapids M14 & H14 Bowl Assembly

CULLIM & BROWN OKLAHOMA CITY, OKLAHOMA

For Gravel Pit 3000 GPM @ 150' TDH H14XHC – 2 Stage

INTAMIN, INC. MILLERSVILLE, MARYLAND

Amusement Park Rides: Busch Gardens, Tampa, FL. Opryland U.S.A., Nashville, TN, Great Adventure, Jackson, NJ . Six Flags Over Georgia, Altlanta, GA. Six Flags Over Texas, Dallas, TX Six Flags Over Mid America, St. Louis, MO Six Flags Magic Mountain, Valencia, CA. Adventure Land Park, Des Moines, IA

KENNER DRY DOCK

KENNER, LOUISIANA

For dry dock application, pumping river water out of dry dock 2300 GPM @ 26' TDH H14XHC – 1 Stage

MARSHALL SPACE FLIGHT CENTER

HUNTSVILLE, AL 6000 GPM @ 80' TDH J18MC – 1 Stage

<u>TITANIC MOVIE SET</u>

ROSARITO, BAJA, CALIFORNIA, MEXICO

For Pumping Sea Water Supply Pumps, all iron construction 3000 GPM @ 80' TDH H14XHC – 1 Stage

PEPSI COMPANY

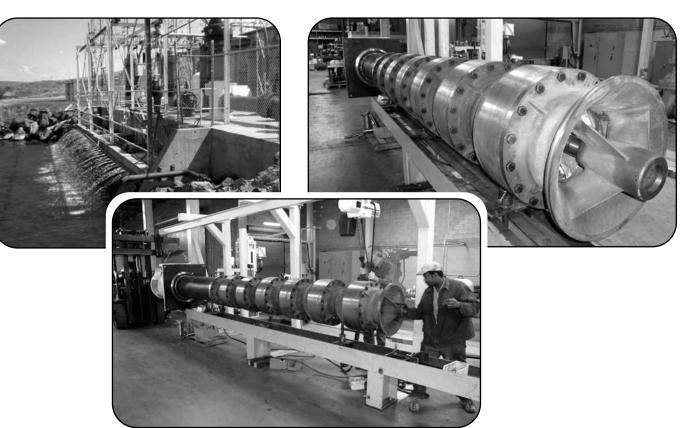
RIYADH, SAUDI ARABIA

Bottling Plant 316SS Material Construction 1050 GPM @ 1150' TDH E12HC –16 Stage



AGRICULTURAL





Materials of Construction: Fabricated steel

Pump Model:

2 x 4 STAGE H24MC 1 x 5 STAGE H24MC

Design Conditions: 2 @ 7,750 G.P.M. @ 440 Feet, T.D.H. close coupled to a fabricated steel discharge head & fitted with 1,000 HP motors. 1 @ 9,400 G.P.M. @ 530 feet, T.D.H. with short column section coupled to a fabricated steel discharge head & fitted with a 1,500 HP motor.

Liquid Pumped: Irrigation Water

Comments: These 3 vertical turbine pumps are part of a larger irrigation process comprising of over one hundred vertical turbine pumps, up to 2,000 HP, delivering water from a river in the Pacific Northwest to 60,000 acres of farmland. Water is delivered through a network of underground pipelines to the various farming areas. More than 25 miles of 60" thru 72" mainlines feed hundreds of miles of smaller distribution lines, feeding center pivot irrigation systems.



AGRICULTURAL INSTALLATIONS

U.S. BUREAU OF INDIAN AFFAIRS

COOLIDGE, ARIZONA San Carlos Irrigation Project 3500 GPM @ 395' TDH

INGENIO MAGDELENA - GUATELMALA INGENIO LA UNION - GUATEMALA INGENIO PANTELEON - NICARAGUA

Deep well irrigation pumps for sugar cane plantations 2 Stages – 8 Stages, depending on area being irrigated J11HC. K12HC M8HC, J8XHC

National Pump's 40 years of commitment and experience within the agricultural and turf irrigation markets has provided the opportunity to supply over 100,000 pumps throughout the Americas and around the world. When considering a 4" submersible or a large 24" canned line-shaft turbine pump, National Pump provides 'best-in-class' performance, reliability, availability, service and value when handling the toughest water applications.

GENERAL ARRANGEMENT (GA DRAWINGS) AVAILABLE FOR VARIOUS TYPES OF CONSTRUCTION WITH VARIOUS TYPES OF OPTIONS LISTED BELOW: CONTACT FACTORY FOR DRAWINGS.

1. WELL PUMP LINESHAFT WITH THE FOLLOWING OPTIONS:

HEAD TYPE	DRIVER
FAB STEEL	ELECTRIC MOTOR
N260	RAGD
HI PROFILE	COMBINATION TYPE
DIESEL ENGINE	

- 2. WELL PUMP SUBMERSIBLE
- 3. CLOSE COUPLED VERTICAL TURBINE PUMP LINESHAFT WITH THE FOLLOWING OPTIONS:

HEAD TYPE	COLUMN TYPE	DRIVER	TYPE OF DRIVER
FAB STEEL	THREADED	ELECTRIC MOTOR	HOLLOWSHAFT
N260	FLANGED	RAGD	SOLID SHAFT
HI PROFILE		COMBINATION TYPE	
UNDERGROUND DISCHARGE		DIESEL ENGINE	

4. CAN BOOSTER VERTICAL TURBINE PUMP LINESHAFT WITH THE FOLLOWING OPTIONS:

TYPE OF DRIVER HOLLOWSHAFT SOLID SHAFT

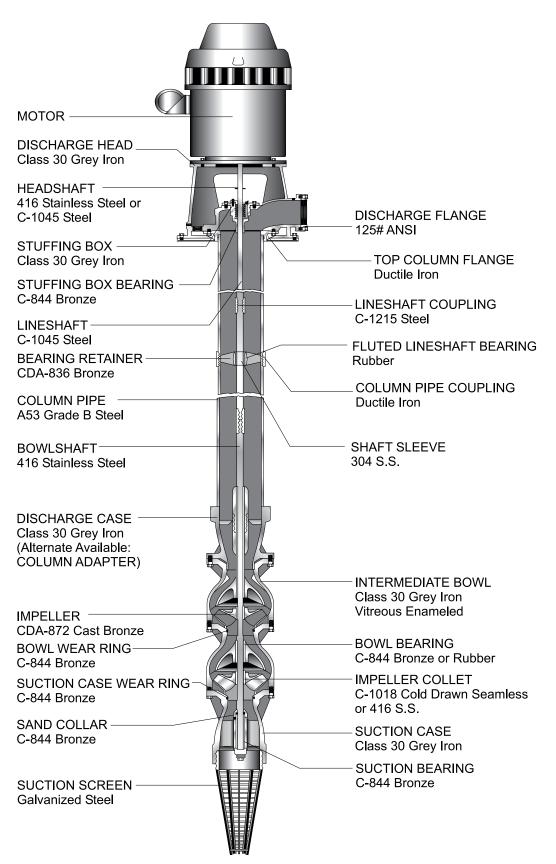
BARREL TYPE BELOW GROUND SUCTION ABOVE GROUND SUCTION

DRIVER ELECTRIC MOTOR RAGD COMBINATION TYPE **DIESEL ENGINE**

TYPE OF DRIVER HOLLOWSHAFT SOLID SHAFT



PRODUCT LUBRICATED DEEP WELL VERTICAL TURBINE PUMP





STANDARD PUMP SPECIFICATION PRODUCT LUBRICATED DEEP WELL VERTICAL TURBINE PUMP

GENERAL

The contractor shall furnish a deep well product lubricated lineshaft vertical turbine pump, manufactured by NATIONAL PUMP or equal, with above ground discharge and furnished with suitable driver and accessories to meet the requirements herein or as shown on the drawings. The pump shall be designed and furnished to conform to the Hydraulic Institute and AWWA specifications for Lineshaft Turbine Pumps and shall comply with all local and state sanitary and safety regulations.

INFORMATION REQUIRED IN PROPOSAL

1. Data sheet completely filled in.

2. Performance curve showing expected performance at design point. Curve will show head, capacity, efficiency, and horsepower based on bowl performances and shall cover the complete operation range of the pump from zero capacity to the maximum capacity.

3. Drawings of the proposed equipment giving general dimensions sufficient to determine how the equipment is to be supported and if it will fit within the space available.

4. Any additional information such as descriptive literature, manufacturer's specifications, and other data to demonstrate compliance with these specifications.

CONDITIONS OF SERVICE

Design conditions_____USGPM, @____feet total dynamic head (TDH), Minimum bowl efficiency _____%, Overall length, bottom of discharge head to bottom of strainer _____feet, Well inside diameter_____inches, Maximum allowable speed______RPM.

PUMP CONSTRUCTION

DISCHARGE HEAD: Shall be of close grained, cast iron ASTM A48 Class 30, or fabricated steel, accurately machined with a rabbet fit for mounting the driver and supporting the pump column assembly and with above ground discharge flange machined and drilled to ANSI standards for _____# rating and ______ inches inside diameter. The design shall allow for the headshaft to couple above the stuffing box.

The standard stuffing box shall be cast iron and rated for _______ discharge pressure and shall contain a minimum of five acrylic graphite packing rings and shall have a grease chamber. The packing gland shall be bronze secured in place with stainless steel studs and adjusting nuts. The stuffing box bearing shall be C89835 bismuth bronze. A rubber slinger shall be installed on the top shaft above the packing gland. The top shaft shall be 416 S.S. and shall extend through the stuffing box.

The headshaft shall be C-1045 carbon steel. Impeller adjustment shall be provided at the top of the headshaft by means of an adjusting nut which shall be locked in place.

COLUMN PIPE shall be ASTM A53 grade B steel pipe, sized such that the friction loss will not exceed 5 ft. per 100 ft., based on the rated capacity of the pump and shall weigh not less than ______ lbs/ft. The column pipe shall be furnished in interchangeable sections not more than (10) ft. in length for 1800 RPM and (5) ft. for 3600 RPM and shall be connected with threaded sleeve type couplings. The ends of each section of column pipe shall be machined with 8 threads per inch with 3/16" taper and faced parallel and the threads machined to such a degree that the ends butt against the bearing retainer shoulder to ensure proper alignment and to secure the bearing retainers when assembled.

NOTE: TOP AND BOTTOM SECTIONS SHALL NOT EXCEED 5 FT. IN LENGTH.



COLUMN ASSEMBLY - PRODUCT LUBRICATED

LINESHAFTS shall be C-1045 turned, ground and polished. They shall be furnished in interchangeable sections not over (10) feet in length. The shaft shall be sized in accordance with the maximum recommended horsepower for a given size of shaft, taking into account the effect of the hydraulic thrust on the pumping equipment and the weight of the shaft and suspended rotating parts. To ensure accurate alignment of the shafts, they shall be straight within 0.005 in. total indicator reading for a 10 ft. section. The butting faces shall be machined with center relief and square to the axis of the shaft. The lineshaft shall be provided with 304 stainless steel sleeves at the location of each bearing retainer. The lineshaft shall be coupled with 1215 steel couplings, and shall be held in place by bronze bearing retainers with neoprene bearings at each threaded joint.

BOWL ASSEMBLY

PUMP BOWLS shall be of close grained, cast iron ASTM A48 Class 30 and shall be free of blow holes, sand holes, or other detrimental faults and shall be accurately machined and fitted to close tolerances. The bowls shall have vitreous enamel lined waterways to reduce friction losses and provide a maximum efficiency and wear protection. The intermediate bowls shall be provided with bismuth bonze C89835 bearings. The intermediate bowls shall be fitted with replaceable wear rings of bismuth bonze C89835.

IMPELLERS shall be of cast silicon bronze grade ASTM B584-C876 and shall be enclosed type accurately machined, balanced, and filed for optimum performance. They shall be securely fastened to the shaft with a taper split collet of ______1215 steel or ______316 stainless steel. Impellers shall be dynamically balanced to ISO 1940 G63 or better.

COLUMN ADAPTER OR DISCHARGE CASE shall be close grained cast iron ASTM A48 class 30, threaded to properly match the discharge column.

SUCTION CASE shall be fitted with a replaceable wear ring of bismuth bronze C89835, grease packed bismuth bronze C89835 bearing and protected by a bismuth bronze C89835 sand collar.

BOWL SHAFT shall be ASTM A276 grade 416 stainless steel, turned, ground and polished.

SUCTION PIPE AND STRAINER

The suction pipe shall be ______ft. in length and of a size and weight at least equal to that of the column pipe. A galvanized steel strainer shall be provided having a net inlet area equal to at least four times the suction pipe area.

<u>MOTOR</u>

The motor shall be squirrel cage induction design, NEMA design B, ______ RPM vertical hollow shaft motor, with a non-reverse ratchet. Thrust bearing shall be chosen to handle the entire hydraulic thrust load of the pump plus the weight of the rotating parts. With an AFBMA B-10 one year minimum or five year average life under design conditions. The motor shall be premium efficiency with a WP-1 enclosure, 1.15 service factor, for use on ______ volt, three phase, 60 cycle electric service. The motor rating shall be such that at design it will not be loaded beyond nameplate rating and at no place on the pump curve shall the loading exceed the service factor.

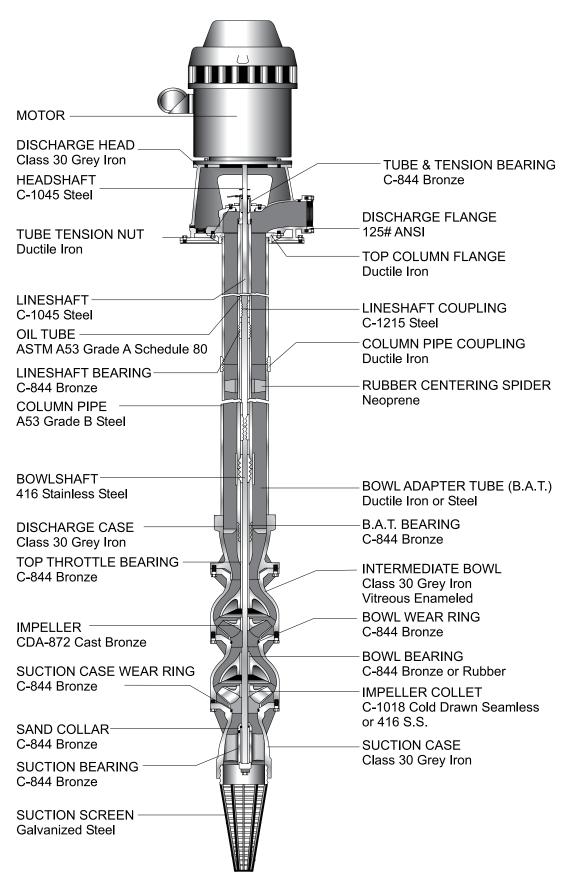


NOTES

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GENERAL INFORMATION

OIL LUBRICATED DEEP WELL VERTICAL TURBINE PUMP





STANDARD PUMP SPECIFICATION OIL LUBRICATED DEEP WELL TURBINE PUMP

GENERAL

The contractor shall furnish a deep well oil lubricated lineshaft vertical turbine pump, manufactured by NATIONAL PUMP or approved equal, with above ground discharge and furnished with suitable driver and accessories to meet the requirements herein or as shown on the drawings. The pump shall be designed and furnished to conform to the Hydraulic Institute and AWWA specifications for Lineshaft Turbine Pumps and shall comply with all local and state sanitary and safety regulations.

INFORMATION REQUIRED IN PROPOSAL

- 1. Data sheet completely filled in.
- Performance curve showing expected performance at design point. Curve will show head, capacity, efficiency, and horsepower based on bowl performances and shall cover the complete operation range of the pump from zero capacity to the maximum capacity.
- 3. Drawings of the proposed equipment giving general dimensions sufficient to determine how the equipment is to be supported and if it will fit within the space available.
- 4. Any additional information such as descriptive literature, manufacturer's specifications, and other data to demonstrate compliance with these specifications.

CONDITIONS OF SERVICE

Design condition	sUSGPM, @	feet total dynamic head (TDI	H), Minimum bowl efficiency
%	, Overall length, bottom of discharge	head to bottom of strainer	feet, Well inside
diameter	inches, Maximum allowable spee	edRPM.	

PUMP CONSTRUCTION

DISCHARGE HEAD: Shall be of close grained, cast iron ASTM A48 Class 30, or fabricated steel, accurately machined with a rabbet fit for mounting the driver and supporting the pump column assembly and with above ground discharge flange machined and drilled to ANSI standards for ______# rating and ______ inches inside diameter. The design shall allow for the headshaft to couple above the tube tension assembly.

The tube tension assembly shall consist of a bronze CDA836 tension bearing installed in top oil tube, threaded tension nut to apply proper tension on oil tube, sealing between tension nut and discharge head shall be accomplished with "o" rings. Locknut with "o" ring and set screw to lock tension assembly after proper tension is accomplished.

Discharge head shall be furnished with one gallon oil reservoir with copper tubing, _____ manual or _____ solenoid valve and sight feed drip oiler.

The headshaft shall be C-1045 carbon steel. Impeller adjustment shall be provided at the top of the headshaft by means of an adjusting nut which shall be locked in place.

COLUMN PIPE shall be ASTM A 53 grade B steel pipe. Size shall be such that the friction loss will not exceed 5 ft. per 100 ft., based on the rated capacity of the pump and shall weigh not less than ______ lbs/ft. The column pipe shall be furnished in interchangeable sections not more than (10) or (20) feet in length and shall be connected with threaded sleeve type couplings. The ends of each section of column pipe shall be machined with 8 threads per inch with 3/16" taper and faced parallel permitting the ends to butt insuring alignment.

NOTE: TOP AND BOTTOM SECTIONS SHALL NOT EXCEED 10 FT. IN LENGTH.



COLUMN ASSEMBLY - OIL LUBRICATED

SHAFT ENCLOSING TUBES shall be ASTM A53 Grade A schedule 80 steel pipe with the ends machined square and parallel and shall butt to ensure proper alignment and sealing, they shall be straight within 0.005 in. total indicator reading for a 5 ft. section. Threaded internally to receive the lineshaft bearings. The enclosing tube shall be stabilized and centered in the column pipe by rubber centering spiders spaced at 40 ft. intervals throughout the column pipe assemblies.

LINESHAFT BEARINGS shall be C-844 bronze, internally grooved to allow proper lubrication to enclosed lineshaft and threaded externally for connecting oil tube sections.

LINESHAFTS shall be C-1045 carbon steel, turned, ground and polished. They shall be furnished in interchangeable sections not over (10) or (20) feet in length to properly match the shaft enclosing tube and discharge column. The shaft shall be sized in accordance with the maximum recommended horsepower for a given size of shaft, taking into account the effect of the hydraulic thrust on the pumping equipment and the weight of the shaft and suspended rotating parts. To ensure accurate alignment of the shafts, they shall be straight within 0.005 in. total indicator reading for a 10 ft. section and 0.010 in. total indicator reading for a 20 ft. section. The butting faces shall be machined with center relief and square to the axis of the shaft. The lineshaft shall be coupled with 1215 steel couplings.

BOWL ASSEMBLY

DISCHARGE CASE shall be cast with by-pass ports to allow release of fluids through the throttle bearing. The discharge case shall be fitted with a Bowl Adapter Tube for connection to the enclosing tube and threaded for connection to the discharge column pipe. The Bowl Adapter Tube will have a bronze sleeve bearing in the bottom and threaded for a bronze lineshaft bearing on top.

TOP BOWL shall have an extra long throttle bearing with two seals to minimize the amounts of leakage through the drain ports.

PUMP BOWLS shall be of close grained, cast iron ASTM A48 Class 30 and shall be free of blow holes, sand holes, or other detrimental faults and shall be accurately machined and fitted to close tolerances. The bowls shall have vitreous enamel lined waterways to reduce friction losses and provide a maximum efficiency and wear protection. The intermediate bowls shall be provided with C89835 bismuth bronze bearings. The intermediate bowls shall be fitted with replaceable wear rings of C89835 bismuth bronze.

IMPELLERS shall be of cast silicon bronze grade ASTM B584-C876 and shall be enclosed type accurately machined, balanced, and filed for optimum performance. They shall be securely fastened to the shaft with a taper split collet of ______1215 steel or ______316 stainless steel.

SUCTION CASE shall be fitted with a replaceable wear ring of bismuth bronze C89835, grease packed bismuth bronze C89835 bearing and protected by a bismuth bronze C89835 sand collar.

BOWL SHAFT shall be ASTM A276 grade 416 stainless steel, turned, ground and polished.

SUCTION PIPE AND STRAINER

The suction pipe shall be ______ft. in length and of a size and weight at lease equal to that of the column pipe. A galvanized strainer shall be provided having a net inlet area equal to at least four times the suction pipe area.

MOTOR

The motor shall be squirrel cage induction design, NEMA design B, ______ RPM vertical hollow shaft motor, with a non-reverse ratchet. Thrust bearing shall be chosen to handle the entire hydraulic thrust load of the pump plus the weight of the rotating parts. With an AFBMA B-10 one year minimum or five year average life under design conditions. The motor shall be premium efficiency with a WP-1 enclosure, 1.15 service factor, for use on _____ volt, three phase, 60 cycle electric service. The motor rating shall be such that at design it will not be loaded beyond nameplate rating and at no place on the pump curve shall the loading exceed the service factor.



Selecting a Vertical Turbine Pump (Information required from client)

1.	Liquid to be pumped: (Note: If liquid is not clear water, the following must also be ascertained).		
	 a. Foreign material present in liquid (describe): b. Specific gravity at pumping temperature: c. Vapor pressure at pumping temperature: d. Viscosity at pumping temperature: 		
2.	Pumping temperature:F		
3.	Required capacity:GPM		
4.	Required pressure at centerline of discharge flange:PSI		
5.	Pumping water levelft. below centerline of pump discharge (static water level plus drawdown).		
6.	 Inside diameter of well or sump:inches. Note: Well or sump must be sufficiently straight or o sufficient diameter to allow bowl assembly and column to hang free and plumb). 		
7.	Size of dischargeinches. Companion flange required?YesNo		
8.	. Required length of column or overall length of pumpft (indicate which).		
9.	Lineshaft lubrication arrangement (per below):		
	Open lineshaftEnclosed lineshaftEnclosed lineshaft (lubricated w/ liquid pumped) (oil lubricated) (injection lubricated)		
	Rubber bearingsRedwood bearingsBronze bearings		
	Bronze bearings Bronze bearings Rubber bearings		
10	. Suction pipe required?Yes lengthftNo.		
11.	. Strainer required?Yes (ConicalBasket)No.		
12	12. Special material requirements (describe)		
	If fluid is corrosive, list satisfactory materials		
13	. Type of driver		
	. Speed of driver:RPM Gear ratio		
15	Self release coupling ornon reverse ratchet		
16	Current characteristicsphaseHzvolts		
17	. Other driver requirements		



GENERAL INFORMATION

"Sample" Pump Data Selecting a Vertical Turbine Pump (Information required from client)

 Liquid to be pumped: <u>Clear water</u> (Note: If liquid is not clear water, the following must also be ascertained). 		
 a. Foreign material present in liquid (describe):None b. Specific gravity at pumping temperature:1.0 c. Vapor pressure at pumping temperature: d. Viscosity at pumping temperature: 		
2. Pumping temperature:AmbF		
3. Required capacity:800GPM		
4. Required pressure at centerline of discharge flange:30PSI		
5. Pumping water level 180 + 20 ft. below centerline of pump discharge (static water level plus drawdown).		
 Inside diameter of well or sump:16"inches. Note: Well or sump must be sufficiently straight or of sufficient diameter to allow bowl assembly and column to hang free and plumb). 		
7. Size of discharge8" inches. Companion flange required?YesX_No		
8. Required length of column or overall length of pump250ft (indicate which).		
9. Lineshaft lubrication arrangement (per below):		
XOpen lineshaftEnclosed lineshaftEnclosed lineshaft(lubricated w/ liquid pumped)(oil lubricated)(injection lubricated)XRubber bearingsRedwood bearingsBronze bearingsBronze bearingsBronze bearingsRubber bearings		
10. Suction pipe required? X Yes length 10 ′ftNo.		
11. Strainer required?X_Yes (X_ConicalBasket)No.		
12. Special material requirements (describe)		
If fluid is corrosive, list satisfactory materials		
13. Type of driver <i>Electrical Motor</i>		
14. Speed of driver:1800RPM Gear ratio		
15Self release coupling orXnon reverse ratchet		
16. Current characteristics3phase60Hz460volts		
17. Other driver requirements Vertical Hollow Shaft, WPI enclosure		



INFORM

Selecting a Vertical Turbine Pump

Since the inside diameter of the well is 16 inches, a 15 inch (or smaller bowl assembly must be selected. With this in mind, refer to the performance curves in the catalog for a unit whose capacity at or near the best efficiency point is 800 GPM. It is found that a J11HC at 1760 RPM will produce 72.3 feed head per stage at this capacity.

Tentative Total Head must be determined by a summation of the required lift, discharge pressure, and an assumed column loss (the actual column loss will be found later). Assume 5 feet loss per 100 feet of column (or 0.06 ft. per foot).

Calculate as follows:

Tentative Total Head = 180 + 20 + (30 x 2.31) + (0.05 x 250) = 281.8 ft. Where: 180 = static water level below discharge. 20 = draw down in feet 30 = pressure at the centerline of the discharge in PSI 2.31 = feet of water equivalent to one PSI 0.05 = assumed loss per foot of column 250 = total length of aslump in fact

250 = total length of column in feet

Number of Stages required is found by dividing the tentative total head by the head per stage as taken from the performance curve as follows:

Number of stages = $\frac{281.8}{72.3}$ = 3.9

Where: 281.8 = tentative total head

72.3 = head per stage from performance curve

Since fractional stages are not feasible, the next larger whole number must be used. Or, in this case, 4 stages.

Efficiency as shown on the performance curve must be corrected in accordance with the schedule at the top of the performance curve for number of stages (corrections are also required when bowls and/or impellers are non-standard materials). Note that in this example, no efficiency correction is required and the bowl efficiency shown on the curve can be used.

Tentative Brake Horsepower can be calculated as follows:

Tentative BHP = <u>281.8 x 800 x 1.0</u> = 66.20 3960 x .86

Where: 281.8 = tentative total head in feed
800 = capacity in gallons per minutes
1.0 = specific gravity of water
3960. = a constant for converting feed TDH and gallons per minutes to horsepower
0.86 = the efficiency as read from the performance curve and corrected by the schedule on the curve. (Expressed as decimal).

At this point, refer to the "Bowl Assembly Data and Limitations" table located in the Engineering Section of the catalog. This table shows that the maximum recommended number of stages for a J11HC is 20. Since the selection that has been made contains four stages, this is satisfactory.



It is further noted that the bowl diameter is 11-1/8" which is small enough to be installed in a 16" well. The maximum head (Bowl Assembly Data and Limitations) for this pump is 377 PSI (871 feet), but the required total head for this application is only 281.8 feet, therefore, this is satisfactory. It will also be noted in the Bowl Assembly Data and Limitation table that a J11HC has a 1-11/16" diameter bowl shaft. The horsepower rating chart for lineshafts shows that a 1-11/16" shaft is adequate for 335 horsepower therefore, since the estimated horsepower required for this application is 66.20, the standard bowlshaft size is satisfactory.

Lineshaft size depends on the speed, (RPM), horsepower and downthrust. The "Shaft Horsepower Rating" chart in the engineering section shows a 1 ¹/₄" lineshaft to be adequate for this application.

Column size depends on the sizes which will fit any given bowl selection, the lineshaft size and the capacity in gallons per minute. From the pump data dimensions page (on the bottom of the curve sheet), it is found that a J11HC can be adapted to a column and from the Column Friction Loss Chart in the engineering section it is found that at 800 GPM, an 8" column with a 1 ¼" lineshaft produces a friction loss of 2.2 feet per 100 feet of column and that a 6" column size is not recommended for this capacity.

A generally accepted criteria for column size selection is that the size be selected such that the friction loss will not exceed 5 feet per 100 feet of column.

Total Head required can now be found by using the hydraulic friction loss for an 8" column with a 1 1/4" shaft as follows:

 $\frac{2.2 \times 250}{\text{TDH} = 180 + 20 + 100} + (30 \times 2.31) + 0.11 = 274.9 \text{ ft.}$ Where: 180 = static water level below discharge 20 = drawdown 2.2 = hydraulic friction loss per 100 ft. column 250 = length of column 30 = required pressure (PSI) at centerline of discharge 2.31 = feed of water equivalent to one PSI 0.11 = friction loss for 8" cast discharge head (engineering section)

Since four stages are required in this illustration, the head requirement per stage is 274.9 divided by 4 = 68.73 ft. Upon re-checking the performance curve in the catalog, it is found that the required head per stage at 800 GPM lies between the top curve and the middle curve and that the efficiency is 86%. In other applications in which the hydraulic condition point is found to lie above the highest head curve on the performance curve, it indicates that the pump will fall short of the desired hydraulic performance and that another stage should be added. In cases where the hydraulic condition point falls below the lowest head curve on the performance curve it suggests that the number of stages should be reduced or the factory contacted if reducing the number of stages is not practical.

Hydraulic Thrust = 274.9 x 7.8 = 2144 lbs.

Where: 274.9 = total head

7.8 = thrust factor for impeller

The thrust factor can be found on the performance curve or Bowl Assembly Data and Limitation page (Engineering section or bottom of the curve sheet).

Shaft Elongation can be found by using the value shown in the "Shaft Elongation Chart" (Engineering section). The elongation of a 1 $\frac{1}{4}$ " lineshaft, 250 feet long, with 2144 pounds hydraulic thrust is 0.18" (0.070 x 2.5) (0.070 is interpolated). This shaft elongation must be less than the maximum lateral dimension shown in the Bowl Assembly Data and Limitation table. For a J11HC, the lateral dimension is 1". This indicates that the standard lateral available in the bowl assembly is adequate for the shaft stretch.



Total Downthrust is found by the summation of the hydraulic thrust and the total weight of the rotating assembly: Total downthrust = $2144 + (18.5 \times 4) + (250 \times 4.17) = 3260.50$ lbs.

Where: 2144 = hydraulic thrust

- 18.5 = weight of each stage taken from the Bowl Assembly Data and Limitation table.4 = number of stages (or impellers)
- 250 = length of column (or shaft)
- 4.7 = weight per foot of 1 ¹/₄ inch line shafting taken from the Shaft Weight Table (Section I)

Shaft Mechanical Friction Loss is found on the Shaft Friction Loss Chart (Engineering section). This chart show that 0.79 BHP is lost per 100 feet of 1 $\frac{1}{4}$ " shafting at 1760 RPM. This loss must be included in the determination of the prime mover horsepower requirement as follows:

BHP =
$$\frac{274.9 \times 800 \times 1.0}{3960 \times .86} + \frac{0.79 \times 250}{100} = 66.55$$

Where: 274.9 = total head in feet 800 = capacity in gallons per minute 1.0 = specific gravity of water 3960 = Ft-GPM/HP constant 0.86 = efficiency expressed as a decimal 0.79 = shaft losses per 100 feet 250 = length of column in feet

The above horsepower represents the requirement at the design point of 800 GPM and 30 PSI at the centerline of the discharge, but when selecting a prime mover, the maximum horsepower across the performance curve must also be considered.

Referring back to the J11HC performance curve it is found that the maximum horsepower is approximately 4 horsepower per stage higher at 1300 GPM that at 800 GPM for the top curve and 2 horsepower higher at 1250 GPM for the middle curve. Since the job requirements (hydraulic performance) lie between the top and middle curves it can be estimated that the maximum horsepower will be 3 horsepower per stage more than design horsepower and occur at 1275 GPM. The approximate maximum horsepower can be calculated as follows:

Max BHP =- 66.55 + (3 x 4) = 78.50

Where: 66.55 = design HP as calculated

3 = estimated rise in HP per stage

4 = number of stages

It is usually good practice and in many cases necessary to size the prime mover for the higher horsepower. The final decision as to whether or not the prime mover should be sized for the higher horsepower depends on the type of application. If the pump installation is such that they hydraulic conditions at the higher horsepower can never exist, then the higher horsepower is of no importance but, on the other hand, if there is a possibility that the unit may operate for an extended period at the higher horsepower conditions then the prime mover should be sized for the higher horsepower. From the above, it can now be said that the pump will require 66.55 horsepower when operating at design head and capacity but 78.5 horsepower may be required under other operating conditions. With this information and the other motor requirements as set forth by the client, a motor catalog can be consulted for further details.



Motor or engine and right angle gear size depends on the speed (RPM), total downthrust and horsepower requirement of the pump. In this illustration, a vertical hollowshaft electric motor is to be used, therefore, a right angle gear will not be required. Right angle gears are used only when the prime mover is designed for horizontal mounting, such as an engine, turbine, etc.

In this application it is apparent that we can use a 75 horsepower 1800 RPM, 3 phase, 60 cycle, 460 volt vertical hollow shaft motor in a weather protected enclosure with a non-reverse ratchet and thrust bearings capable of sustaining 3622 lbs. downthrust. Note that a 75 horsepower motor with a 1.15 service factor is capable of 86 horsepower (75 x 1.15) but may not be used for this application if the pump has to be non-overloading on the curve. A 100 HP motor should be used. At this point, it is advisable to recheck the horsepower rating of the lineshaft that was selected. In the preliminary selection of the lineshaft, hydraulic thrust was used whereas the total thrust should be used for final sizing. Also, the possibility that the pump may on occasions be operated at a higher horsepower was not taken into account. Upon rechecking the Lineshaft Horsepower Rating Chart, it is found that the previously selected 1 ¼" lineshaft with 3260 pounds downthrust has a horsepower limitation of 124 horsepower. Therefore, the lineshaft as initially selected is adequate for this application.

Discharge Head selection depends on the discharge size, column size and the base diameter (BD) of the driver. In this particular example, it will be noted in the electric motor catalog that a 75 horsepower 1800 RPM VHS motor has a BD dimension of either 16 $\frac{1}{2}$ inches or 12 inches. Therefore an 8 inch discharge head with either a 12" or 16 $\frac{1}{2}$ " BD will be satisfactory.

Referring to the Discharge Head section of the catalog, it will be found that an N8-260 discharge head has a BD dimension of 16 $\frac{1}{2}$ " which is satisfactory for the motor required. The N8-260 discharge head will accept the 8" column and 1 $\frac{1}{4}$ " shaft and has an 8" discharge and is satisfactory for 250' setting.

Suction Pipe and Strainers should be selected to fit the intake connection of the bowl assembly. Referring to the performance curve; the J11HC will accept 8" suction pipe. It is common to use the same size suction pipe as column pipe so an 8" suction pipe would be selected.

Conical strainers are recommended for well service while the basket type strainers are used when pumping from sumps or other large bodies of liquid. Size to fit the suction pipe or bowl assembly.

Lubrication of the lineshaft bearings of an open lineshaft pump is accomplished by the pumped fluid, however some method of providing initial lubrication as start up must be provided see "Pre-lubrication Recommendations" in this section of the catalog.

Enclosed lineshaft pumps are usually lubricated by oil, the necessary reservoir and fittings for a manual system are included as standard equipment with the discharge head assembly.

The pump selection is now completed and can be summarized as follows:

- 1. Suction pipe with strainer
- 2. 4 stage J11HC bowl assembly
- 3. 250 feet of 8" x 1 ¼" column and open lineshaft
- 4. N8-260 discharge head assembly
- 5. 75 horsepower 1800 RPM 3/60/460 volt VHS weather protected motor for 3622 lbs. downthrust and with non-reverse ratchet.



INDUSTRIAL PUMP SPECIFICATION PRODUCT LUBRICATED CLOSE COUPLED TURBINE PUMP

GENERAL

The contractor shall furnish an industrial product lubricated lineshaft vertical turbine pump, manufactured by NATIONAL PUMP or approved equal, with above ground discharge and furnished with suitable driver and accessories to meet the requirements herein or as shown on the drawings. The pump shall be designed and furnished to conform to the Hydraulic Institute and AWWA specifications for Lineshaft Turbine Pumps and shall comply with all local and state sanitary and safety regulations.

INFORMATION REQUIRED IN PROPOSAL

- 1. Data sheet completely filled in.
- 2. Performance curve showing expected performance at design point. Curve will show head, capacity, efficiency, and horsepower based on bowl performances and shall cover the complete operation range of the pump from zero capacity to the maximum capacity.
- 3. Drawings of the proposed equipment giving general dimensions sufficient to determine how the equipment is to be supported and if it will fit within the space available.
- 4. Any additional information such as descriptive literature, manufacturer's specifications, and other data to demonstrate compliance with these specifications.

CONDITIONS OF SERVICE

Design conditions_____USGPM, @_____feet total dynamic head (TDH), Minimum bowl efficiency _____%, Overall length, bottom of discharge head to bottom of strainer _____feet, sump depth _____feet, Suction barrel (if required) length _____inches and diameter _____inches, Maximum allowable speed ______RPM.

PUMP CONSTRUCTION

DISCHARGE HEAD: Shall be of close grained, cast iron ASTM A48 Class 30, or fabricated steel, accurately machined with a rabbet fit for mounting the driver and supporting the pump column assembly and with above ground discharge flange machined and drilled to ANSI standards for ______# rating and ______ inches inside diameter. The design shall allow for the headshaft to couple above the mechanical seal or stuffing box.

The standard stuffing box shall be cast iron and rated for _______ discharge pressure and shall contain a minimum of five acrylic graphite packing rings and shall have a grease chamber. The packing gland shall be bronze secured in place with stainless steel studs and adjusting nuts. The stuffing box bearing shall be C89835 bismuth bronze. A rubber slinger shall be installed on the top shaft above the packing gland. The top shaft shall be 416 S.S. and shall extend through the stuffing box.

If a mechanical seal is used, then a four piece spacer type coupling shall be used to allow seal replacement without motor removal. This will require a motor stand to be used with a cast iron discharge head or an extra height fabricated steel discharge head.

Impeller adjustment shall be provided at the top of the headshaft by means of an adjusting nut which shall be locked in place.

COLUMN PIPE shall be ASTM A 53 grade B steel pipe. Size shall be such that the friction loss will not exceed 5 ft. per 100 ft., based on the rated capacity of the pump and shall weigh not less than ______ lbs/ft. The column pipe shall be furnished in interchangeable sections not more than (10) feet in length for 1800 RPM and (5) feet for 3600 RPM and shall be threaded or flanged. If threaded, the ends of each section of column pipe shall be machined with 8 threads per inch with 3/16" taper and faced parallel and the threads machined to such a degree that the ends butt against the bearing retainer shoulder to ensure proper alignment and to secure the bearing retainers when assembled.

NOTE: TOP AND BOTTOM SECTIONS SHALL NOT EXCEED 5 FEET IN LENGTH.



COLUMN ASSEMBLY - PRODUCT LUBRICATED

LINESHAFTS shall be 416 stainless steel, turned, ground and polished. They shall be furnished in interchangeable sections not over (10) feet in length for 1800 RPM and (5) feet for 3600 RPM to properly match the discharge column. The shaft shall be sized in accordance with the maximum recommended horsepower for a given size of shaft, taking into account the effect of the hydraulic thrust on the pumping equipment and the weight of the shaft and suspended rotating parts. To ensure accurate alignment of the shafts, they shall be straight within 0.005 in. total indicator reading for a 10 ft. section. The butting faces shall be machined with center relief and square to the axis of the shaft. The lineshaft shall be coupled with 304 S.S. stainless steel couplings, and shall be held in place by bronze bearing retainers with neoprene bearings at each flanged or threaded joint.

BOWL ASSEMBLY

PUMP BOWLS shall be of close grained, cast iron ASTM A48 Class 30. Shall be free of blow holes, sand holes, or other detrimental faults and shall be accurately machined and fitted to close tolerances. The bowls shall have vitreous enamel lined waterways to reduce friction losses and provide a maximum efficiency and wear protection. The intermediate bowls shall be provided with bismuth bonze C89835 bearings. The intermediate bowls shall be fitted with replaceable wear rings of bismuth bonze C89835.

IMPELLERS shall be of cast silicon bronze grade ASTM B584-C876 and shall be enclosed type accurately machined, balanced, and filed for optimum performance. They shall be securely fastened to the shaft with a taper split collet of ______1215 steel or ______316 stainless steel. Impellers shall be dynamically balanced to ISO 1940 G63 or better.

COLUMN ADAPTER shall be of close grained cast iron ASTM A48 class 30, threaded to properly match the discharge column. (Note: If column pipe is flanged, column adapter is not required.)

SUCTION BELL shall be fitted with a replaceable wear ring of bismuth bronze C89835, grease packed bismuth bronze C89835 bearing and protected by a bismuth bronze C89835 sand collar. Suction shall be fitted with a galvanized steel clip on type basket strainer.

BOWL SHAFT shall be ASTM A276 grade 416 stainless steel, turned, ground and polished.

MOTOR

The motor shall be squirrel cage induction design, NEMA design B, ______ RPM vertical hollow shaft motor*, with a non-reverse ratchet. Thrust bearing shall be chosen to handle the entire hydraulic thrust load of the pump plus the weight of the rotating parts. With an AFBMA B-10 one year minimum or five year average life under design conditions. The motor shall be premium efficiency with a WP-1 enclosure, 1.15 service factor, for use on _____ volt, three phase, 60 cycle electric service. The motor rating shall be such that at design it will not be loaded beyond nameplate rating and at no place on the pump curve shall the loading exceed the service factor.

* Solid shaft with mechanical seal.



Selecting a Short Coupled Vertical Turbine Pump

GENERAL

Step 1 Bowl Selection

From the catalog rating curves select the bowl assembly which will meet the customer's requirements with respect to capacity and total dynamic head. Usually the operating speed (RPM) will be specified. 1800 RPM (nominal) is the most common operating speed, although 3500 RPM is widely used for clean fluid service. In general, lowering the operating speed will lower the noise and vibration level, increase the life expectancy of the pump and increase the initial investment.

Step 2 Column and Shaft Assembly

Select the length of column and shaft to suit the overall length of the pump. Refer to the "Bowl Assemblies" section for dimensional data on bowl assemblies. Due to the relative short lengths of column involved it is common to select column size for higher friction losses than would be desirable for deep well units. A friction loss of 7-1 /2' per 100' is generally acceptable.

On units requiring less than 5 feet of column length at speeds up to 1800 RPM, a bearing will not be included in the column. Should, for example, the column requirements work out to be 12'0", two bearings will be installed at 5' intervals above the bowl assembly, with a 2' column pipe below the discharge head. Therefore, the column assembly should be selected as follows:

1800 RPM Maximum*	
up to 5' column length required	1 section
5' to 10' column length required	2-5' sections
10' to 15' column length required	3-5' sections
More than 15'	2-5' sections and additional 10' sections as required.
Above 1900 DDM	

Above 1800 RPM 5' bearing centers required.

Lineshaft size DOES NOT necessarily have to match the bowl shaft size. For the shaft size and horsepower ratings refer to the "Engineering Section" of the catalog. Minimum recommended line shaft size for short coupled pumps regardless of horsepower is 1".

Step 3 Discharge Head

Once the column and shaft sizes have been determined, the head selection follows. The discharge size will usually be specified, if not, the following can be used as a guideline.

Discharge Size	Maximum Recommended Capacity*
4"	. 475 GPM
6"	. 1050 GPM
8"	. 1900 GPM
10"	. 3000 GPM
12"	. 4700 GPM
14"	. 5700 GPM

*Based on velocity of 12 F.P.S.



Check the driver mounting flange for compatibility with the discharge head. Remember ----a 10" B.D. drive will mount on a 12" BD discharge head and vice-versa, also a 16 ½" BD driver will mount on a 20" BD discharge head. We must know the driver manufacturer, "CD" dimension, "BD" dimension, clutch size and keyway, and frame number if the customer furnishes his own driver (preferably send certified prints with order).

Remember, the maximum working pressure of the standard cast iron discharge head is 175 PSI for the N-260 model and 275 PSI for the HI-PRO model. Above this, a fabricated discharge head must be used. A hipressure packing box will be required if the pressure exceeds 175 PSI (price addition required).

A discharge companion flange will usually not be required, if desired a price addition is required. Applicable discharge head dimensions can be found in the "Discharge Head" section of the catalog.

Step 4 Driver

The driver requirements are usually specified. Hollow shaft drivers are more common due to the ease of the shaft adjustment and lower initial cost (up to about 250 HP) of the complete unit. Solid shaft drivers should be considered for the larger units and for certain mechanical seal applications (see mechanical seal pages in "Discharge Head" section for details). Hollow shaft motors are available equipped with a steady bushing. Steady Bushings are required when mechanical seals are used in conjunction with hollow shaft motors regardless of speed, and when the shaft span between the packing box and motor clutch on 3600 RPM units exceed the following:

Shaft Diameter	Maximum Span
1"	36"
1 3/16"	41"
1 1⁄2"	47"
1 11/16"	50"

Solid shaft drivers provide rigid shaft support near the shaft sealing device and can always be recommended where the cost is not prohibitive. Adjustable couplings must be used with solid shaft drivers. Spacer type adjustable couplings are recommended when mechanical seals are used to allow removal of the mechanical seal without removing the driver. See "Discharge Head" section for details on adjustable couplings.

Step 5 Special Requirements

The specifications and/or service requirements should be carefully reviewed for special requirements such as strainers, non-standard materials, mechanical seals, driver protective devices, special painting or coating, tests, etc. See Engineering (Pump Selection) section for further detailed instructions on pump selection.

Step 6 Assembly and Shipping

All close coupled vertical turbine pumps as standard will be shipped assembled (bowl, column and discharge head) as long as the total pump length (T.P.L.) as measured from the bottom of the discharge head or base plate, if used, to the bottom of the suction bell, suction case, or strainer, if used, does not exceed 15 ft.

The driver, drive coupling, head shaft and mechanical seal are never shipped assembled to the pump to prevent damage during transit.

When the T.P.L. exceeds 15 ft. the pump will be shipped in separate assemblies (bowl assembly, column assembly, discharged head assembly, drives, mechanical seal and miscellaneous parts).

For pumps requiring assembly that exceed 15 ft. T.P.L. as defined above, contact the factory for special price additions.



NOTES

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STANDARD BOWL ASSEMBLY LIMITATIONS DATA

This pages lists the limitations of National Pump bowl assemblies. See next page for additional notes.

	т	HRUST DATA									MAXIMUM
MODEL	FACTOR "K" (1)	1 STG. WEIGHT	ADDL. STG. WT.		-ATERAL 2)	SHAFT DIA.	WR2 (WET) LBS. (3)	EYE AREA IN.2	SPHERE SIZE MAX. (4)	MAX # STG. (5)	ALLOWABLE NON-SHOCK PRESSURE OPERATING
			•••	STD.	MAX.		LDO. (J)	114.2	(4)	(3)	(6)
L6LC	1.30	7.5	3.5	3/16	3/8	1	0.14	5.38	0.15	60	430
M6LC	2.40	8.00	3.90	3/16	3/8	1	0.14	3.82	0.15	55	500
M6MC	2.40	8.00	3.90	3/16	3/8	1	0.14	3.88	0.20	55	500
M6HC	2.30	8.00	3.90	3/16	3/8	1	0.14	4.89	0.28	55	500
E6XHC	3.00	8.25	4.00	3/16	3/8	1	0.14	7.12	0.39	32	390
H7LC	4.40	20.00	10.50	3/4	7/8	1 1/4	0.22	9.09	0.47	29	520
H7HC	4.40	21.50	11.50	3/4	7/8	1 1/4	0.25	9.09	0.47	29	520
K8LC	4.70	17.00	10.60	3/4	1	1 1/4	0.27	8.05	0.56	30	480
K8HC	4.70	17.20	8.11	3/4	1	1 1/4	0.27	8.05	0.56	30	480
M8XLC	4.40	20.60	10.60	3/4	7/8	1 1/4	0.32	7.72	0.27	27	460
M8MC	4.40	20.60	10.60	3/4	1 1/4 1	1 1/4 1 1/4	0.32	8.74	0.34	27 27	460
M8HC M8XHC	4.40 4.50	20.60 20.60	10.60 10.60	3/4 5/8	3/4	1 1/4	0.32	8.84 10.70	0.34 0.50	27	460 460
J8XHC	8.20	20.00	12.00	1 3/8	1 5/8	1 1/4	0.32	12.81	0.59	27	400
M9MC	4.30	22.00	11.50	5/8	1 1/8	1 1/4	0.30	9.78	0.39	25	440
M10LC	6.10	32.50	17.00	1	1 3/8	1 1/2	0.43	13.25	0.38	20	390
M10EC	6.10	33.50	18.00	1	1 3/8	1 1/2	0.78	13.25	0.38	20	390
H10MC	7.40	32.50	17.00	1 1/4	1 3/8	1 1/2	0.75	16.89	0.56	20	370
H10HC	7.40	32.50	17.00	1 1/4	1 3/8	1 1/2	0.75	16.89	0.56	20	370
J10HC	9.90	32.80	17.10	1 1/4	1	1 1/2	0.69	21.80	0.25	20	300
K10LC	6.60	21.25	12.50	1	TBD	1 1/2	0.73	13.80	0.69	22	370
K10MC	6.60	21.25	12.50	1	TBD	1 1/2	0.78	13.80	0.69	22	370
K10HC	6.60	21.25	12.50	1	TBD	1 1/2	0.78	13.80	0.69	24	370
L10LC	4.50	10.00	8.00	1/2	TBD	1 1/2	0.44	8.53	0.50	30	500
L10MC	4.50	10.00	8.00	1/2	TBD	1 1/2	0.44	8.53	0.50	30	500
L10HC	4.50	10.00	8.00	1/2	TBD	1 1/2	0.44	8.53	0.50	30	500
E10HC	11.60	34.50	18.00	3/4	1	1 1/2	0.59	26.50	0.75	20	330
E10HO	11.60	34.50	18.00	3/4	1	1 1/2	0.59	26.50	0.75	20	330
J11LC	7.90	38.50	18.50	3/4	1 1/4	1 11/16	1.02	15.90	1.00	20	340
J11LO	10.00	38.50	18.50	3/4	1 1/4	1 11/16	1.02	15.90	1.00	20	340
J11MC	7.90	38.50	18.50	3/4	1 1/4	1 11/16	1.02	15.90	1.00	20	340
J11MO	10.30	38.50	18.50	1	1 1/4	1 11/16	1.02	15.90	1.00	20	340
J11HC	7.90	38.50	18.50	1	1 1/4	1 11/16	1.02	15.90	1.00	20	340
J11HO	10.00	38.50	18.50	1	1 1/4	1 11/16	1.02	15.90	1.00	20	340
M12LC	8.50	40.00	23.50	1	1 1/4	1 11/16	1.51	18.39	0.47	17	330
M12MC	8.30	40.00	23.50	1	1 1/4	1 11/16	1.51	18.39	0.47	17	330
M12HC	8.40	40.00	23.50	1	1 1/4	1 11/16	1.51	18.39	0.63	17	330
E12LC	8.30	43.00	22.50	15/16	1 1/4	1 11/16	1.20	14.07	0.63	19	330
E12MC	8.10	43.00	22.50	15/16	1 1/4	1 11/16	1.20	14.07	0.63	19	330
E12HC	8.10	43.00	22.50	15/16	1 1/4	1 11/16	1.20	14.07	0.63	19	330
K12HC	10.50	41.00	26.00	7/8	1 1/8	1 11/16	1.20	21.50	0.75	19	340
K12HO	13.40	41.00	26.00	7/8	1 1/8	1 11/16	1.20	21.50	0.75	19	340
H12MC	15.80	47.50	26.60	1	1 1/2	1 11/16	2.23	33.40	0.90	16	410
H12HC	15.80 19.20	47.50 47.50	26.60	1	1 1/2	1 11/16	2.32	33.40	0.90	16 16	410
H12HO J12XHC	19.20	47.50 68.50	26.60 42.50	1 1 3/8	1 1/2 1 1/2	1 11/16 1 15/16	2.32 2.71	33.40 36.70	0.90 0.75	16 16	410 280
J12XHC	13.70	68.50 68.50	42.50	1 3/8	1 1/2	1 15/16	2.71	36.70	0.75	16	280
JIZXHU	19.70	00.50	42.50	I 3/8	I 1/Z	01/01	2.71	30.70	0.75	10	200



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ENGINEERING

STANDARD BOWL ASSEMBLY LIMITATIONS DATA

THRUST DATA MAXIMUM BOWL LATERAL ALLOWABLE WR2 NON-SHOCK (2)EYE SPHERE MODEL FACTOR 1 STG. ADDL. STG. SHAFT (WET) MAX # PRESSURE AREA SIZE MAX. WT. STG. (5) "K" (1) WEIGHT DIA. LBS. OPERATING (4) IN.2 (3) STD. MAX. (6) M14MC 11.90 68.50 42.50 1-1/8 1-7/8 1-15/16 3.50 25.32 0.60 15 310 M14HC 42.50 25.32 15 11.90 68.50 1-1/8 1-7/8 1-15/16 3.62 0.60 310 M14XHC 11.90 68.50 42.50 7/8 1 - 1/21-15/16 3.62 25.32 0.64 15 310 42.50 M14XXHC 11.90 68.50 7/8 1 - 1/21-15/16 3.62 25.32 0.64 14 310 H14LC 53.00 20.80 78.00 1-1/4 1-3/4 2-3/16 38.96 0.92 14 340 4.15 H14MC 78.00 53.00 1-1/4 1-3/4 2-3/16 4.15 38.96 0.92 14 340 20.30 H14MO 78.00 53 00 1-1/4 1-3/4 2-3/16 38.96 14 24.30 4.15 0.92 340 H14XHC 20.30 78.00 53.00 1-1/4 1-3/4 2-3/16 4.52 38.96 0.92 14 340 TBD 58.70 H16MC 90.00 60.00 15/16 2-3/16 12 24.10 9.15 1.05 350 H16XHC 23.50 90.00 60.00 15/16 TBD 2-3/16 9.15 58.70 1.05 12 350 E18LC 29.10 114.00 82.50 5/8 1 2-3/16 9.01 63.88 1.13 13 360 E18HC 28.70 114.00 82.50 5/8 2-3/16 9.26 13 360 1 63.88 1.13 K20LC 33.00 127.50 91.60 1 1-1/4 2-7/16 12.23 72.60 1.50 10 300 K20MC 33.00 127.50 91.60 1 1 - 1/42-7/16 12.23 72.60 1.50 10 330 K20HC 33.00 127.50 91.60 1 1-1/4 2-7/16 12.23 72.60 1.50 10 300 148.30 H24LC 53.80 197.40 1-1/4 1 - 1/22-11/16 148.40 9 280 51.10 1.50 148.30 H24MC 53.60 197.40 1-1/4 9 1-1/2 2-11/16 51.10 148.40 1.50 280 H24XHC 148 30 53.10 197.40 1 - 1/41-1/2 2-11/16 51.10 148.40 1.50 9 280

Continued from prior page

The previous page and this page lists the limitations of National Pump bowl assemblies. These limitations may be varied by changing the design and or materials.

These changes require factory approval and special price quotations. Temperature limits for standard construction = 0 - 180 degrees F. If rubber neoprene bearings are used, the maximum temperature is 150 degrees F.

Footnotes

1. For use in calculating hydraulic thrust.

2. Shaft elongation must not exceed available standard bowl lateral, contact the factory.

3. WR² is in lb. ft. for one stage of the rotating assembly (impeller, collet & shaft). Multiply by the number of stages for WR2 for a complete bowl assembly. Multiply by 144 for WR² in lb. in².

4. Maximum sphere size is the size of the water-passage ways in the pump -- not an indication of the size of solids which the pump can handle. Based on standard lateral and operation from uppermost lateral position.

5. Based on the available lengths of commercial shafting and assembly considerations.

6. Based on the SAE grade 5 standard bolting and ASTM A48 Class 30 material for the bowl walls. Pressure rating must be adjusted for special materials (see chart below). "O" ringed joints are recommended for pressures that exceed 250 PSI, may be lower pressures for some applications.

7. Data for Low NPSH first stage impellers is available. Contact Factory.

Special Material Pressure	Material	304 Stainless	316SS	410SS	Alloy 20	C876 Bronze	Class 45 Cast Iron	Ductile Iron	Ni-Resist	Steel	Zincless (AL-Bronze)
Ratings	Multiplier	2.1	2.3	3.0	2.1	1.3	1.5	2.0	0.8	2.33	2.1

When bowl assemblies or other cast parts are constructed of special material, the above multipliers

must be applied to the standard pressure ratings.

NOTE: When higher pressure applications are needed--than published--and standard materials are

satisfactory, a steel jacket may be fitted around the bowl assembly for an additional presure rating.

This will provide approximately 300% to the standard material construction. Do not use this type of

construction with oil lubricated pumps.

Line Shaft Size	1"	1 3/16"	1 1/4"	1 1/2"	1 11/16"	1 15/16"	2 3/16"	2 7/16"	2 11/16"	2 15/16"
Weight per Foot with Coupling	2.71	3.9	4.2	6.08	7.7	10.22	12.78	15.86	19.8	23.56



STANDARD SHAFT MATERIALS, ALLOWABLE STRESS & CORRECTION FACTORS

				Stress (psi)		Rating
	Material	ASTM	Ultimate	Yield	Allowable	Mutliplier
	416SS	A582 TYPE 416	110,000	85,000	19,800	-
Stock	C-1045	A108 GRADE 1045	90,000	60,000	16,200	0.81
l S	316SS	A276 TYPE 316	75,000	30,000	9,000	0.42
	17-4PH 1150	A564 TYPE 17-4PH CONDITION H1150	135,000	105,000	24,300	1.23
e L	316L	A276 TYPE 316L	70,000	25,000	7,500	0.33
rder	NITRONIC 50	A276 TYPE XM-19	100,000	55,000	16,500	0.83
2	K500	B865 ALLOY 500	140,000	100,000	25,200	1.28
cial	DUPLEX	A276 2205	100,000	75,000	18,000	0.91
be	S.DUPLEX	A479 2507	115,000	80,000	20,700	1.05
S	17-4PH 900	A564 TYPE 17-4PH CONDITION H900	175,000	155,000	31,500	1.61

Note: Rating Multiplier based on thrust listed in table 0.

MECHANICAL FRICTION HORSEPOWER LOSSES PER 100' OF OPEN OR ENCLOSED LINESHAFT

SHAFT DIAMETER (INCHES)		_	ME		H.P. LOSS A	T RPM SHC	OWN		
	3550	2900	2200	1760	1450	1160	970	860	720
1	1.10	.88	.69	.53	.44	.35	.29	.26	.23
1-1/4	1.60	1.33	.96	.79	.67	.48	.44	.38	.31
1-1/2	2.20	1.85	1.42	1.14	.96	<u>.</u> 74	.62	.56	<u>.</u> 47
1-11/16	2.80	2.33	1.68	1.40	1.18	.94	.78	.70	.59
1-15/16	_	_	—	1.83	1.55	1.20	1.00	.90	.76
2-3/16	_	_	—	2.30	2.00	1.50	1.30	1.20	1.00
2-7/16	_	4.83	3.66	2.92	2.40	1.90	1.60	1.40	1.19
2-11/16	_	5.38	4.08	3.27	2.70	2.10	1.81	1.60	1.31
2-15/16	_	6.59	5.00	4.00	3.30	2.60	2.21	1.90	1.60





THREADED SHAFT QUICK REFERENCE POWER RATING CHART – 416SS

	Thread				00.11	0	()		50.11	- O	(
Shaft	Minor				60 Hz	z Speeds	(rpm)		50 Hz	z Speeds	(rpm)
Diameter	Diameter	Thrust	hp/100 rpm								
(in)	(in)	(lb)		3600	1800	1200	900	720	3000	1500	1000
1.00	0.8773	5000	4.1	147	73	49	37	29	122	61	41
1.19	1.0648	7500	7.3	262	131	87	65	52	218	109	73
1.25	1.1273	10000	8.5	308	154	103	77	62	256	128	85
1.50	1.3773	12500	15.7	567	283	189	142	113	472	236	157
1.69	1.5648	15000	23.2	834	417	278	209	167	695	348	232
1.94	1.8148	20000	36.2	1302	651	434	325	260	1085	542	362
2.19	2.0648	27000	53.2		957	638	478	383		797	532
2.44	2.3148	30000	75.3		1355	903	677	542		1129	753
2.69	2.5700	33000	103.3		1860	1240	930	744		1550	1033
2.94	2.8200	36000	136.9		2463	1642	1232	985		2053	1369
Maximum	Allowable S	Stress =	19,800	psi							

THREADED SHAFT QUICK REFERENCE POWER RATING CHART – C-1045

Shaft	Thread Minor				60 H .	z Speeds	(rnm)		50 H	z Speeds	(mm)
Diameter	Diameter	Thrust	hp/100 rpm		00112	- Opecus	(ipiii)		00112		(ipiii)
(in)	(in)	(lb)		3600	1800	1200	900	720	3000	1500	1000
1.00	0.8773	5000	3.3	119	59	40	30	24	99	49	33
1.19	1.0648	7500	5.9	212	106	71	53	42	176	88	59
1.25	1.1273	10000	6.9	248	124	83	62	50	206	103	69
1.50	1.3773	12500	12.7	458	229	153	115	92	382	191	127
1.69	1.5648	15000	18.8	676	338	225	169	135	563	282	188
1.94	1.8148	20000	29.3	1055	527	352	264	211	879	439	293
2.19	2.0648	27000	43.0		775	516	387	310		645	430
2.44	2.3148	30000	61.1		1099	733	550	440		916	611
2.69	2.5700	33000	84.0		1512	1008	756	605		1260	840
2.94	2.8200	36000	111.4		2005	1336	1002	802		1671	1114
Maximum	Allowable S	Stress =	16,200	psi							

The above ratings are based on the following formula:

$$P = \frac{ND^{3}}{321,000} \left[S^{2} - \left(\frac{2F}{\pi D^{2}} \right)^{2} \right]^{1/2}$$

P = Power transmitted (in horsepower)

N = RPM

D = Shaft diameter (at root of threads)

S = Combined allowable shear stress (psi)*

F = Axial thrust

*S shall not exceed 30% of elastic limit or 18% of ultimate tensile strength of shafting.

THRUST BEARING HORSEPOWER LOSS

H.P. LOSS = <u>0.0075 X RPM</u> X <u>TOTAL DOWNTHRUST (LBS.</u>) 100 1000



COLUMN FRICTION LOSS CHART 50 - 1400 GPM

LOSS IN FEET OF HEAD PER 100 FEET OF COLUMN OPEN OR ENCLOSED LINESHAFT

COL. SIZE	SHAFT SIZE						C	APACIT	'Y IN GA	ALLONS	S PER I	MINUTE					
		50	60	70	80	90	100	125	150	175	200	225	250	275	300	325	350
4	1 1-1/4	.9 1.6	1.2 2.2	1.5 2.9	1.9 3.6	2.4 4.4	2.8 5.3	4.2 7.7	5.7 10.5	7.5 13.5	9.5	11.5	14.0				
5	1 1-1/4 1-1/2 - 1-11/16					1.0	.9 1.2	1.0 1.4 1.8	1.3 1.9 2.5	1.7 2.5 3.2	2.2 3.1 4.0	2.7 3.9 5.0	3.3 4.6 6.0	3.9 5.5 7.1	4.5 6.4 8.3	5.2 7.2	5.9 8.3
6	1 1-1/4 1-1/2 - 1-11/16 1-15/16							.9	.9 1.3	1.1 1.7	1.0 1.4 2.2	.9 1.2 1.7 2.7	1.1 1.4 2.0 3.3	1.3 1.7 2.4 3.9	1.5 2.0 2.8 4.5	1.7 2.3 3.2 5.2	2.0 2.6 3.6 6.0

COL. SIZE	SHAFT SIZE						CA	PACITY	IN GA		6 PER	MINUT	E				
		375	400	450	500	550	600	650	700	750	800	900	1000	1100	1200	1300	1400
5	1 1-1/4	6.6 9.4	7.5 10.5	9.3	11.2												
6	1 1-1/4 1-1/2 - 1-11/16 1-15/16	2.2 2.9 4.1 6.7	2.5 3.3 4.6 7.5	3.1 4.1 5.7 9.3	3.7 4.9 6.9 11.5	4.4 5.8 8.1	5.2 6.8 9.5	6.0 7.8 11.0	6.8 9.0	7.7 10.1	8.6	10.7					
8	1 1-1/4 1-1/2 - 1-11/16 1-15/16 2-3/16 - 2-7/16	.9 1.3	1.0 1.5	.9 1.2 1.8	.9 1.1 1.5 2.2	1.1 1.3 1.8 2.6	1.0 1.3 1.5 2.1 3.0	1.2 1.5 1.8 2.4 3.5	1.4 1.7 2.0 2.8 4.1	1.7 1.9 2.3 3.2 4.6	2.0 2.2 2.6 3.6 5.2	2.5 2.7 3.2 4.5 6.4	3.0 3.2 3.9 5.4 7.8	3.5 3.8 4.6 6.4 9.4	4.2 4.5 5.4 7.5	4.8 5.2 6.2 8.8	5.5 6.0 7.2 10.0
10	1 1-1/4 1-1/2 - 1-11/16 1-15/16 2-3/16 - 2-7/16 2-11/16								1.0	1.1	.9 1.3	1.0 1.2 1.6	1.0 1.2 1.4 1.9	1.0 1.2 1.4 1.7 2.2	1.1 1.2 1.4 1.6 2.0 2.6	1.2 1.4 1.6 1.9 2.3 3.0	1.4 1.6 1.8 2.2 2.7 3.5

Maximum friction loss as recommended by A.W.W.A. is 5' per 100' of column.



COLUMN FRICTION LOSS CHART 1,500 - 12,000 GPM

LOSS IN FEET OF HEAD PER 100 FEET OF COLUMN OPEN OR ENCLOSED LINESHAFT

COL. SIZE	SHAFT SIZE							CAP	ACITY	N GAL	LONSI	PER MI	NUTE						
		1500	1600	1800	2000	2200	2400	2600	2800	3000	3200	3400	3600	3800	4000	4250	4500	4750	5000
8	1 1-1/4	6.2 6.8	6.9 7.6	8.6 9.4	10.5 11.4														
10	1 1-1/4 1-1/2 - 1-11/16 1-15/16 2-3/16 - 2-7/16 2-11/16	1.6 1.8 2.0 2.5 3.0 3.9	1.8 2.0 2.3 2.8 3.4 4.5	2.2 2.5 2.8 3.4 4.3 5.5	2.7 3.0 3.5 4.2 5.2 6.7	3.2 3.6 4.1 5.0 6.1 7.9	3.7 4.2 4.8 5.8 7.2 9.3	4.3 4.9 5.6 6.8 8.2	5.0 5.6 6.4 7.8 9.4	5.6 6.4 7.2 8.9	6.3 7.1 8.2 10.0	7.0 8.0 9.1	7.8 8.9	8.7 9.8	9.6				
12	1-1/4 1-1/2 - 1-11/16 1-15/16 2-3/16 - 2-7/16 2-11/16	.9 1.1 1.3	.9 1.0 1.2 1.4	1.0 1.1 1.3 1.5 1.8	1.2 1.4 1.6 1.8 2.1	1.4 1.6 1.9 2.1 2.5	1.7 1.9 2.2 2.5 3.0	1.9 2.2 2.5 2.9 3.5	2.2 2.5 2.9 3.3 4.0	2.5 2.9 3.3 3.8 4.5	2.8 3.2 3.7 4.3 5.1	3.1 3.6 4.1 4.8 5.7	3.5 4.0 4.6 5.4 6.4	3.9 4.4 5.1 5.9 7.1	4.2 4.8 5.6 6.5 7.8	4.8 5.3 6.3 7.2 8.8	5.3 6.0 7.0 8.0 9.9	5.8 6.6 7.8 8.8	6.4 7.3 8.5 9.7
14	1-1/2 - 1-11/16 1-15/16 2-3/16 - 2-7/16 2-11/16 2-15/16	.9	1.0	.9 1.1	.9 1.0 1.4	.9 1.1 1.2 1.6	1.0 1.1 1.3 1.4 1.9	1.2 1.3 1.5 1.7 2.2	1.3 1.5 1.7 2.0 2.5	1.5 1.7 2.0 2.2 2.9	1.7 1.9 2.2 2.5 3.2	1.9 2.1 2.4 2.7 3.6	2.1 2.4 2.7 3.1 4.0	2.3 2.6 3.0 3.4 4.4	2.6 2.9 3.3 3.8 4.9	2.9 3.2 3.7 4.2 5.4	3.2 3.5 4.0 4.6 5.9	3.6 3.9 4.4 5.0 6.7	4.0 4.3 4.9 5.5 7.2
16	1-1/2 - 1-11/16 1-15/16 2-3/16 - 2-7/16 2-11/16 2-15/16							.9	<u>.9</u> 1.0	.9 1.0 1.1	.9 1.0 1.1 1.3	1.0 1.1 1.1 1.2 1.4	1.1 1.2 1.3 1.4 1.6	1.2 1.3 1.4 1.5 1.8	1.3 1.4 1.5 1.6 1.9	1.4 1.6 1.7 1.8 2.1	1.6 1.7 1.9 2.0 2.4	1.8 1.9 2.1 2.2 2.7	1.9 2.1 2.3 2.5 2.9

COL. SIZE	SHAFT SIZE							CAP	ACITY I	N GAL	LONS	PER MI	NUTE					
		4500	4750	5000	5500	6000	6500	7000	7500	8000	8500	9000	9500	10000	11000	12000		
14	1-1/2 - 1-11/16 1-15/16 2-3/16 - 2-7/16 2-11/16 2-15/16	3.2 3.5 4.0 4.6 5.9	3.6 3.9 4.4 5.0 6.7	4.0 4.3 4.9 5.5	4.7 5.1 5.8 6.7	5.6 6.0 6.9 8.0	7.0 8.0	7.4 8.0 9.2	8.5	9.7								
16	1-1/2 - 1-11/16 1-15/16 2-3/16 - 2-7/16 2-11/16 2-15/16	1.6 1.7 1.9 2.0 2.4	1.8 1.9 2.1 2.2 2.7	1.9 2.1 2.3 2.5 2.9	2.3 2.5 2.7 2.9 3.5	2.6 3.0 3.3 3.5 4.1	3.4 3.8	3.6 3.8 4.4 4.6 5.4	4.1 4.3 5.0 5.3 6.1	4.6 4.8 5.6 5.9 6.8	6.3 6.5	5.8 6.0 7.0 7.3 8.3	6.4 6.6 7.7 8.0 9.0	7.1 7.2 8.5 8.8	7.8 7.9	8.6		

Maximum friction loss as recommended by A.W.W.A. is 5' per 100' of column.



DISCHARGE HEAD FRICTION LOSS CHART

DISCHARGE SIZE					CA	PACITY	IN GALL	ONS PE	R MINUTE	I				
	100	125	150	175	200	250	300	350	400	450	500	550		
3	.25	.38	.55	.75	1.0	1.5	2.2	3.0						
4		.12	.18	.24	.32	.49	.70	.97	1.2	1.5	1.9	2.3		
6		.37												
		CAPACITY IN GALLONS PER MINUTE												
	600	800	1000	1250	1500	1750	2000	2500	3000	3500	4000	4500	5000	
6	.54	.96	1.5	2.4	3.4									
8	.17	.31	<u>.</u> 47	<u>.</u> 74	1 <u>.</u> 1	1.5	2.0	3.0						
10			.19	.30	.43	.59	.77	1.2	1.7	2.4	3.0			
12					<u>.</u> 21	.29	.37	.58	.85	1.2	1.5	1.9	2.3	
14							.20	.31	.45	.65	.80	1.0	1.2	

CAST DISCHARGE HEADS

FABRICATED DISCHARGE HEADS

DISCHARGE SIZE					CAPAC	CITY IN GA	ALLONS F	PER MINU	TE					
	100	125	150	175	200	250	300	350	400	450	500	600		
3	.36	.57	.82	1.1	1.5	2.3	3.2							
4	.12	.19	.27	.38	.50	.79	1.1	1.5	2.0	2.5				
5					.20	.31	.45	.61	.80	1.0	1.2	1.9		
6											.60	.86		
8											.20	.29		
		CAPACITY IN GALLONS PER MINUTE												
	800	1000	1250	1500	1750	2000	2500	3000	3500	4000	4500	5000		
5	3.1													
6	1.5	2.4												
8	.51	.78	1.2	1.8	2.3	3.2								
10	.20	.31	.48	.69	.95	1.2	1.9	2.8						
12		.16	.24	.34	.48	.61	.96	1.4	1.9	2.4	3.0			
14			.16	.23	.31	.41	.63	.92	1.3	1.6	2.1	2.5		



FRICTION LOSS OF WATER IN FEET PER 100 FEET LENGTH OF PIPE, BASED ON WILLIAMS & HAZEN FORMULA USING CONSTANT 100 SIZES OF STANDARD PIPE IN INCHES.

U.S.	1/2"P	ipe	3/4"	Pipe	1"Pi	pe	1-1/4	"Pipe	1-1/2"F	Pipe	2"P	ipe	2-1/2	'Pipe	3"	Pipe	4"P	ipe	5"F	Pipe	6"	Pipe	U.S.
Gals. per	Vel.	Loss	Vel.	Loss	Vel.	Loss in	Vel.	Loss in	Vel.	Loss	Vel.	Loss	Vel.	Loss	Vel.	Loss	Vel.	Loss	Vel.	Loss	Vel.	Loss	Gals. per
Minute 2 4 6 8 10	Et/Sec. 2.10 4.21 6.31 8.42 10.52	Feet 7 4 27.0 57.0 98.0 147.0	Ft/Sec. 1.20 2.41 3.61 4.81 6.02	Feet 1.9 7.0 14.7 25.0 38.0	Ft/Sec. 1.49 2.23 2.98 3.72	Feet 2.14 4.55 7.8 11.7	86 1.29 1.72 2.14	.57 1.20 2.03 3.05	63 94 1.26 1.57	Feet .26 .56 .95 1.43	.61 .82 1.02	Feet .20 .33 .60	Ft./Sec .52 .65	.11 .17	Ft/Sec	Feet 0.07	Ft./Sec	Feet	Ft/Sec	Feet	Ft./Sec	Feet	Minute 2 4 6 8 10
12 15 18 20 25 30 35			7.22 9.02 10.84 12.03	53.0 80.0 108.2 136.0	4.46 5.60 6.69 7.44 9.30 11.15 13.02	16.4 25.0 35.0 42.0 64.0 89.0 119.0	2.57 3.21 3.86 4.29 5.36 6.43 7.51	4.3 6.5 9.1 11.1 16.6 23.0 31.2	1.89 2.36 2.83 3.15 3.80 4.72 5.51	2.01 3.00 4.24 5.20 7.30 11.0 14.7	1.23 1.53 1.84 2.04 2.55 3.06 3.57	79 1.08 1.49 1.82 2.73 3.84 5.10	78 98 1.18 1.31 1.63 1.96 2.29	.23 .36 .50 .61 .92 1.29 1.72	.54 .68 .82 .91 1.13 1.36 1.59	10 15 21 25 38 54 71	.51 .64 .77 .89	.06 .09 .13 .17	.49 .57	.04 .06			12 15 18 20 25 30 35
40 45 50 55 60 65					14.88	152.0	8.58 9.65 10.72 11.78 12.87 13.92	40.0 50.0 60.0 72.0 85.0 99.7	6.30 7.08 7.87 8.66 9.44 10.23	18.8 23.2 28.4 34.0 39.6 45.9	4.08 4.60 5.11 5.62 6.13 6.64	6.6 8.2 9.9 11.8 13.9 16.1	2.61 2.94 3.27 3.69 3.92 4.24	2.20 2.80 3.32 4.01 4.65 5.4	1.82 2.04 2.27 2.45 2.72 2.89	.91 1.15 1.38 1.58 1.92 2.16	1.02 1.15 1.28 1.41 1.53 1.66	22 28 34 41 47 53	.65 .73 .82 .90 .98 1.06	.08 .09 .11 .14 .16 .19	.57 .62 .68 .74	.04 .05 .06 .076	40 45 50 55 60 65
70 75 80 85 90 95							15.01 16.06 17.16 18.21 19.30	113.0 129.0 145.0 163.8 180.0	11.02 11.80 12.59 13.38 14.71 14.95	53.0 60.0 68.0 75.0 84.0 93.0	7.15 7.66 8.17 8.68 9.19 9.70	18.4 20.9 23.7 26.5 29.4 32.6	4.58 4.91 5.23 5.56 5.88 6.21	6.2 7.1 7.9 8.1 9.8 10.8	3.18 3.33 3.63 3.78 4.09 4.22	2.57 3.00 3.28 3.54 4.08 4.33	1.79 1.91 2.04 2.17 2.30 2.42	.63 .73 .81 .91 1.00 1.12	1.14 1.22 1.31 1.39 1.47 1.55	.21 .24 .27 .31 .34 .38	79 85 91 96 1.02 1.08	08 10 11 12 14 15	70 75 80 85 90 95
100 110 120 130 140 150	8"PI .90 .96	.08 .09							15.74 17.31 18.89 20.46 22.04	102.0 122.0 143.0 166.0 190.0	10.21 11.23 12.25 13.28 14.30 15.32	35.8 42.9 50.0 58.0 67.0 76.0	6.54 7.18 7.84 8.48 9.15 9.81	12.0 14.5 16.8 18.7 22.3 25.6	4.54 5.00 5.45 5.91 6.35 6.82	4.96 6.0 7.0 8.1 9.2 10.5	2.55 2.81 3.06 3.31 3.57 3.82	1.22 1.46 1.17 1.97 2.28 2.62	1.63 1.79 1.96 2.12 2.29 2.45	41 49 58 67 76 88	1.13 1.25 1.36 1.47 1.59 1.70	.17 .21 .24 .27 .32 .36	100 110 120 130 140 150
160 170 180 190 200 220	1.02 1.06 1.15 1.21 1.28 1.40	.10 .11 .13 .14 .15 .18	10"P .90	.06							16.34 17.36 18.38 19.40 20.42 22.47	86.0 96.0 107.0 118.0 129.0 154.0	10.46 11.11 11.76 12.42 13.07 14.38	29.0 34.1 35.7 39.6 43.1 52.0	7.26 7.71 8.17 8.63 9.08 9.99	11.8 13.3 14.0 15.5 17.8 21.3	4.08 4.33 4.60 4.84 5.11 5.62	2.91 3.26 3.61 4.01 4.4 5.2	2.61 2.77 2.94 3.10 3.27 3.59	.98 1.08 1.22 1.35 1.48 1.77	1.82 1.92 2.04 2.16 2.27 2.50	.40 .45 .50 .66 .62 .73	160 170 180 190 200 220
240 260 280 300 320 340	1.53 1.66 1.79 1.91 2.05 2.18	.22 .25 .28 .32 .37 .41	.96 1.06 1.15 1.22 1.31 1.39	07 08 09 11 12 14	12"F	PIPE					24.51 26.55	182.0 211.0	15.69 16.99 18.30 19.61 20.92 22.22	61.0 70.0 81.0 92.0 103.0 116.0	10.89 11.80 12.71 13.62 14.52 15.43	25.1 29.1 33.4 38.0 42.8 47.9	6.13 6.64 7.15 7.66 8.17 8.68	6.2 7.2 8.2 9.3 10.5 11.7	3.92 4.25 4.58 4.90 5.23 5.54	2.08 2.41 2.77 3.14 3.54 3.97	2.72 2.95 3.18 3.40 3.64 3.84	.87 1.00 1.14 1.32 1.47 1.62	240 260 280 300 320 340
360 380 400 450 500 550	2.30 2.43 2.60 2.92 3.19 3.52	.45 .50 .54 .68 .82 .97	1.47 1.55 1.63 1.84 2.04 2.24	15 17 19 23 28 33	1.08 1.14 1.28 1.42 1.56	069 075 96 113 136	14" 1.04 1.15	.06 .07					23.53 24.84 26.14	128.0 142.0 156.0	16.34 17.25 18.16 20.40 22.70 24.96	53.0 59.0 65.0 78.0 98.0 117.0	9.19 9.69 10.21 11.49 12.77 14.04	13.1 14.0 16.0 19.8 24.0 28.7	5.87 6.19 6.54 7.35 8.17 8.99	4.41 4.86 5.4 6.7 8.1 9.6	4.08 4.31 4.55 5.11 5.68 6.25	1.83 2.00 2.20 2.74 2.90 3.96	360 380 400 450 500 550
600 650 700 750 800 850	3.84 4.16 4.46 4.80 5.10 5.48	1.14 1.34 1.54 1.74 1.90 2.20	2.45 2.65 2.86 3.06 3.26 3.47	39 45 52 59 66 75	1.70 1.84 1.99 2.13 2.27 2.41	.159 .19 .22 .24 .27 .31	1.25 1.37 1.46 1.58 1.67 1.79	.08 .09 .10 .11 .13 .14	16"F	PIPE	20"	PIPE			27.23	137.0	15.32 16.59 17.87 19.15 20.42 21.70	33.7 39.0 44.9 51.0 57.0 64.0	9.80 10.62 11.44 12.26 13.07 13.89	11.3 13.2 15.1 17.2 19.4 21.7	6.81 7.38 7.95 8.50 9.08 9.65	4.65 5.40 6.21 7.12 7.96 8.95	600 650 700 750 800 850
900 950 1000 1100 1200 1300	5.75 6.06 6.38 7.03 7.66 8.30	2.46 2.87 2.97 3.52 4.17 4.85	3.67 3.88 4.08 4.49 4.90 5.31	.83 .91 1.03 1.19 1.40 1.62	2.56 2.70 2.84 3.13 3.41 3.69	.34 .38 .41 .49 .58 .67	1.88 2.00 2.10 2.31 2.52 2.71	.16 .18 .19 .23 .27 .32	1.44 1.52 1.60 1.76 1.92 2.08	.084 .095 .10 .12 .14 .17	1.02 1.12 1.23 1.33	.04 .04 .05 .06	24"	PIPE			22.98	71	14.71 15.52 16.34 17.97 19.61	24.0 26.7 29.2 34.9 40.9	10.20 10.77 11.34 12.48 13.61 14.72	10.11 11.20 12.04 14.55 17.10 18.40	900 950 1000 1100 1200 1300
1400 1500 1600 1800 2000 2200	8.95 9.58 10.21 11.50 12.78 14.05	5.50 6.24 7.00 8.78 10.71 12.78	5.71 6.12 6.53 7.35 8.16 8.98	1.87 2.13 2.39 2.96 3.59 4.24	3.98 4.26 4.55 5.11 5.68 6.25	.78 .89 .98 1.21 1.49 1.81	2.92 3.15 3.34 3.75 4.17 4.59	.36 .41 .47 .58 .71 .84	2.24 2.39 2.56 2.87 3.19 3.51	.19 .21 .24 .30 .37 .44	1.43 1.53 1.63 1.84 2.04 2.25	.064 .07 .08 .10 .12 .15	1.28 1.42 1.56	.04 .05 .06	30"F	PIPE					15.90 17.02 18.10	22.60 25.60 26.90	1400 1500 1600 1800 2000 2200
2400 2600 2800 3000 3200 3500	15.32	14.2	9.80 10.61 11.41 12.24 13.05 14.30	5.04 5.81 6.70 7.62 7.80 10.06	6.81 7.38 7.95 8.52 9.10 9.95	2.08 2.43 2.75 3.15 3.51 4.16	5.00 5.47 5.84 6.01 6.68 7.30	.99 1.17 1.32 1.49 1.67 1.97	3.83 4.15 4.47 4.79 5.12 5.59	.52 .60 .68 .78 .88 1.04	2.45 2.66 2.86 3.08 3.27 3.59	.17 .20 .23 .27 .30 .35	1.70 1.84 1.98 2.13 2.26 2.49	.07 08 .09 10 .12 .14	1.09 1.16 1.27 1.37 1.46 1.56	.02 .027 .03 .037 .041 .047							2400 2600 2800 3000 3200 3500
3800 4200 4500 5000 5500 6000			15.51	13.4	10.80 11.92 12.78 14.20	4.90 5.88 6.90 8.40	7.98 8.76 9.46 10.50 11.55 12.60	2.36 2.77 3.22 3.92 4.65 5.50	6.07 6.70 7.18 8.01 8.78 9.68	1.20 1.44 1.64 2.03 2.39 2.79	3.88 4.29 4.60 5.13 5.64 6.13	.41 .49 .56 .68 .82 .94	2.69 2.99 3.20 3.54 3.90 4.25	.17 .20 .22 .27 .33 .38	1.73 1.91 2.04 2.26 2.50 2.73	.05 .07 .08 .09 .11 .13							3800 4200 4500 5000 5500 6000
6500 7000 8000 9000 10000 12000							13.65 14.60	6.45 7.08	10.39 11.18 12.78 14.37 15.96	3.32 3.70 4.74 5.90 7.19	6.64 7.15 8.17 9.20 10.20 12.25	1.10 1.25 1.61 2.01 2.44 3.41	4.61 4.97 5.68 6.35 7.07 8.60	.45 .52 .66 .81 .98 1.40	2.96 3.18 3.64 4.08 4.54 5.46	15 17 23 28 33 48							6500 7000 8000 9000 10000 12000
14000 16000 18000											14.30	4.54	9.95 11.38 12.76 14.20	1.87 2.40 2.97	6.37 7.28 8.18	.63 .81 1.02							14000 16000 18000



ENGINEERING

SHAFT ELONGATION INCHES PER 100 FT. OF SHAFT

HYDRAULIC					SHAFT D	IAMETER				
THRUST LBS.	3/4	1	1-1/4	1-1/2	1-11/16	1-15/16	2-3/16	2-7/16	2-11/16	2-15/16
400	0.037	0.021	0.013	0.009	0.007					
600	0.056	0.032	0.020	0.014	0.011	0.008				
800	0.075	0.042	0.027	0.019	0.015	0.011	0.009			
1000	0.094	0.053	0.034	0.023	0.019	0.014	0.011	0.009		
1200	0.112	0.063	0.041	0.028	0.022	0.017	0.013	0.011	0.009	
1400	0.131	0.074	0.047	0.033	0.026	0.020	0.015	0.012	0.010	0.009
1600	0.150	0.084	0.054	0.035	0.030	0.022	0.018	0.014	0.012	0.010
1800	0.169	0.095	0.061	0.042	0.033	0.025	0.020	0.016	0.013	0.011
2000	0.187	0.105	0.067	0.047	0.037	0.028	0.022	0.018	0.015	0.012
2400	0.225	0.127	0.081	0.056	0.044	0.034	0.026	0.021	0.018	0.015
2800	0.262	0.148	0.094	0.066	0.052	0.039	0.031	0.025	0.020	0.017
3200	0.300	0.169	0.108	0.075	0.059	0.045	0.035	0.028	0.023	0.020
3600		0.190	0.121	0.084	0.067	0.050	0.040	0.032	0.026	0.022
4000		0.211	0.135	0.094	0.074	0.056	0.044	0.036	0.029	0.024
4400		0.232	0.148	0.103	0.081	0.062	0.048	0.039	0.032	0.027
4800		0.253	0.162	0.112	0.089	0.067	0.053	0.043	0.035	0.029
5200		0.274	0.175	0.122	0.096	0.073	0.057	0.046	0.038	0.032
5600		0.295	0.189	0.131	0.104	0.079	0.062	0.050	0.041	0.034
6000			0.202	0.141	0.111	0.084	0.066	0.053	0.044	0.037
6500			0.219	0.152	0.120	0.091	0.072	0.058	0.047	0.040
7000			0.236	0.164	0.130	0.098	0.077	0.062	0.051	0.043
7500			0.253	0.176	0.139	0.105	0.083	0.067	0.055	0.046
8000			0.270	0.187	0.148	0.112	0.088	0.071	0.058	0.049
9000			0.303	0.211	0.167	0.126	0.099	0.080	0.066	0.055
10000				0.234	0.185	0.140	0.110	0.089	0.073	0.061
12000				0.281	0.222	0.168	0.132	0.106	0.088	0.073
14000				0.328	0.259	0.197	0.154	0.124	0.102	0.085
16000					0.296	0.225	0.176	0.142	0.117	0.098
18000					0.333	0.253	0.198	0.160	0.131	0.110
20000						0.281	0.220	0.177	0.146	0.122
22000						0.309	0.242	0.195	0.161	0.134
24000							0.264	0.213	0.175	0.147
26000							0.286	0.231	0.190	0.159
28000							0.308	0.248	0.204	0.171
30000								0.266	0.219	0.183

Shaft elongation is caused by both hydraulic thrust produced by the pump and static weight of the rotating pump elements. Once the static weight has been compensated for by lifting the impellers off of the bottom of the bowls, only the hydraulic thrust remains a factor. The shaft lateral available in the bowls must be sufficient enough to allow for the shaft elongation produced by the hydraulic thrust when pump is in operation. This is to prevent the impellers from rubbing on the bottom of the bowls. The impellers must be raised off the bottom of the bowls to allow for this stretch plus the proper running clearances.

 $e = \frac{1 \times HT}{E \times A}$

e = Shaft Elongation, (in.) 1 = Shaft Length, (in.) E = Modulus of elasticity (29 x 10⁶ lbs./in.²) HT = Hydraulic Thrust (lbs.) A = Shaft Area (in.²)



COLUMN ELONGATION

INCHES PER 100 FT. OF COLUMN

(FOR OPEN LINESHAFT COLUMN MULTIPLY VALUES BY 1.3)

COLUMN DIAMETER Standard pipe, nominal I.D. except as indicated by * HYDRAULIC													
HYDRAULIC THRUST LBS.	3"	4"	5"	6"	8"	10"	12"	14"*	16"*				
500	.007	.005	.004	.003									
600	.008	.006	.005	.004									
800	.011	.008	.006	.005									
1000	.013	.010	.008	.006	.004								
1200	.016	.012	.009	.007	.005								
1400	.019	.014	.011	.008	.006								
1600	.021	.016	.012	.009	.007	.005							
1800	.024	.018	.014	.011	.008	.006							
2000	.027	.020	.015	.012	.009	.007							
2400	.032	.023	.019	.014	.010	.008	.006						
2800	.037	.027	.022	.016	.012	.010	.007						
3200	.043	.031	.025	.019	.014	.011	.008						
3600	.048	.035	.028	.021	.016	.012	.009	.008					
4000		.039	.031	.023	.017	.014	.010	.008					
4400		.043	.034	.026	.019	.015	.0110	.009					
4800		.047	.037	.028	.021	.016	.013	.010	.009				
5200		.051	.040	.030	.023	.018	.014	.011	.010				
5600		.055	.043	.033	.024	.019	.015	.012	.011				
6000			.046	.035	.026	.020	.016	.013	.011				
6500			.050	.038	.028	.022	.017	.014	.012				
7000			.054	.041	.030	.024	.018	.015	.013				
7500			.058	.044	.033	.025	.020	.016	.014				
8000			.062	.047	.035	.027	.021	.017	.015				
9000				.053	.039	.030	.023	.019	.017				
10,000				.059	.043	.034	.026	.021	.019				
12,000				.070	.052	.041	.031	.025	.023				
14,000				.082	.061	.048	.036	.029	.026				
16,000				.094	.070	.054	.042	.034	.030				
18,000					.078	.061	.047	.038	.034				
20,000					.087	.068	.052	.042	.037				
22,000					.096	.075	.057	.046	.041				
24,000					.104	.082	.063	.050	.045				
26,000					.113	.088	.068	.055	.049				
28,000						.095	.073	.059	.052				
30,000						.102	.078	.063	.056				
32,000						.109	.083	.067	.060				
34,000						.115	.089	.071	.064				
36,000						.122	.094	.076	.068				
38,000						.129	.099	.080	.071				
40,000						.126	.104	.084	.075				

Downthrust due to the hydraulic thrust of the pump causes the shaft and column to stretch after the pump is in operation. Unless the impellers can be and are raised off the bottom of the bowls enough to allow for this stretch plus some running clearance, the impellers will drag, causing the pump to wear and increase the horsepower required. With the total hydraulic downthrust known and the Column Elongation determined from this Chart, the total stretch of the column tube for the setting in question can be determined. To find the NET elongation, subtract from Column Elongation the Shaft Elongation.



MAXIMUM ALLOWABLE BEARING SPACING (INCHES)

OPEN LINESHAFT CONSTRUCTION

SHAFT SIZE	1	NON RUBBER BEARINGS										
	RPM (60 CYCLES) RPM (50 CYCLES)											
	3600	1800	1200	900	720	3000	1500	1000	750	600		
1"	30	40	40	60	60	30	40	60	60	60		
1-1/4"	30	60	60	60	60	40	40	60	60	60		
1-1/2" - 2-3/16"	40	60	60	60	60	40	60	60	60	60		
2-7/16" - 2-11/16"		60	60	60	60		60	60	60	120		

OPEN LINESHAFT CONSTRUCTION

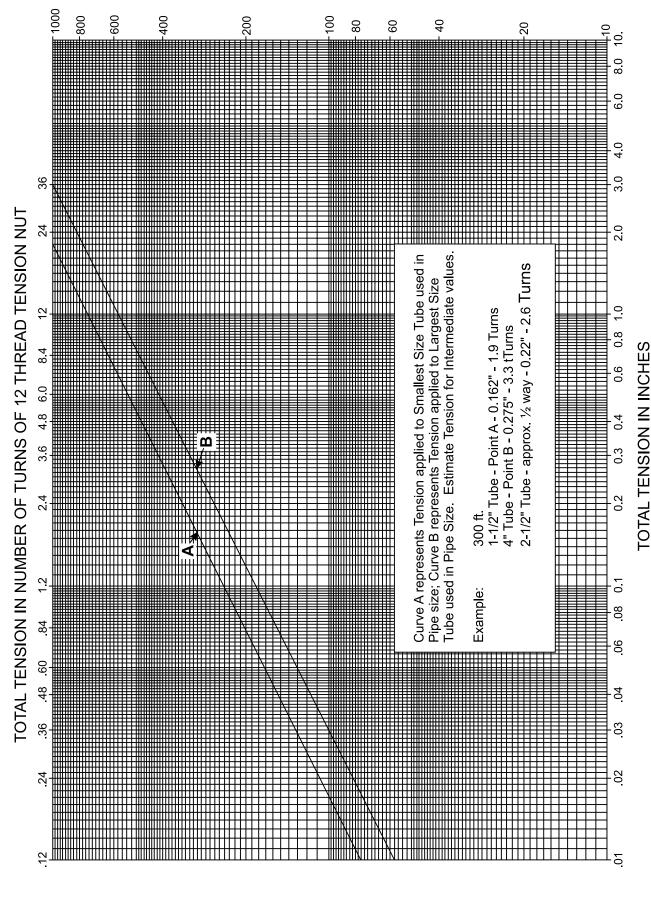
SHAFT SIZE	1)		RI	JBBER I	BEARIN	GS				
	RPM (60 CYCLES) RPM (50 CYCLES)										
	3600	1800	1200	900	720	3000	1500	1000	750	600	
1"	60	120	120	120	120	60	60	120	120	120	
1-1/4"	60	120	120	120	120	60	60	120	120	120	
1-1/2" - 2-3/16"	60	120	120	120	120	60	120	120	120	120	
2-7/16" - 2-11/16"		120	120	120	120	60	120	120	120	120	

ENCLOSED LINESHAFT CONSTRUCTION

SHAFT SIZE	(1)		NON	RUBBE	R BEAR	INGS			
	RPM (60 CYCLES) RPM (50 CYCLES)									
	3600	1800	1200	900	720	3000	1500	1000	750	600
1"	30	40	40	60	60	30	40	60	60	60
1-1/4"	30	40	60	60	60	40	40	60	60	60
1-1/2" - 2-3/16"	40	60	60	60	60	40	60	60	60	60
2-7/16" - 2-11/16"		60	60	60	60		60	60	60	120

(1) FOR SPECIFIC APPLICATIONS THAT MAY DIFFER FROM THE ABOVE, CONTACT FACTORY. DIMENSIONS LISTED ABOVE ARE TO BEARING CENTERS.





TUBING TENSION



NGINEERING

TOTAL SETTING IN FEET

PUMP LINESHAFT ELONGATION

Pump lineshaft elongation is caused by the weight of the shaft and the hydraulic thrust of the pump. Weight stretch is compensated for by field adjustment. Hydraulic thrust elongation must be calculated and allowed for in the shaft lateral adjustment. HYDRAULIC ELONGATION ALLOWANCE BEGINS ONLY AFTER THE WEIGHT STRETCH HAS BEEN ADJUSTED. The weight adjustment is accomplished by turning the motor shaft nut until the shaft starts to turn freely.

SHAFT HYDRAULIC ELONGATION EXAMPLE

M9MC, 14 Stage Bowl Assembly

500 foot setting of 6" x 2" x 1-1/4" column, tube and shaft, 400 GPM, 550 feet of head

FROM CATALOG CHART......FOR EXACT CALCULATION

SHAFT ELONGATION Hydraulic Thrust = K factor X TDH From Catalog page 33, K = 5.1 $5.1 \times 550 = 2,805$ Lbs. From Page 41, 2,800 Lb. thrust with 1-1/4" shaft Elongation = 0.094" per 100 ft. of setting $\frac{500}{100}$ X 0.094 = 0.470" $\frac{F \times L \times 12}{29 \times 10^{6} \times A}$ F = HYDRAULIC FORCE L = SHAFT LENGTH A = SHAFT CROSS SECTION AREA IN.² $\frac{2,805 \times 500 \times 12}{29 \times 10^{6} \times 1.23} = 0.472"$

FROM CATALOG CHART......FOR EXACT CALCULATION

COLUMN AND TUBE ELONGATION The total column thrust = pipe I.D. area x $\frac{\text{TDH}}{2.31}$ minus impeller wear ring area Hydraulic Thrust = $\frac{6.065^2 \times .785 \times 550}{2.31}$ -2,805 Lbs. = 4,070 Lbs. From page 42, 4,000 Lbs. thrust for 6" col. = 0.023" per 100 Ft. of setting $\frac{500}{100} \times 0.023$ " = 0.115"

 $\frac{F \times L \times 12}{26 \times 10^{6} \times (A_{c} + A_{\tau})}$ F = HYDRAULIC FORCE L = COLUMN AND TUBE LENGTH A_c = COLUMN METAL AREA A_T = TUBE METAL AREA

 $\frac{4,070 \times 500 \times 12}{29 \times 10^6 \times (5.6 + 1.5)} = 0.119"$

Using the catalog numbers the net stretch is 0.470" - 0.115" = 0.355" From catalog Pg. 33 the available standard lateral for M9MC bowl assembly is 0.625". Subtract 0.355" from 0.625" is 0.270" net available lateral.

FIELD LATERAL ADJUSTMENT

(for above example)

Lift the shaft to the point where the shaft turns freely. Since the net stretch is 0.355" add 0.125" for impeller seal ring running clearance 0.355 + 0.125 = 0.480" lift required after the shaft turns freely.



DEFINITION OF TERMS COMMONLY USED IN DESCRIBING MOTOR CONTROL EQUIPMENT

- **STARTER:** Device to connect motor to power supply. Normally provides overload protection for all three power lines (commonly called legs) as this is required by virtually all electrical codes.
- **DISCONNECT SWITCH:** Device to disconnect starter from power supply. Uses fuses, fusetrons or circuit breakers to provide short circuit protection to motor.
- MANUAL: Term used to describe any device in which the contactors are opened and closed by manual operation.
- **MAGNETIC:** Term used to describe any device in which the contactors are opened and closed electrically by magnetic coils.
- **COMBINATION MAGNETIC STARTER:** General designation applied to all devices which contain a starter and a disconnect switch within a common enclosure. Pumping plant panels are included in this classification.
- **PUMPING PLANT PANEL:** Consists of a starter and a disconnect switch in one common weather resistant (NEMA 3) enclosure. Also known as a combination outdoor starter.
- **FUSETRON:** Trade name for a bi-metallic type fuse. Allows a smaller fuse clip size to be used in some sizes, thus reducing price.
- **OVERLOAD RELAY:** Device used in starters to prevent motor from operating at an excessive overload for a long period of time. Also provided protection when ambient temperature is high.
- **INRUSH CURRENT:** A momentary surge of current which takes place when a motor is started. Most power companies have rules regulating the maximum allowable inrush current. NEMA code letters have been assigned to motors classifying them according to the relation of their inrush current to their horsepower. A code "F" motor has a higher inrush current than a code "C" motor of the same horsepower.
- **FULL VOLTAGE STARTER:** Most widely used starter for motors up to 200 horsepower. Applies full-line voltage across motor instantaneously. This causes high inrush current, normally in the magnitude of 500% to 600% of full load current.
- **PART WINDING STARTER:** (Also known as Increment Start.) Starter which reduces inrush current to motor by energizing only a portion (1/2 to 2/3) of the motor windings until the motor reaches approximately 80% speed when the remaining windings are also energized. Any 230/460 dual voltage motor is suitable for use with a part winding starter if the line voltage is 230 volts. If the line voltage is 460 volts, the motor must be specially wound. Part winding is the most economical method of reducing motor inrush current.
- VFD (VARIABLE FREQUENCY DRIVE) or AFD (ADJUSTABLE FREQUENCY DRIVE): A motor controller that controls the start and run speeds of a motor by varying the frequency that is output to the motor. This allows for accurate motor speed control based on the pressure and/or flow of the system.
- **AUTO TRANSFORMER REDUCED VOLTAGE STARTER:** Starter which reduces inrush current by using a transformer to obtain a lower than line voltage with which the motor is started. Voltages normally available are 50%, 65% and 80% of full voltage. Can be used with any standard motor.

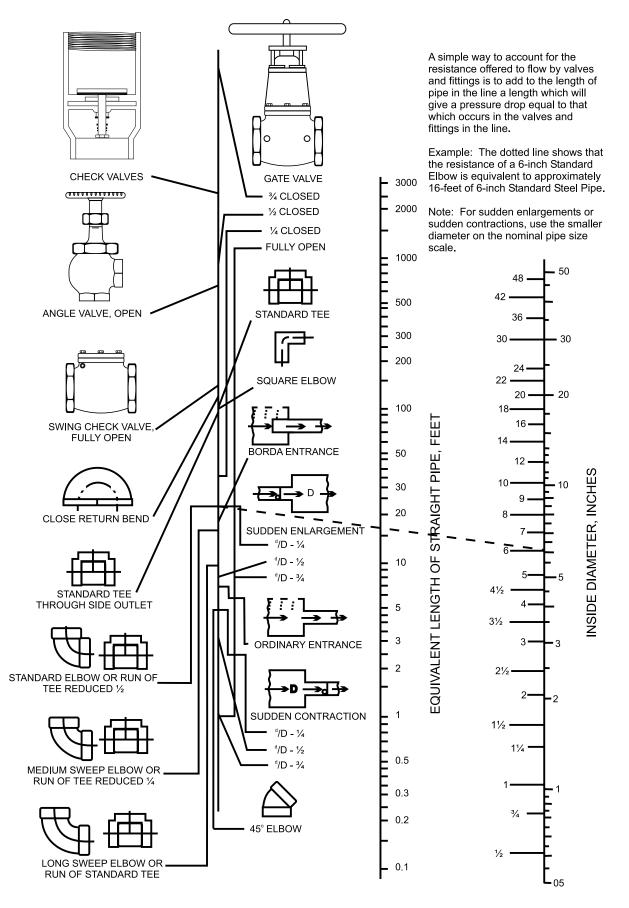


DEFINITION OF TERMS COMMONLY USED IN DESCRIBING MOTOR CONTROL EQUIPMENT CONT.

- **PRIMARY RESISTOR REDUCED VOLTAGE STARTER**: Starter using a resistor in series with the motor windings to reduce the inrush current . Standard starter is a two point, single step type. Multiple step starters are also available. Can be used with any standard motor.
- **WYE-DELTA REDUCED VOLTAGE STARTER:** Starter which reduces inrush current by switching motor leads from wye connection at start to delta connection for running. Motors for use with this type of starter must be ordered special.
- **BACK SPIN TIMER:** (Time delay relay.) Timing device which prevents pump from being restarted until pump has had time to complete back spin after stop.
- **PRESSURE SWITCH:** Switch which is actuated by the pressure in an enclosed system. Switch operates starter to turn pump off and on.
- **UNDER VOLTAGE RELAY:** Device which automatically actuates starter to stop motor if line voltage drops below a predetermined level. Relay must be reset manually.
- PHASE FAILURE AND REVERSE RELAY: Device to prevent operation of motor if any of the three power supply leads are disconnected or crossed. Two different versions of this type relay are available. The less expensive model is known as "starting open phase and phase sequence reversal" and will prevent a motor from starting if one of the three power leads is disconnected but will not necessarily stop a motor which is running. The more expensive model is known as "running open phase and phase sequence reversal" and will stop a motor which is running if one of the three power leads is disconnected.



RESISTANCE OF VALVES AND FITTINGS TO FLOW OF FLUIDS





GENERAL ELECTRICAL INFORMATION

ELECTRICAL DATA

HORSEPOWER-HOUR (H.P.Hr.) = Unit of mechanical work.

No. working hours x .746 x HP motor = K.W.Hr. consumed

working hours per day, week, month, or year:

Efficiency of motor

Cost current for time specified

To determine the cost of Power, for any specified period of time -

K.W.Hr. consumed at Motor Terminals x Rate per K.W.Hr. = Total

at motor terminals

FOOT-POUNDS = Unit of work.

HORSEPOWER (HP) = (33,000 ft. pounds per min. - 746 watts - .746 kilowatts = Unit for measurement of power or rate of work.

VOLT AMPERES = Product of volts and amperes.

KILOVOLT - AMPERES (KVA) = 1000 volt-amperes.

WATT-HOUR = Small unit of electrical work - watts times hours.

KILOWATT-HOUR (K.W.Hr.) = Large unit of electrical work - 1000 watt-hours.

TORQUE is that force which produces or tends to produce torsion (around on axis). Turning effort. It may be thought of as a twist applied to turn a shaft. It can be defined as the push or pull in pounds, along an imaginary circle of one foot radius which surrounds the shaft, or, in an electric motor, as the pull or drag at the surface of the armature multiplied by the radius of the armature, the term being usually expressed in foot-pounds (or pounds at 1 foot radius).

STARTING TORQUE is the torque which a motor exerts when starting. It can be measured directly by fastening a piece of belt to a 25" diameter pulley, wrapping it part way around and measuring the pounds pull the motor exerts, with a spring balance. In practice, any pulley can be used, for Torque = Lbs. pull x pulley radius in feet. A motor that has a heavy starting torque is one that starts up easily with a heavy load.

RUNNING TORQUE is the pull in pounds a motor exerts on a belt running over a pulley 24" in diameter. FULL LOAD TORQUE is the turning moment required to develop normal horsepower output at normal speed. The torque of any motor at any output with a known speed may be determined by the formula: T = Brake HP x 5250 RPM

With a known foot-pounds torque, the horsepower at any given speed can be determined by the formula:: $HP = \underline{T \times RPM} \text{ or } HP = \underline{T \times speed of belt on 24" pulley in feet per minute}$

5250

33000

COST OF PUMPING WATER

Cost per 1000 gallons pumped: <u>189 x Power Cost per kilowatt-hour x Head in fee</u>t

Pump Eff. x Motor Eff. x 60

EXAMPLE:

Power costs .01 per k.w.-hour; pump efficiency is 75%; motor efficiency is 85%; total head is 50 feet:

 $\frac{.189 \times .01 \times 50}{.75 \times .85 \times 60}$ = \$.0025 The cost of pumping 1000 gallons of water under the above conditions is 1/4 of a cent,

Cost per hour of pumping: <u>.000189 x GPM x Head in feet x Power Cost per kilowatt-ho</u>ur Pump Eff. x Motor Eff.

Cost per acre foot of water: <u>1.032 x Head in feet x Power per kilowatt-hour</u> Pump Eff. x Motor Eff.

Pump efficiency: <u>GPM x Head in feet</u> 3960 x BHP (to pump) Head: <u>3960 x Pump Eff. x BHP</u> GPM

BHP (brake horsepower) to pump: Motor efficiency x HP at motor

GPH

 BHP:
 <u>GPM x Head in feet</u>
 GPM:
 <u>3960 x Pump Eff. x BHP</u>

 3960 x Pump Eff.
 Head in feet
 Head in feet

COMPUTING HP INPUT FROM REVOLVING WATT HOUR METERS (Disk Constant Method)

Kilowatts Input = KW in = $K \times R \times 3.60$

 $\begin{array}{rl} \text{HP Input} &= \text{HP in} = \frac{K \ x \ R \ x \ 3600}{t \ x \ 746} \ x \ \frac{4.83 \ x \ K \ x \ R}{t} \\ \text{K} &= \text{Constant representing numbers of watt-hours through} \\ &\text{meter for one revolution of the disk.} \end{array}$

t

meter name-plate or face of disk.) R = Number of revolutions of the disk.

t - Seconds for R revolutions.

Cost per 1000 gallons of water: C = 746 x r x HP in.

C = Cost in dollars per 1000 gallons. r = Power rate per kilowatt hour (dollars). HP in = HP input measured at the meter (see above). H = Total pumping head. GPH = Gallons per hour discharged by pump. Cost per 1000 gallons of water -For each foot of head: C = $\frac{746 \text{ x r x HP in.}}{\text{H x GPH}}$

Cost per hour: $C^1 = .746 \times r \times HP$ in.



USEFUL FORMULAS

Water Horsepower = <u>GPM x 8.</u> 330		WHERE: GPM = Gallons per minute 8.33 = Pounds of water per gallon 33000 = Ft. Lbs. per minute in one horsepower Head = Difference in energy head in feet (field head)							
Laboratory BHP = <u>Head x GPM</u> 3960 x E Field BHP = Laboratory BHP + S Total BHP = Field BHP + Thrust	Eff. Shaft Loss	WHERE: GPM = Gallons per minute Head = Lab. head (including column loss) Eff. = Lab. eff. of pump bowls (from price book curves) Shaft Loss = HP Loss due to mechanical friction of lineshaft bearings (See Page 1) Thrust Bearing Loss = HP loss in driver thrust bearings (1)							
<i>Input Horsepower</i> = <u>Total BHP</u> Motor Eff.		Motor Eff. from motor mfg. (as a decimal)							
Field Efficiency = <u>Water Horsepo</u> Total BHP	ower	Water HP as determined above Total BHP as determined above							
Overall Plant Efficiency = <u>Water</u> Inpu	Horsepower t Horsepower	Water HP as determined above Input HP as determined above (2)							
Electrical	Motor Eff. BHP = Brake horsepower as d Mot. Eff. = Rated motor efficier K = Power company meter cor M = Power company meter mu meter R = Revolutions of meter disk T = Time in sec. for R E = Voltage per leg applied to I = Amperes per leg applied to PF = Power factor of motor	ncy Istant Itiplier, or ratio of current and potential transformers connected with motor motor tors. This reduces to 1 for single phase motors.							
	KW-Hrs. per 1000 Gallons of Co	old Water Pumped per Hour = <u>HD in ft. x 0.00315</u> Pump Eff. x Mot. Eff.							
Miscellaneous	Discharge Head (in feet of fluid pumped) = <u>Discharge Pressure (PSI) x 2.31</u> Sp. Gr. of Fluid Pumped								
Velocity Head = $\frac{V^2}{2G}$ V = Velocity of Water G = Accelerated due to gravity = 32.2 ft/sec ²									
	Torque (foot pounds) = $\frac{HP \times 5250}{n}$ HP = Horsepower n = RPM								

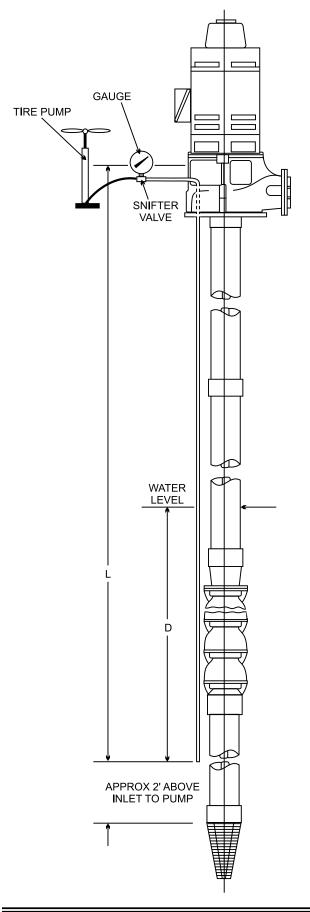
Thrust Bearing Loss = .0075 HP per 100 RPM per 1000 lbs. thrust
 Overall plant efficiency sometimes referred to as "Wire to Water" efficiency



		NVERSION FACTORS	
1 U.S. Gallon =	8.33 lbs. 231 cu. inches 0.1337 cu. feet 3.785 liters 0.833 imp. gallon	1 Lb./Sq. Inch =	2.31 ft. head of water 2.04 in. of mercury 0.0703 kg./sq. centimeter
1 Imperial Gallon =	1.2 U.S. gal. 9.988 lbs.	1 Atmosphere =	10.35 meters of water 29.92 in. of mercury 34.0 ft. of water 14.7 lbs./sq. inch
1 Cubic Foot =	7.48 U.S. gal. 28.316 liters 0.0283 cu. meter 62.35 lbs.	1 Inch of Mercury =	0.49 lbs./sq. inch 1.132 ft. of water
		1 Lb. of Water =	27.71 cu. inches 0.12 U.S. gallon
1 Cubic Ft./Sec. =	449 U.S. GPM	1 Kilogram =	2.2 lbs.
1 Cubic Meter =	264.2 U.S. gal. 35.31 cu. ft. 220 Imp. gal.	1 Kg./Sq. Centimeter =	14.22 lbs./sq. inch
1 Cubic Meter/Hr. =	4.4 U.S. GPM	1 Foot of Water =	0.0295 atmosphere 0.433 lbs./sq. inch
1 Million Gal./Day =	695 U.S. GPM	2000 Lbs. of Water =	240.2 U.S. gallons
1 Million U.S. Gal. =	3.07 Acre ft.	Metric Ton =	2204.6 lbs.
1 Acre Foot =	325,829 U.S. gal.	1000 Lbs. Water/Hour = GPM (Water @ 205°F.) =	2 U.S. GPM (39°F.) Boiler H.P. x 0.072
1 Acre Ft./Day =	227 U.S. GPM	1 Second Foot =	40 CA, NV, MT, Miner's In. 50 ID, NM, UT, Miner's In. 38.4 CO Miner's Inches
1 Liter =	0.2642 U.S. gal. 0.03531 cu. ft. 0.22 Imp. gal.		
1 Liter/Second =	15.85 U.S. GPM	1 Miner's Inch CA, NV, MT = 1 Miner's Inch ID, NM, UT = 1 Miner's Inch CO = 1 Miner's Inch CA, NV, MT = 1 Miner's Inch ID, NM, UT = 1 Miner's Inch CO =	11.22 U.S. GPM 8.98 U.S. GPM 11.69 U.S. GPM 1.5 cu. ft. minute 1.2 cu. ft. minute 1.563 cu. ft. minute
1 Inch =	2.54 Centimeter 25.4 Millimeter		
1 Centimeter =	0.3937 Inch		
1 Meter =	39.37 Inch 3.281 Feet		
1 Kilometer =	3281 Feet	100 U.S. GPM =	0.223 second-foot
1 Mile =	5280 Feet 1.61 Kilometer	1 Meter Head Water =	1.42 lbs./sq. inch
	F° = 9/5 C°(+)32°	Temperature C° = 5/9 (F°	(-)32°)
	UN 1 Kilowatt = KWH per 1000 gallons	ITS OF USAGE COSTS 1.341 horsepower = 737.5 ft. pounds per sec. = Head in feet x 0.00315	



WATER LEVEL TESTING



There are two commonly used methods to determine the water level in wells - airline and gauge, or an electric sounder.

AIRLINE METHOD:

The airline method can use a standard pressure gauge, indirect reading depth gauge, or direct reading depth gauge.

Installation: The airline is installed so that the lower end is near the bottom of the pump - for reliable readings the airline should extend 20' below low water level if possible. All airline joints must be air tight for proper operation. The upper end of the airline is connected to a gauge and snifter valve. Exact vertical length of the airline must be noted at time of installation, this length should be recorded on the face of the gauge.

Operation: A tire pump is used to expel all water from the airline, when this point is reached the gauge reading will remain constant. The maximum maintained pressure is equal to the height of water above the end of the airline (D). Indirect Reading Depth Gauge (Fixed Dial): Pump up airline until maximum pressure (all water is expelled from airline) is reached, reading on gauge will be distance "D". Water level (below surface) is obtained by subtracting "D" from "L" (WL = L - D).

Direct Reading Depth Gauge (Movable Dial): Set the movable gauge dial so that the length of airline (L) is at the pin stop (gauge pointer position at) pressure). Pump airline to maximum pressure, gauge will read water level (L - D) direct.

Pressure Gauge: A pressure gauge can be used by converting PSI to feet of water as follows:

Feet of Water = PSI x 2.31

Operation would be identical to indirect reading gauge.

ELECTRIC SOUNDER METHOD

The electric sounder consists essentially of a battery, a spool of well insulated waterproof wire and a millivolt meter. One terminal of the battery is connected to the pump head and the other through the potentiometer to one end of the spool of wire. The other end of the wire from the spool must be protected so that it will not close the circuit if it should bump against the pump in being lowered into the well, but at the same time so arranged that the circuit will be closed when the end of the wire contacts the water in the well. The wire from the spool is then lowered into the well until the needle of the potentiometer deflects, indicating that the water level has been reached an the contact closed. The wire is then properly marked, pulled from the well and measured with a steel tape to determine the water level. (It is possible to calibrate the spool of wire so that it is direct reading).

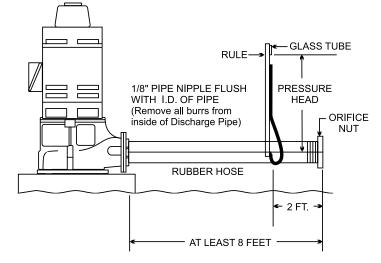


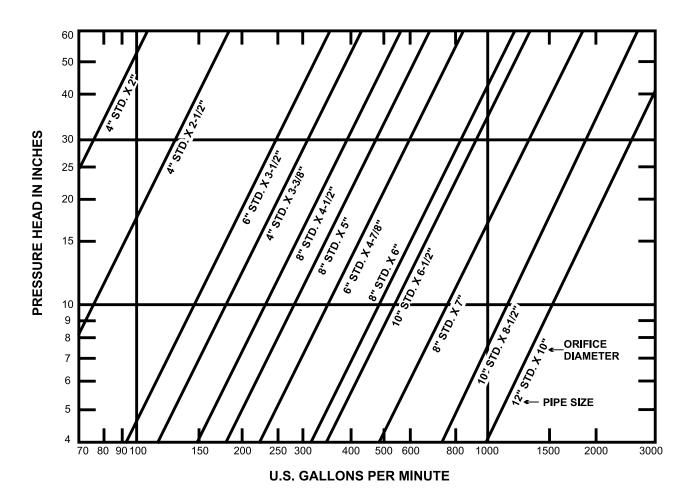
MEASURING FLOW ORIFICE METHOD

MEASURING WATER USING AN ORIFICE

The use of an orifice is one of the simplest methods of accurately measuring the discharge from a vertical turbine pump in the field. The equipment and method is as illustrated.

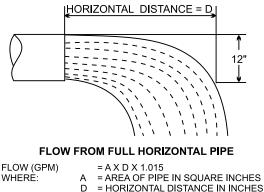
- a. Discharge pipe must be horizontal and measuring tube connection in center of pipe.
- b. Pipe must be flowing full with clear water free of sand and air, with a minimum pressure head 2" above top of pipe.
- c. Pressure head is the vertical distance from the horizontal center line of the orifice to the level of the water in the measuring tube.
- d. Rubber hose and glass tube must be free of air bubbles.







Where no instruments are available to accurately measure the flow of water from a pump, the following method will serve as an approximation.



D = HORIZONTAL DISTANCE I 1.015 = CORRECTION FACTOR Using an ordinary ruler or carpenter's square, measure the horizontal distance from the end of the discharge pipe to a point exactly 12 inches above the falling stream of water. The discharge pipe must be level and running full of water when the reading is taken. Multiply this distance (in inches) by the cross sectional area of the pipe in square inches and the answer will be the approximate capacity in gallons per minute. For example: assume that the horizontal distance from the end of an 8" discharge pipe is 20". Multiplying 20" by the cross sectional area of an 8" pipe (approximately 50 sq. in.) we obtain a capacity of 1000 GPM.

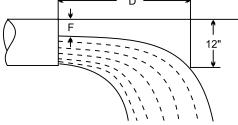
By checking this method of estimation using accurate flow meters it has been found a correction factor of 1.015 should be applied. The table below gives the approximate rates of flow for various distances after applying this factor.

APPROXIMATE FLOW IN GALLONS PER MINUTE WITH PIPE RUNNING FULL

DIA.				HORIZON	ITAL DIST	ANCE D IN	INCHES			
INCHES	12	14	16	18	20	22	24	26	28	30
4	150	181	207	232	258	284	310	336	361	387
6	352	410	470	528	587	645	705	762	821	880
8	610	712	813	915	1017	1119	1221	1322	1425	1527
10	960	1120	1280	1440	1600	1760	1920	2080	2240	2400
12	1378	1607	1835	2032	2286	2521	2760	2980	3210	3430

MEASURING FLOW AREA FACTOR METHOD (PIPE NOT RUNNING FULL)





FLOW FROM HORIZONTAL PIPE (NOT FULL)

FLOW (GPM) WHERE:	-	= A X D X 1.039 X F = AREA OF PIPE IN SQUARE INCHES = HORIZONTAL DISTANCE IN INCHES = EFFECTIVE AREA FACTOR SHOWN BELOW AREA OF PIPE EQUALS INSIDE DIA. X 0.7854	E
	-	= AREA OF PIPE IN SQUARE INCHES = HORIZONTAL DISTANCE IN INCHES = EFFECTIVE AREA FACTOR SHOWN BELOW	

	RATIO F/D = R %	EFF. AREA FACTOR F	RATIO F/D = R %	EFF. AREA FACTOR F	
	5	0.981	55	0.436	
	10	0.948	60	0.373	
	15	0.905	65	0.312	
	20	0.858	70	0.253	
	25	0.805	75	0.195	
	30	0.747	80	0.142	
	35	0.688	85	0.095	
	40	0.627	90	0.052	
	45	0.564	95	0.019	
	50	0.500	100	0.000	
EXAMPLE: D = 20 INCHES - PIPE INSIDE DIAMETER = 10					

D = 20 INCHES - PIPE INSIDE DIAMETER = 10 INCHES

F = 2-1/2 INCHES

A = 10 X 10 X 0.7854 = 78.54 SQUARE INCHES

R = 2-1/2 / 10 = 25%

F = 0.805

FLOW = 78.54 X 20 X 0.805 = 1314 GPM



ENGINEERING

DATA REQUIRED BY PUMP MANUFACTURERS FOR PROPER SELECTION OF MATERIAL

1. SOLUTION TO BE PUMPED (Give common name, where possible, such as "spinning bath", "black liquor", "spent pickle", etc.

 PRINCIPAL CORROSIVES (H₂SO₄, HCI, ETC) _____% by weight (In the case of mixtures, state definite percentages by weight. For example: mixture contains 2% acid, in terms of 96.5% H₂SO₄.)_____

3. pH (if aqueous solution)______ At _____ F.

4. Impurities or other constituents not given in "2" (List amounts of any metallic salts, such as chlorides, sulphates, sulphides, chromates, and any organic materials which may be present, even though in percentages as low as .01%. Indicated, where practical, whether they act as accelerators or inhibitors on the pump material.)

5. SPECIFIC GRAVITY (solution pumped)______at _____F.

TEMPERATURE OF SOLUTION: Maximum ______F, Minimum _____F, Normal _____F. 6. VAPOR PRESSURES AT ABOVE TEMPERATURES: Maximum _____Minimum _____Normal _____ 7.

(indicate units used, such as pounds, gauge, inches water, milimeters mercury.)

8.	VISCOSITY	SSU; or		_centistokes; at		F.
9.	AERATION: Air-Free		Partial		_Saturated _	
	Does liquid have tendency to foam?					
10.	OTHER GASES IN SOLUTION		ppm, c	or		_cc per liter

11. SOLIDS IN SUSPENSION: (state types)_____



COMMON MATERIALS OF CONSTRUCTION FOR VARIOUS LIQUIDS

MATERIAL SELECTION	ASTM NUMBER	REMARKS	
А		ALL BRONZE CONSTRUCTION	
В		BRONZE FITTED CONSTRUCTION	
С		ALL IRON CONSTRUCTION	pH VALUE
3	A216-WCB	CARBON STEEL	GENER
4	A217-C5	5% CHROMIUM STEEL	PUMP C
5	A743-CA15	12% CHROMIUM STEEL	
6	A743-CB630	20% CHROMIUM STEEL	
7	A743-CC50	28% CHROMIUM STEEL	Corrosion
8	A743-CF-8	19-9 AUSTENITIC STEEL	Resistant Alloys
9	A743-CF-8M	19-10 MOLYBDENUM AUSTENITIC STEEL	
10	A743-CN-7M	20-29 CHROMIUM NICKEL AUSTENITIC STEEL WITH COPPER & MOLYBDENUM	All Iron or Steel Standard
11		A SERIES OF NICKEL-BASED ALLOYS	Iron fitted or Bronze Ftd.
12	A518	CORROSION-RESISTANT HIGH- SILICON CAST IRON	All Bronze
13	A436	AUSTENITIC CAST IRON - 2 TYPES	
13(a)	A439	DUCTILE AUSTENITIC CAST IRON	Corrosion Resistant
14		NICKEL-COPPER ALLOY	Alloy Steels
15		NICKEL	

Table shows the materials commonly used for pumping various liquids. The material selection codes shown in column 5 are described below. When pumping liquids other than water, it may be necessary to specify special pump construction and/or shaft seal materials that will be compatible with the liquid being pumped. The following pump materials guide for various liquids is intended only as a guide. It merely suggests materials of construction which have been used successfully and does not constitute a guarantee of performance.



pH INDICATORS pH OF COMMON ACIDS

<u>ACIDS (pH <7)</u>	MOLARITY	рH
ACETIC	 Ν	 2.4
ACETIC	 0.1N	 2.9
ACETIC	 0.01N	 3.4
ALUM	 0.1N	 3.2
ARSENIOUS	 SATURATED	 5.0
BENZOIC	 0.1N	 3.0
BORIC	 0.1N	 5.3
CARBONIC	 SATURATED	 3.8
CITRIC	 0.1N	 2.1
FORMIC	 0.1N	 2.3
HYDROCHLORIC	 Ν	 0.1
HYDROCHLORIC	 0.1N	 1.1
HYDROCHLOIRC	 0.01N	 2.0
HYDROCYANIC	 0.1N	 5.1
HYDROGEN SULFIDE	 0.1N	 4.1
LACTIC	 0.1N	 2.4
MALIC	 0.1N	 2.2
ORTHOPHOSPHORIC	 0.1N	 1.5
OXALIC	 0.1N	 1.3
SUCCINIC	 0.1N	 2.7
SALICYLIC	 SATURATED	 2.4
SULFURIC	 Ν	 0.3
SULFURIC	 0.1N	 1.2
SULFURIC	 0.01N	 2.1
SULFUROUS	 0.1N	 1.5
TARTARIC	 0.1N	 2.0
TRICHLORACETIC	 0.1N	 1.2

pH OF COMMON BASES

<u>ACIDS (pH >7)</u>	MOLARITY	<u>рН</u>
AMMONIA	 Ν	 11.6
AMMONIA	 0.1N	 11.1
AMMONIA	 0.01N	 10.6
BARBITAL SODIUM	 0.1N	 9.4
BORAX	 0.01N	 9.2
CALCIUM CARBONATE	 SATURATED	 9.4
CALCIUM HYDROXIDE	 SATURATED	 12.4
FERROUS HYDROXIDE	 SATURATED	 9.5
LIME	 SATURATED	 12.4
MAGNESIA	 SATURATED	 10.5
POTASSIUM ACETATE	 0.1N	 9.7
POTASSIUM BICARBONATE	 0.1N	 8.2
POTASSIUM CARBONATE	 0.1	 11.5
POTASSIUM CYANIDE	 0.1N	 11.0
POTASSIUM HYDROXIDE	 Ν	 14.0
POTASSIUM HYDROXIDE	 0.1N	 13.0
POTASSIUM HYDROXIDE	 0.01N	 12.0
SODIUM ACETATE	 0.1N	 8.9
SODIUM BENZOATE	 0.1N	 8.0
SODIUM BICARBONATE	 0.1N	 8.4
SODIUM CARBONATE	 0.1N	 11.6
SODIUM HYDROXIDE	 Ν	 14.0
SODIUM HYDROXIDE	 0.1N	 13.0
SODIUM HYDROXIDE	 0.01N	 12.0
SODIUM METASILICATE	 0.1N	 12.6
SODIUM SESQUICARBONATE	 0.1N	 10.1
TRISODIUM PHOSPHATE	 0.1N	12.0



pH INDICATORS pH OF COMMON ACIDS

INDICATOR	ACI	D COLOR		<u>pH</u>	BA	<u>SE COLOR</u>
CRESOL RED #1		RED		0.2-1.8		YELLOW
CRESOL PURPLE #1		RED		1.2-2.8		YELLOW
THYMOL BLUE		RED		1.2-2.8		YELLOW
METANIL YELLOW		RED		1.2-2.3		YELLOW
TROPAEOLIN LL		RED		1.4-3.2		YELLOW
2,6 DINITROPHENOL		NO COLOR		1.7-4.4		YELLOW
BENZYL ORANGE		RED		1.9-3.3		YELLOW
2,6 DINITROPHENOL		NO COLOR		2.0-4.7		YELLOW
BENZO YELLO		RED		2.4-4.0		YELLOW
p-DIMETHYLANINOAZOBENZENE		RED		2.9-4.0		YELLOW
BROMOPHENOL BLUE		RED		3.0-4.6		VIOLET
CONGO RED		BLUE		3.0-5.0		RED
BROMOCHLOROPHENOL BLUE		YELLOW		3.0-4.6		PURPLE
METHYL ORANGE		RED		3.1-4.4		YELLOW
BROMOCRESOL GREEN		YELLOW		3.8-5.4		BLUE
2,5 DINITROPHENOL		NO COLOR		4.0-5.8		YELLOW
METHYL RED		RED		4.4-6.0		YELLOW
AZOLITMIN (LITMUS)		RED		4.4-6.6		BLUE
PROPYL RED		RED		4.6-6.6		YELLOW
p-NITROPHENOL		NO COLOR		4.0-0.0		YELLOW
BROMOCRESOL PURPLE				4.8-6.8		PURPLE
BROMOCRESOL FORFLE BROMOPHENOL RED		YELLOW				
		YELLOW		4.8-6.8		PURPLE
CHLOROPHENOL RED		YELLOW		5.0-6.9		PURPLE
		YELLOW		6.0-7.6		BLUE
m-NITROPHENOL		NO COLOR		6.6-8.6		YELLOW
NEUTRAL RED		RED		6.8-8.0		YELLOW
PHENOL RED	•••••	YELLOW	•••••	6.8-8.4		RED
ROSOLIC ACID	•••••	BROWN		6.9-8.0	•••••	RED
CRESOL RED #2		YELLOW		7.2-8.8		PURPLE
a-NAPHTHOLPHTHALEIN		BROWN		7.3-8.7		GREEN
ORANGE I		YELLOW		7.6-6.9		ROSE
m-CRESOL PURPLE #2		YELLOW		7.6-9.2		PURPLE
THYMOL BLUE #2		YELLOW		8.0-9.6		BLUE
o-CRESOLPHTHALEIN		NO COLOR		8.2-9.8		RED
PHENOLPHTHALEIN		NO COLOR		8.3-10.0		RED
PHTHALEIN RED		YELLOW		8.6-10.2		RED
THYMOLPHTHALEIN		NO COLOR		9.3-10.5		BLUE
TOLYL RED		RED		10.0-11.6		YELLOW
b-NAPHTHOL VIOLET		YELLOW		10.0-12.0		VIOLET
ALIZARIN YELLOW R		YELLOW		10.0-12.1		BROWN
ALIZARIN YELLOW GG		YELLOW		10.0-12.0		ORANGE
NITRAMINE		NO COLOR		10.8-13.0		BROWN
PARAZO ORANGE		YELLOW		11.0-12.6		ORANGE
[PORROER BLUE		BLUE		11.0-13.0		RED
TROPAEOLIN O		YELLOW		11.1-12.7		ORANGE
ACYL BLUE		RED		12.0-13.6		BLUE
	•••••		•••••	12.0 10.0	•••••	DLOL

pH VALUES ARE APPROXIMATE VALUES AND HAVE BEEN ROUNDED OFF TO THE NEAREST TENTH. VALUES ASSUME A TEMPERATURE OF 25° C (77° F).



COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5
LIQUID	CONDITIONS OF LIQUID	CHEMICAL	SPECIFIC	MATERIAL
		SYMBOL	GRAVITY	SELECTION
ACETALDEHYDE		C2H4O	0.78	С
ACETATE SOLVENTS				A, B, C, 8, 9, 10, 11
ACETONE		C3H6O	0.79	B, C
ACETIC ANHYDRIDE		C2H6O3	1.08	8, 9, 10, 11, 12
ACID, ACETIC	CONC. COLD	C2H4O2	1.05	8, 9, 10, 11, 12
ACID, ACETIC	DIL. COLD			A, 8, 9, 10, 11, 12
ACID, ACETIC	CONC. BOILING			9, 10, 11, 12
ACID, ACETIC	DIL. BOILING			9, 10, 11, 12
ACID, ARSENIC, ORTHO		H2AsO4.1/2H2O	2.0-2.5	8, 9, 10, 11, 12
ACID, BENZOIC		C7H6O2	1.27	8, 9, 10, 11
ACID, BORIC	AQUEOUS SOL.	H3BO3		A, 8, 9, 10, 11, 12
ACID, BUTYRIC	CONC.	C4H8O2	0.96	8, 9, 10, 11
ACID, CARBOLIC	CONC. (M.P. 106°F)	C6H6O	1.07	C, 8, 9, 10, 11
ACID, CARBOLIC	(SEE PHENOL)			B, 8, 9, 10, 11
ACID, CARBONIC	AQUEOUS SOL.	CO2 + H2O		Α
ACID, CHROMIC	AQUEOUS SOL.	CR2O3 + H2O		A, 8, 9, 10, 11, 12
ACID, CITRIC	AQUEOUS SOL.	C6H8O7 + H2O		A, 8, 9, 10, 11, 12
ACIDS, FATTY (OLEIC,				,, , , , , , , , , , , , , , , , , , , ,
PALMITIC, STEARIC, ETC.)				A, 8, 9, 10, 11
ACID, FORMIC		CH ₂ O ₂	1.22	9, 10, 11
ACID, FRUIT		011202		A, 8, 9, 10, 11, 14
ACID, HYDROCHLORIC	COML CONC.	HCI	1.19(38%)	11, 12
ACID, HYDROCHLORIC	DIL. COLD		1.10(0070)	10, 11, 12, 14, 15
ACID, HYDROCHLORIC	DIL. HOT			11,12
ACID, HYDROCYANIC	DIE. HOT	HCN	0.70	C, 8, 9, 10, 11
ACID, HYDROFLUORIC	ANHYDROUS, WITH HYDRO	HF + HxCx		3, 14
	CARBON			-,
ACID, HYDROFLUORIC	AQUEOUS SOL.	HF		A, 14
ACID, HYDROFLUOSILCIC		H ₂ SiF ₆	1.30	A, 14
ACID, LACTIC		C3H6O3	1.25	A, 8, 9, 10, 11, 12
ACID, MINE WATER			1120	A, 8, 9, 10, 11
ACID, MIXED	SULFURIC + NITRIC			C, 3, 8, 9, 10, 11, 12
ACID, MURIATIC	(SEE ACID, HYDROCHLORIC)			
ACID, NAPHTHENIC				C, 5, 8, 9, 10, 12
ACID, NITRIC	CONC. BOILING	HNO3	1.50	6, 7, 10, 12
ACID, NITRIC	DILUTE			5, 6, 7, 8, 9, 10, 12
ACID, OXALIC	COLD	C2H2O4.2H2O	1.65	8, 9, 10, 11, 12
ACID, OXALIC	НОТ	C2H2O4.2H2O		10, 11, 12
ACID, ORTHO-PHOSPHORIC		H3PO4	1.87	9, 10, 11
ACID, PICRIC		C6H3N3O7	1.76	8, 9, 10, 11, 12
ACID, PYROGALLIC		C6H6O3	1.45	8, 9, 10, 11
ACID, PYROLIGNEOUS		5011000		A, 8, 9, 10, 11
ACID, SULFURIC	>77% COLD	H ₂ SO ₄	1.69-1.84	C, 10, 11, 12
ACID, SULFURIC	65/93%. 175°F	12004		11, 12
ACID, SULFURIC	65/93%, 175 F			10, 11, 12
	00/95%, 1/0 F			10, 11, 12



COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5
LIQUID	CONDITIONS OF LIQUID	CHEMICAL	SPECIFIC	MATERIAL
		SYMBOL	GRAVITY	SELECTION
ACID, SULFURIC	10-65%			10, 11, 12
ACID, SULFURIC	10%			A, 10, 11, 12, 14
ACID, SULFURIC (OLEUM)	FUMING	H2SO4 + SO3	1.92-1.94	3, 10, 11
ACID SULFUROUS		H2SO3		A, 8, 9, 10, 11,
ACID, TANNIC		C14H10O9		A, 8, 9, 10, 11, 14
ACID, TARTARIC	AQUEOUS SOL.	C4H6O6. H20		A, 8, 9, 10, 11, 14
ALCOHOLS				А, В
ALUM	(SEE ALUMINUM SULPHATE			
	AND POTASH ALUM)			
ALUMINUM SULPHATE	AQUEOUS SOL.	AL2(SO4)3		10, 11, 12,14
AMMONIA, AQUA		NH4OH		С
AMMONIUM BICARBONATE	AQUEOUS SOL.	NH4HCO3		С
AMMONIUM CHLORIDE	AQUEOUS SOL.	NH4CI		9, 10, 11, 12, 14
AMMONIUM NITRATE	AQUEOUS SOL.	NH4NO3		C, 8, 9, 10, 11, 14
AMMONIUM PHOSPHATE,	AQUEOUS SOL.	(NH4)2HPO4		C, 8, 9, 10, 11, 14
DIBASIC				
AMMONIUM SULFATE	AQUEOUS SOL.	(NH4)2SO4		C, 8, 9, 10, 11
AMMONIUM SULFATE	WITH SULFURIC ACID			A, 9, 10, 11, 12
ANILINE		C6H7N	1.02	B, C
ANILINE HYDROCHLORIDE	AQUEOUS SOL.	C6H5NH2HCI		11, 12
ASPHALT	НОТ		0.98-1.4	C, 5
BARIUM CHLORIDE	AQUEOUS SOL.	BaCı2		C, 8, 9, 10, 11
BARIUM NITRATE	AQUEOUS SOL.	Ba(NO3)2		C, 8, 9, 10, 11
BEER				A, 8
BEER WORT				A, 8
BEET JUICE				A, 8
BEET PULP				A, B, 8, 9, 10, 11
BENZENE		C6H6	0.88	
BENZINE	(SEE PETROLEUM ETHER)			
BENZOL	(SEE BENZENE)			B, C
BICHLORIDE OFMERCURY	(SEE MERCURIC CHLORIDE)			
BLACK LIQUOR	(SEE LIQUOR, PULP MILL)			
BLEACH SOLUTIONS	(SEE TYPE)			
BLOOD				А, В
BOILER FEEDWATER	(SEE WATER, BOILER FEED)			
BRINE, CALCIUM CHLORIDE	pH>8	CaCl ₂		С
BRINE, CALCIUM CHLORIDE	pH<8			A, 10, 11, 13, 14
BRINE, CALCIUM AND	AQUEOUS SOL			A, 10, 11, 13, 14
MAGNESIUM CHLORIDES				
BRINE, CALCIUM AND	AQUEOUS SOL.			A, 10, 11, 13, 14
SODIUM CHLORIDE				
BRINE, SODIUM CHLORIDE	UNDER 3% SALT, COLD	NaCl		A, C, 13
BRINE, SODIUM CHLORIDE	OVER 3% SALT, COLD		1.02-1.20	A, 8, 9, 10, 11, 13, 14
BRINE, SODIUM CHLORIDE	OVER 3% SALT, HOT			9, 1, 11, 12, 14
BRINE, SEAWATER	· -		1.03	A, B, C
,			0.60 @32°F	B, C, 3



COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5
LIQUID	CONDITIONS OF LIQUID	CHEMICAL	SPECIFIC	MATERIAL
		SYMBOL	GRAVITY	SELECTION
CALCIUM BISULFITE	PAPER MILL	Ca(HSO ₃)	1.06	9, 10, 11
CALCIUM CHLORATE	AQUEOUS SOL.	Ca(C103)22H2O		10, 11, 12
CALCIUM HYPOSCHLORITE		Ca(OCI)2		C, 10, 11,12
CALCIUM MAGNESIUM	(SEE BRINES)			-, -, -,
CHLORIDE	()			
CANE JUICE				A, B, 13
CARBON BISULFIDE		CS ₂	1.26	C
CARBONATE OF SODA	(SEE SODA ASH)			-
CARBON TETRACHLORIDE	ANHYDROUS	CCI4	1.50	B, C
CARBON TETRACHLORIDE	PLUS WATER			A, 8
CATSUP				A, 8, 9, 10, 11
CAUSTIC POTASH	(SEE POTASSIUM			7, 0, 0, 10, 11
	HYDROXIDE)			
CAUSTIC SODA	(SEE SODIUM HYDROXIDE)			
CELLULOSE ACETATE				9, 10, 11
CHLORATE OF LIME	(SEE CALCIUM CHLORATE)			3, 10, 11
CHLORIDE OF LIME	(SEE CALCIUM			
	HYPOCHLORITE)			
	(DEPENDING ON CONC.)			9, 10, 11, 12
	(DEFENDING ON CONC.)	C₀H₅CI	1.1	
CHLOROBENZENE				A, B, 8
CHLOROFORM			1.5	A, 8, 9, 10, 11,14
CHROME ALUM		CrK(SO4)2.12H2O		10, 11, 12
CODENSATE	(SEE WATER, DISTILLED)			
COPPERAS, GREEN	(SEE FERROUS SULFATE)			
COPPER AMMONIUM	AQUEOUS SOL.			C, 8, 9, 10, 11
				44.40
COPPER CHLORIDE (CUPRIC)	AQUEOUS SOL.			11, 12
COPPER NITRATE		Cu(NO ₃) ₂		8, 9, 10, 11
COPPER SULFATE, BLUE VITRIOL		CuSO4		8, 9, 10, 11, 12
CREOSOTE	(SEE OIL, CREOSOTE)			
CRESOL,META		C7H9O	1.03	C, 5
CYANIDE	(SEE SODIUM CYANIDE			
	AND POTASSIUM CYANIDE)			
CYANOGEN	IN WATER	(CN)2GAS		C
DIPHENYL		C6H5.C6H5	.99	C, 3
ENAMEL				С
ETHANOL	(SEE ALCOHOLS)			
ETHYLENE CHLORIDE	COLD	C2H4CI2	1.28	A, 8, 9, 10, 11, 14
(DI-CHLORIDE)				
FERRIC CHLORIDE	AQUEOUS SOL.	FeCl₃		11,12
FERRIC SULPHATE	AQUEOUS SOL.	FE2(SO4)3		8, 9, 10,11, 12
FERROUS CHLORIDE	COLD, AQUEOUS	FeCL ₂		11, 12
FERROUS SULPHATE	AQUEOUS SOL.	FeSO4		9, 10, 11, 12, 14
(GREEN COPPERAS)				
FORMALDEHYDE		CH2O	1.08	A, 8, 9, 10, 11
FRUIT JUICES				A, 8, 9, 10, 11, 14
FURFURAL		C5H4O2	1.16	



COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5
LIQUID	CONDITIONS OF LIQUID	CHEMICAL		
GASOLINE		SYMBOL	GRAVITY 0.68-0.75	B, C
GAUBES SALT	(SEE SODIUM SULFATE)		0.00-0.75	В, С
GLUCOSE				A, B
GLUE	НОТ			B, C
GLUE SIZING				A A
GLYCEROL (GLYCERIN)		C3H8O3	1.26	A, B, C
GREEN LIQUOR	(SEE LIQUOR, PULP MILL)	0311803	1.20	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
HEPTANE		C7H16	0.69	B, C
HYDROGEN PEROXIDE	AQUEOUS SOL.	H2O2	0.00	8, 9, 10, 11
HYDROGEN SULFIDE	AQUEOUS SOL.	H ₂ S		8, 9, 10, 11
HYDROSULFITE OF SODA	(SEE SODIUM HYDROSULFITE)	1120		0, 0, 10, 11
HYPOSULFITE OF SODA	(SEE SODIUM THIOSULFATE)			
KAOLIN SLIP	SUSPENSION IN WATER			C, 3
KAOLIN SLIP	SUSPENSION IN ACID			10, 11, 12
KEROSENE	(SEE OIL KEROSENE)			,,
LARD	НОТ			B, C
LEAD ACETATE	AQUEOUS SOL.	Pb(C2H3O2)2. 3H2O		9, 10, 11, 14
(SUGAR OF LEAD)				-, -, -, -, -
	MOLTEN			C, 3
LIME WATER (MILK OF LIME)		Ca(OH)2		C, 3 C
LIQUOR-PULP MILL: BLACK				C, 3, 9, 10, 11, 12, 14
LIQUOR-PULP MILL: GREEN				C, 3, 9, 10, 11, 12, 14
LIQUOR-PULP MILL:WHITE				C, 3, 9, 10, 11, 12, 14
LIQUOR-PULP MILL: PINK				C, 3, 9, 10, 11, 12, 14
LIQUOR-PULP MILL: SULFITE				9, 10, 11
LITHIUM CHLORIDE	AQUEOUS SOL.	LiCI		С
LYE, CAUSTIC	(SEE POTASSIUM AND			
	SODIUM HYDROXIDE)			
MAGNESIUM CHLORIDE	AQUEOUS SOL.	MgCI ₂		10, 11, 12
MAGNESIUM SULFATE	AQUEOUS SOL.	MgSo ₄		C, 8, 9, 10, 11
(EPSON SALTS)		-		
MANGANESE CHLORIDE	AQUEOUS SOL.	Mnc12.4H2O		A, 8, 9, 10, 11, 12
MANGANOUS SULFATE	AQUEOUS SOL.	MnSO4. 4H2O		A, C, 8, 9, 10, 11
MASH				A, B, 8
MERCURIC CHLORIDE	VERY DILUTE AQUEOUS SOL.	HgCl ₂		9, 10, 11, 12
MERCURIC CHLORIDE	COMPL. CONC. AQUEOUS SOL.	HgCl ₂		11, 12
MERCURIC SULFATE	IN SULFURIC ACID	HgSO ₄ + H ₂ SO ₄		10, 11, 12
MERCUROUS SULFATE	IN SULFURIC ACID	Hg2SO4 + H2SO4		10, 11, 12
METHYL CHLORIDE		CH₃CI	0.52	С
METHYLENE CHLORIDE		CH ₃ Cl ₂	1.34	C, 8
MILK			1.03-1.04	8
MILK OF LIME	(SEE LIME WATER)			
MINE WATER	(SEE ACID, MINE WATER)			
MISCELLA	(20% SOYBEAN OIL & SOLVENT		0.75	С
MOLASSES				А, В



ENGINEERING

COLUMN 1	COLUMN 2		COLUMN 4	COLUMN 5
		COLUMN 3		MATERIAL
		CHEMICAL	GRAVITY	SELECTION
MUSTARD		SYMBOL		A, 8, 9, 10, 11, 12
NAPHTHA			0.78-0.88	B, C
NAPHTHA, CRUDE			0.92-0.95	B, C
NICOTINE SULFATE		(Curl I) No 201	0.02 0.00	10, 11, 12, 14
NITRE	(SEE POTASSIUM NITRATE)	(C10H14N2)2H2SO4		10, 11, 12, 11
NITRE CAKE	(SEE SODIUM BISULPHATE)			
NITRO ETHANE		0.11-NO.	1.04	B, C
NITRO METHANE		C2H5NO2	1.14	B, C
OIL, COAL TAR		CH3NO2		B, C, 8, 9, 10, 11
OIL, COCONUT			0.91	A, B, C, 8, 9, 10, 11, 14
OIL, CREOSOTE			1.04-1.10	B, C
OIL, CRUDE	COLD		1.04-1.10	B, C
OIL, CRUDE	НОТ			3
OIL, ESSENTIAL				А, В, С
OIL, ESSENTIAL				А, В, С В, С
OIL, FOEL				B, C B, C
			0.94	в, с А, В, С, 8, 9, 10, 11, 14
			0.94	
				B, C
			0.00	B, C,
			0.90	B, C
OIL, PALM			0.90	A, B, C, 8, 9, 10, 11, 14
			0.91	B, C
OIL, RAPESEED			0.92	A, 8, 9, 10, 11, 14
OIL, SOYA BEAN				A, B, C, 8, 9, 10, 11, 14
OIL, TURPENTINE			0.87	B, C
PARAFFIN	НОТ			B, C
PERHYDROL	(SEE HYDROGEN PEROXIDE)			
PEROXIDE OF HYDROGEN	(SEE HYDROGEN PEROXIDE)			
PETROLEUM ETHER				B, C
PHENOL		CeHeO	1.07	
PINK LIQUOR	(SEE LIQUOR, PULP MILL)			
PHOTOGRAPHIC DEVELOPERS				8, 9, 10, 11
PLATING SOLUTIONS	(VARIED AND COMPLICATED,			
	CONSULT PUMP MFRS.)			
POTASH	PLANT LIQUOR			A, 8, 9, 10, 11,13, 14
POTASH ALUM	AQUEOUS SOL.	AI2(SO4)3K2SO4.24H20		A, 9, 10, 11,12, 13, 14
POTASSIUM BICHROMATE	AQUEOUS SOL.	K2Cr2O7		С
POTASSIUM CARBONATE	AQUEOUS SOL.	K2CO3		С
POTASSIUM CHLORATE	AQUEOUS SOL.	KCIO3		8, 9, 10, 11, 12
POTASSIUM CHLORIDE	AQUEOUS SOL.	КСІ		A, 8, 9, 10, 11, 14
POTASSIUM CYANIDE	AQUEOUS SOL.	KCN		С
POTASSIUM HYDROXIDE	AQUEOUS SOL.	кон		C, 5,8,9,10,11,13,14, 15
POTASSIUM NITRATE	AQUEOUS SOL.	KNO3		C, 5, 8, 9, 10, 11
POTASSIUM SULFATE	AQUEOUS SOL.	K2SO4		A, 8, 9, 10, 11
PROPANE		C3H8	0.59@48 [°] F	B, C, 3



COLUMN 1	COLUMN 2	COLUMN 3	COLUMN 4	COLUMN 5
LIQUID	CONDITIONS OF LIQUID	CHEMICAL	SPECIFIC	MATERIAL
		SYMBOL	GRAVITY	SELECTION
PYRIDINE		C5H5N	0.98	С
PYRIDINE SULFATE				10, 12
RHIDOLENE				В
ROSIN (COLOPHONY)				С
SALT AMMONIAC	(SEE AMMONIUM CHLORIDE)			
SALT LAKE	AQUEOUS SOL.	Na ₂ SO ₄ + IMPURITIES		A, 8, 9, 10. 11, 12
SALT WATER	(SEE BRINES)			
SEA WATER	(SEE BRINES)			
SEWAGE				A, B, C
SHELLAC				A
SILVER NITRATE	AQUEOUS SOL.	AgNo ₃		8, 9, 10, 11, 12
SLOP, BREWERY				A, B, C
SLOP DISTILLERS				A, 8, 9, 10, 11,
SOAP LIQUOR				С
SODA ASH	COLD	Na2CO3		С
SODAASH	HOT			8, 9, 10, 11,13, 14
SODIUM BICARBONATE	AQUEOUS SOL.	NaHCO₃		C, 8, 9, 10, 11, 13
SODIUM BISULFATE	AQUEOUS SOL.	NaHSO ₄		10, 11, 12
SODIUM CARBONATE	(SEE SODA ASH)			
SODIUM CHLORATE	AQUEOUS SOL.	NaCIO ₃		8, 9, 10, 11, 12
	(SEE BRINES)	N. ON		
	AQUEOUS SOL.	NaCN		C
SODIUM HYDROXIDE	AQUEOUS SOL.	NaOH		C, 5, 8, 9, 10, 11, 13, 14, 15
SODIUM HYDROSULFITE	AQUEOUS SOL.	Na2S204, 2H20		8, 9, 10, 11
SODIUM HYPOCHLORITE		NaOCI		10, 11, 12
SODIUM HYPOSULFITE	(SEE SODIUM THIOSULFATE)			
SODIUM META SILICATE				С
SODIUM NITRATE	AQUEOUS SOL.	NaNO ₃		C, 5, 8, 9, 10, 11
SODIUM PHOSPHATE:	AQUEOUS SOL.	NaH2PO4, H20		A,8, 9, 10, 11
MONOBASIC				
SODIUM PHOSPHATE:	AQUEOUS SOL.	Na2HPO4. 7H2O		A, C, 8, 9, 10, 11
DIBASIC				
SODIUM PHOSPHATE:	AQUEOUS SOL.	NaPO4.12H2O		С
TRIBASIC				
SODIUM PHOSPHATE: META	AQUEOUS SOL.	Na4P4O12		A, 8, 9, 10, 11
SODIUM PHOSPHATE:	AQUEOUS SOL.	(NaPo₃)6		8, 9, 10, 11
HEXAMETA				
SODIUM PLUMBITE	AQUEOUS SOL.			С
SODIUM SULFATE	AQUEOUS SOL.	Na2SO4		A, 8, 9, 10, 11
SODIUM SULFIDE	AQUEOUS SOL.	Na ₂ S		C, 8, 9, 10, 11
SODIUM SULFITE	AQUEOUS SOL.	Na ₂ SO ₃		A, 8, 9, 10,11
SODIUM THIOSULFATE	AQUEOUS SOL.	Na2S2O3.5H2O		8, 9, 10, 11
STANNIC CHLORIDE	AQUEOUS SOL.			11, 12
STANNOUS CHLORIDE	AQUEOUS SOL.	SnCl ₂		11, 12
STARCH		(C6H10O5)x		A, B



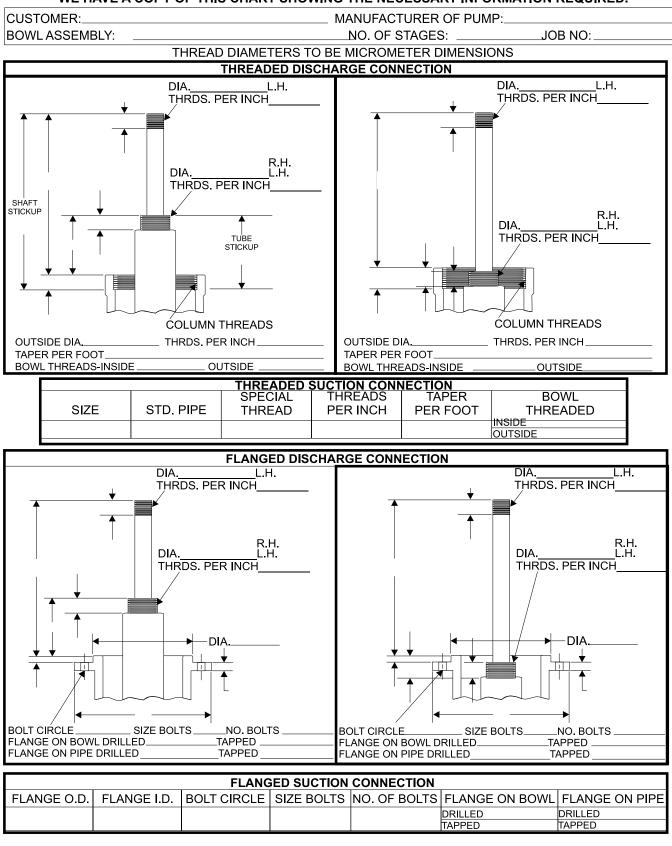
COLUMN 1 LIQUID	COLUMN 2 CONDITIONS OF LIQUID	COLUMN 3 CHEMICAL SYMBOL	COLUMN 4 SPECIFIC	COLUMN 5 MATERIAL SELECTION
	STRONTIUM NITRATE		AQUEOUS SOL.	
SUGAR	AQUEOUS SOL.			A, 8, 9, 10, 11, 13
SULFITE LIQUOR	(SEE LIQUOR, PULP MILL)			
SULFUR	IN WATER	S		A, C, 8, 9, 10, 11
SULFUR	MOLTEN	S		С
SULFUR CHLORIDE	COLD	S2CI2		С
SYRUP	(SEE SUGAR)			
TALLOW	НОТ		0.99	С
TANNING LIQUORS				A, B, 9, 10, 11, 12, 14
TAR	НОТ			C, 3
TAR AND AMMONIA	IN WATER			С
TETRACHLORIDE OF TIN	(SEE STANNIC CHLORIDE)			
TETRAETHYL LEAD		Pb(C2H5)4	1.66	B, C
TOLUENE (TOLUOL)		C7H8	0.87	B, C
TRICHLOROETHYLENE		C2HCI3	1.47	A, B, C, 8
URINE				A, 8, 9, 10, 11
VARNISH				A, B, C, 8, 14
VEGETABLE JUICES				A, 8, 9, 10, 11, 14
VINEGAR				A, 8, 9, 10, 11, 12
VITRIOL BLUE	(SEE COPPER SULFATE)			
VITRIOL, GREEN	(SEE FERROUS SULFATE)			
VITRIOL, OIL OF	(SEE ACID, SULFURIC)			
VITRIOL, WHITE	(SEE ZINC SULFATE)			
WATER, BOILER FEED	NOT EVAPORATE pH>8.5		1.00	С
WATER, BOILER FEED	HIGH MAKEUP pH<8.5			В
	LOW MAKEUP			
WATER, BOILER FEED	EVAPORATED, ANY pH		1.00	4, 5, 8, 14
WATER, DISTILLED	HIGH PURITY		1.00	A, 8
WATER, DISTILLED	CONDENSATE			A, B
WATER, FRESH				В
WATER, MINE	(SEE ACID, MINE WATER)		_	
WATER, SALT AND SEA	(SEE BRINES)			
WHISKEY				A, 8
WHITE LIQUOR	(SEE LIQUOR, PULP MILL)			
WHITE WATER	PAPER MILL			A, B, C
WINE				A, 8
WOOD PULP (STOCK)				A, B, C
WOOD VINEGAR	(SEE ACID PYROLIGNEOUS)			
WORT	(SEE BEER WORT)			
XYLOL (XYLENE)		C8H10	0.87	B, C, 8, 9, 10, 11
YEAST				А, В
ZINC CHLORIDE	AQUEOUS SOL.	ZnCl ₂		9, 10, 11, 12
ZINC SULFATE	AQUEOUS SOL.	ZnSO4		A, 9, 10, 11



ENGINEERING

ADAPTING NATIONAL PUMP BOWL ASSEMBLIES TO SPECIAL COLUMNS

MACHINING DATA REQUIREMENTS: NO MACHINE WORK CAN BE DONE ON A REPLACEMENT BOWL UNTIL WE HAVE A COPY OF THIS CHART SHOWING THE NECESSARY INFORMATION REQUIRED.





"N-260" DISCHARGE HEADS

CAST IRON DISCHARGE HEAD 175 PSI MAXIMUM DISCHARGE PRESSURE

"N-260" discharge head assemblies include the following:

PRODUCT-LUBRICATED

Cast iron head, 416 S.S. top shaft, C-1045 steel headshaft through motor, acrylic graphite packing, bronze gland and bearing, headshaft nut, lock screws, gib key, threaded shaft coupling below motor, cast iron top column flange, bolts, nuts, and gaskets as required. Pre-lubrication system not included.

- A. Manual water pre-lube system consists of 30 gal. min. tank, manual shut-off valve, and necessary fittings.
- B. Automatic water pre-lube system consists of 30 gal. min. tank, solenoid valve (specify voltage), and necessary fittings.
- C. Specify which is required when ordering (manual or automatic).
- D. IMPORTANT: 5 foot top and bottom column assemblies required on all product lube pumps. When pumping water level is greater than 50' pre-lube system is required.

OIL-LUBRICATED

Same as product lubricated except the stuffing box is replaced with a tube tension assembly and a manual oiler with oil pot. Head/topshaft is one piece or two piece steel with steel coupling; specify which is required when ordering.

A. For automatic oil lube system with solenoid valve (specify voltage).

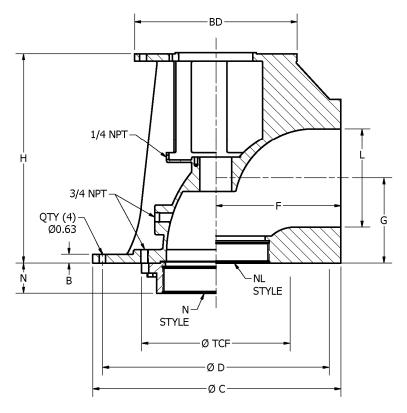
PRODUCT & OIL LUBRICATED

- A. For size other than "L" on the dimension print, a female threaded reducing companion flange with gasket, nuts, and bolts is furnished.
- B. Combination drive headshafts available.
- C. Contact factory for use with solid shaft drivers and/or mechanical seals!

NOTE: For threaded column pipe connection on the Model NL8 and NL10 Discharge Head, Top Column Flange is not required.



DIMENSIONS "N-260" DISCHARGE HEAD



THREADED COLUMN

MODEL	DRIVER BD	COL.	MAX. SHAFT				DIMENS	IONS IN	INCHES				WEIGHT
MODEL	DRIVER DD	SIZE	SIZE	В	С	D	F	G	Н	L	Ν	TCF	LBS
N4	10 & 12	3, 4		0.75	16.00	14.25	8.50	5.38	15.75	4.00	2.00	7.50	195
N6	10, 12 & 16.5	5, 6		0.75	19.00	17.00	9.75	6.75	17.25	6.00	2.50	9.75	245
N8	10, 12 & 16.5	6, 8	1.69	0.75	25.00	23.00	12.50	6.75	19.25	8.00	3.75	11.25	275
NL8	10, 12 & 16.5	8	1.09	0.75	25.00	23.00	12.50	6.75	19.25	8.00	-	-	275
N10	10, 12 & 16.5	8, 10		0.88	25.00	23.00	12.69	8.63	21.25	10.00	3.06	15.13	350
NL10	10, 12 & 16.5	10		0.88	25.00	23.00	12.69	8.63	19.25	10.00	-	-	350

MAXIMUM SETTING DEPTH AND MINIMUM WELL CASING

MODEL			MAX. STETTING FEET ⁽¹⁾				
MODEL	COLUMN	OIL LUBE	PRODUCT LUBE	CASING ⁽²⁾			
N4	3	280	330	8.00			
114	4	230	250	8.00			
N6	5	330	375	10.00			
INO	6	240	280	10.00			
N8	6	370	410	12.00			
INO	8	270	320	12.00			
NL8	8	270	320	10.00			
N10	8	260	300	16.00			
NIU	10	210	250	16.00			
NL10	10	210	210	12.00			
NOTE:							

(1) SETTING DEPTH BASED ON NATIONAL PUMP COMPANY STANDARD PIPE WALL THICKNESS PIPE, CONTACT FACTORY WHEN USING HEAVIER PIPE. (2) MIN. CASING SIZE WHEN CASING IS FLUSH WITH FOUNDATION.

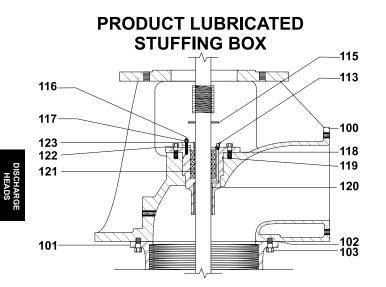
MAXIMUM POWER RATING

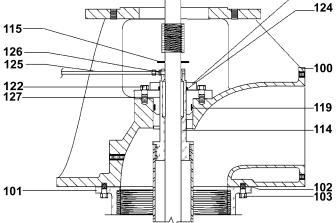
MODEL	3600 RPM	1800 RPM	1200 RPM
N4	60	40	20
N6	125	60	40
N8	200	100	60
NL8	200	100	60
N10	250	200	125
NL10	250	200	125

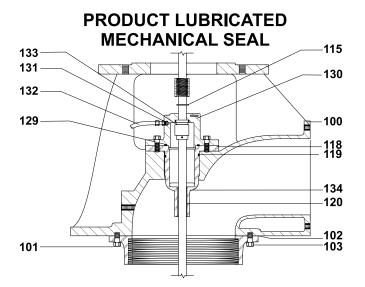
CONTACT FACTORY FOR HIGHER RATINGS



"N-260" DISCHARGE HEAD







ITEM	PART DESCRIPTION	MATERIAL
100	DISCHARGE HEAD	CLASS 30 GREY IRON
101	TOP COLUMN FLANGE	CLASS 30 GREY IRON
102	TOP COLUMN FLANGE GASKET	VELLUMOID
103	TOP COLUMN CAP SCREW	GRADE 5 STEEL
113	GREASE ZERK	SAE J534 STEEL
114	TENSION BEARING	C-844 BRONZE
115	SLINGER	RUBBER
116	PACKING GLAND STUD	18.8 S.S.
117	GLAND STUD NUT	18.8 S.S.
118	STUFFING BOX	CLASS 30 GREY IRON
119	STUFFING BOX "O" RING	BUNA - N
120	STUFFING BOX BEARING	C-844 BRONZE
121	STUFFING BOX PACKING	TEFLON

ITEM	PART DESCRIPTION	MATERIAL
122	STUFFING BOX CAP SCREW	GRADE 5 STEEL
123	PACKING GLAND	C-844 BRONZE
124	LOCK NUT "O" RING	BUNA - N
125	COPPER TUBING	COPPER
126	FERRULE FITTING	ASA J512 BRASS
127	TENSION NUT	DUCTILE IRON
128	LOCK NUT	CLASS 30 GREY IRON
129	SEAL GLAND CAP "O" RING	RUBBER
130	MECHANICAL SEAL GLAND CAP	CAST IRON
131	TUBING CONNECTOR	BRASS
132	COPPER TUBING	COPPER
133	JOHN CRANE MECHANICAL SEAL	SPECIFY MATERIAL
134	MECHANICAL SEAL RETAINER	CAST IRON



HI - PRO DISCHARGE HEAD

"HI - PROFILE" CAST IRON DISCHARGE HEAD

"Hi-Profile" discharge head assemblies include the following:

PRODUCT-LUBRICATED

Cast iron head, 416 S.S. top shaft, C-1045 steel headshaft thru motor, acrylic graphite packing, bronze gland and bearing, headshaft nut, lock screws, gib key, threaded shaft coupling below motor, ductile iron top column flange, bolts, nuts, and gaskets as required. Pre-lubrication system not included.

- A. Manual water pre-lube system consisting of 30 gal. min. tank, manual shut-off valve, and necessary fittings available.
- B. Automatic water pre-lube system consisting of 30 gal. min. tank, solenoid valve (specify voltage), and necessary fittings available.
- C. Add for high pressure stuffing box when pressure at stuffing box exceeds 175 PSI.
- D. IMPORTANT: 5 foot top and bottom column assemblies required on all product lube pumps. When pumping water level is greater than 50' pre-lube system is required.

OIL-LUBRICATED

Same as product lubricated except the stuffing box is replaced with a standard tube tension and a manual oiler with oil pot. Head/topshaft is one piece or two piece steel with steel coupling; specify which is required when ordering.

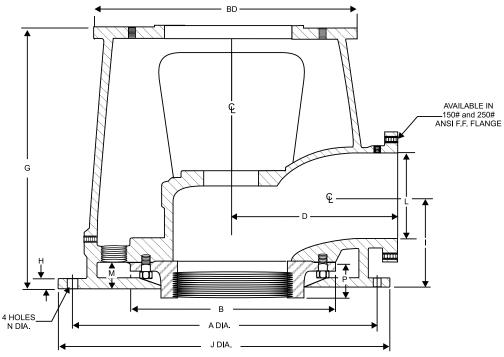
A. Automatic oil lube system with solenoid valve available (specify voltage).

PRODUCT AND OIL LUBRICATED

- A. For size other than "L," on the dimension print, a female threaded reducing companion flange with gasket, nuts, and bolts is furnished.
- B. Combination drive headshafts available as adder.
- C. Contact factory for use with solid shaft drivers and/or mechanical seals.
- D. Max. shaft size for any combination is 2-3/16".



DIMENSIONS "HI - PROFILE" DISCHARGE HEAD



MODEL	BD	Α	В	D	G	Н	I	J	L	М	N	WEIGHT
16 X 6	16-1/2, 20	20-1/2	11	13	21-1/2	1"	9	22	6	2-1/4	7/8	400
16 X 8	16-1/2, 20	23	15	13 - 1/2	22 - 1/2	1"	9	24 - 1/2	8	2-1/4	7/8	450
16 X 10	16-1/2, 20	25	17	14-7/8	24-1/2	1"	10-1/2	26-1/2	10	2-1/4	7/8	560
20 X 12	20	24	17	15	29	1-1/8"	12	27	12	2-3/4	1-1/4	685

MODEL	DISCH. SIZE	COLUMN	Р	MIN. WELL CASING (3)	MAX. SETTING D.I.TCF	MAX. SHAFT Size	RPM	HORSE POWER	MAX. THRUST	
		5"	3-15/16	10"	1100'		3600	800	20,000	
16 X 6	6"	6"	3-15/16	10"	1000'	2-3/16"	1800	700	20,000	
							1200	475	20,000	
		6"	3-15/16	10"	1000'		3600	800	20,000	
16 X 8	8"	8"	4-3/16	12"	800'	2-3/16"	1800	700	20,000	
		10"	4-15/16	16"	700'		1200	475	20,000	
		8"	2-5/16	12"	800'		3600	800	20,000	
16 X 10	10"	10"	3-1/16	14"	700'	2-3/16"	1800	700	20,000	
		12"	3-1/16	16"	500'		1200	475	20,000	
								3600	500	13,000
20 X 12	12"	12"	." 3-1/16	16"	500'	2-3/16"	1800	435	13,000	
							1200	300	13,000	

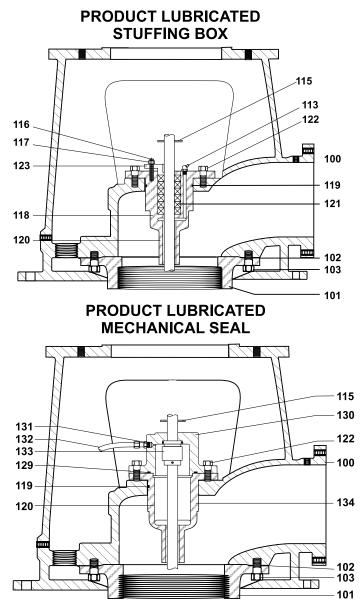
1. 16" min. casing required when allowing casing to stick up 1-7/8" max. above foundation pad without grout plate for 16 x 8.

2. 18" min. casing required when allowing casing to stick up 1-7/8" max. above foundation pad without grout plate for 16 x 10.

3. Referring to chart; min. casing size when casing is flush with foundation pad.

4. Head should be raised by lifting lugs ONLY. If necessary to insure stabilization, secure lifting strap to top of base to prevent tilting.

"HI - PROFILE" DISCHARGE HEAD

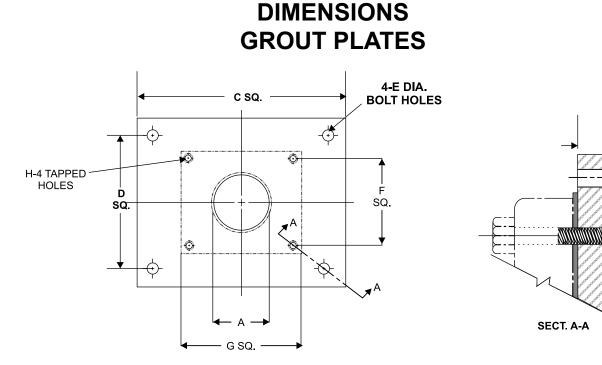


	OIL LUBRICATED
	128
126	
127	
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ITEM	PART DESCRIPTION	MATERIAL
122	STUFFING BOX CAP SCREW	GRADE 5 STEEL
123	PACKING GLAND	C844 BRONZE
124	LOCK NUT "O" RING	BUNA - N
125	COPPER TUBING	COPPER
126	FERRULE FITTING	ASA J512 BRASS
127	TENSION NUT	DUCTILE IRON
128	LOCK NUT	CLASS 30 GREY IRON
129	SEAL GLAND CAP "O" RING	RUBBER
130	MECHANICAL SEAL GLAND CAP	CAST IRON
131	TUBING CONNECTOR	BRASS
132	COPPER TUBING	COPPER
133	JOHN CRANE MECHANICAL SEAL	SPECIFY MATERIAL
134	MECHANICAL SEAL RETAINER	CAST IRON

ITEM	PART DESCRIPTION	MATERIAL
100	DISCHARGE HEAD	CLASS 30 GREY IRON
101	TOP COLUMN FLANGE	CLASS 60 DUCTILE IRON
102	TOP COLUMN FLANGE GASKET	VELLUMOID
103	TOP COLUMN CAP SCREW	GRADE 5 STEEL
113	GREASE ZERK	SAE J534 STEEL
114	TENSION BEARING	C844 BRONZE
115	SLINGER	RUBBER
116	PACKING GLAND STUD	18.8 S.S.
117	GLAND STUD NUT	18.8 S.S.
118	STUFFING BOX	CLASS 30 GREY IRON
119	STUFFING BOX "O" RING	BUNA - N
120	STUFFING BOX BEARING	C844 BRONZE
121	STUFFING BOX PACKING	ACRYLIC GRAPHITE





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DISCHARGE HEAD & B.D.		DIMENSIONS IN INCHES							
	A *	в	с	D	Е	F	G	н	
N4-260	9	1	16	13-1/4	3/4	10	16 (1)	1/2-13UNC	55
N6-260	12	1	19	16	3/4	12	19 (1)	1/2-13UNC	70
N8-10-260	17	1	25	22	7/8	16-1/4	25 (1)	1/2-13UNC	140
HiPRO 16 x 6	13	1	24	21	7/8	14-1/2	22 (1)	3/4-10UNC	125
HiPRO 16 x 8	17	1	25	22	7/8	16-1/4	24-1/2 (1)	3/4-10UNC	140
HiPRO 16 x 10	19	1-1/4	27	24	1-1/8	17-11/16	26-1/2 (1)	3/4-10UNC	185
HiPRO 20 x 12	19	1-1/4	39	35	1-1/4	17	26-1/2 (1)	1-1/8-7UNC	440
NF3-4x10-12	11	1	21	18-1/2	3/4	13	16	5/8-11UNC	120
NF3-4x16-1/2	13	1	24	21-1/2	7/8	16	19	3/4-10UNC	155
NF5-6x10-12	11	1	21	18-1/2	3/4	13	16	5/8-11UNC	120
NF5-6x16-1/2	13	1	24	21-1/2	7/8	16	19	3/4-10UNC	155
NF8x10-12	14	1	23	20-1/2	7/8	15	18	5/8-11UNC	130
NF8x16-1/2	14	1-1/4	27	23-1/2	1-1/8	18	21	3/4-10UNC	200
NF8x20	19	1-1/4	31	27-1/2	1-1/8	22	25	3/4-10UNC	285
NF10x16-1/2	19	1-1/4	31	27-1/2	1-1/8	22	25	3/4-10UNC	285
NF10x20	19	1-1/4	33	29-1/2	1-1/8	24	27	3/4-10UNC	340
NF10x24-1/2	19	1-1/4	34	30-1/2	1-1/8	25	28	7/8-9UNC	390
NF12x16-1/2	19	1-1/4	31	27-1/2	1-1/8	22	25	3/4-10UNC	285
NF12x20	19	1-1/4	33	29-1/2	1-1/8	24	27	3/4-10UNC	340
NF12x24-1/2	19	1-1/4	38	34	1-1/4	27	30	7/8-9UNC	400

1. THESE HEADS HAVE ROUND BASE. ALL THE OTHERS ARE SQUARE.

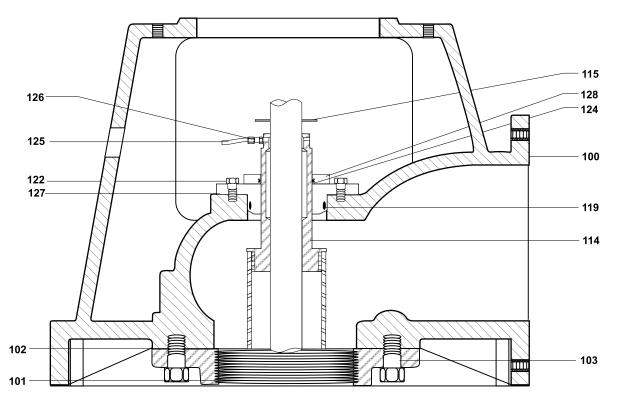
Steel plate machined on one side to match machined bottom of head and steel cap screws for securing head to plate. (Anchor bolts by others.) Contact factory for dimension variations or larger sizes.

*Ensure largest diameter component will pass through this hole. Larger I.D. holes cane used if necessary.



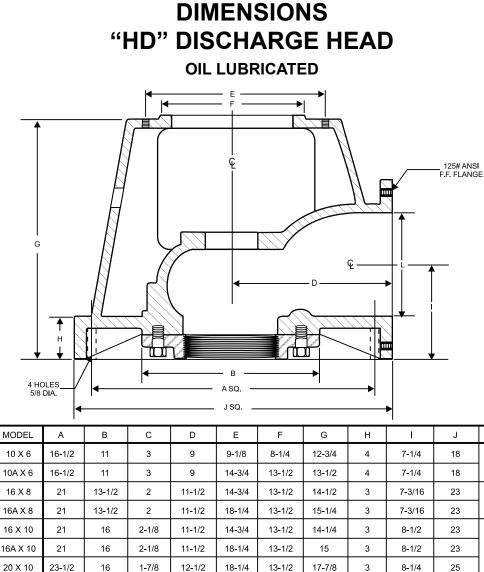
"HD" DISCHARGE HEAD

OIL LUBRICATED ONLY 175 PSI MAXIMUM DISCHARGE PRESSURE



ITEM	PART DESCRIPTION	MATERIAL
100	DISCHARGE HEAD	CLASS 30 GREY IRON
101	TOP COLUMN FLANGE	CLASS 30 GREY IRON
102	TOP COLUMN FLANGE GASKET	VELLUMOID
103	TOP COLUMN CAP SCREW	GRADE 5 STEEL
114	TENSION BEARING	C844 BRONZE
115	SLINGER	RUBBER
119	TENSION NUT "O" RING	BUNA - N
122	TENSION NUT CAP SCREW	GRADE 5 STEEL
124	LOCK NUT "O" RING	BUNA - N
125	COPPER TUBING	COPPER
126	FERRULE FITTING	ASA J512 BRASS
127	TENSION NUT	DUCTILE IRON
128	LOCK NUT	CLASS 30 GREY IRON





L

6

8

10

12

	2.)-1/Z	- I	0	1-77	0	12-1/2	10-1/4	13-1/2		17-170		3		5-1/4		25
)	23	8-1/2	1	6	1-7/	/8	12-1/2	18-1/4	13-1/2	,	18-5/8		3	8	3-1/4		25
	30)-1/2	1	9	1-7	/8	16-1/4	18-1/4	13-1/2	2	20-5/8		4		12	32	2-1/2
				COL	.UMN			SHAFT			DRIVE	٦	MAX (1)	WEIGH	т	
		MOE	DEL	SIZ	ZES			SIZE			BD	5	SETTI	٩G	LBS.		
		10 >	Κ6		- 0						10		500'		356		
		10A	X 6	4,:	5,6			1, 1-1/4			16-1/2		500'		386		
		16 >	K 8	5 (2 0		1 1 1/	4 1 1/0 1	11/16		16-1/2		600'		568		
		16A	X 8	5, 6	6, 8		1, 1-1/4	4, 1-1/2, 1-	11/10		20		600'		635		
		16 X	10								16-1/2		300'		483		
		16A X	K 10								20		300'		535		
		20 X	10	8,	10		1, 1-1/4, 1-	1/2, 1-11/16	5, 1-15/16		20		600'		848		
		20A X	(10								24		600'		943		
		24 X	12	1	2	1	-1/4, 1-1/2,	1-11/16, 1- [.]	15/16,2-3/16		24		800'		1,460		

ALL DIMENSIONS ARE IN INCHES EXCEPT (1)

1. Includes: Cast iron discharge head, top column flange, make up tube assembly, C-1045 steel headshaft, key adjusting nut, bolts, nuts and gaskets as required, manual oiler with oil pot.

2. Automatic oil lube system with solenoid available.

3. Combination drive headshafts available.

20A X 10 24 X 12

4. Contact factory for grout plates.

5. For size other than "L" on the dimension print, a female threaded reducing companion flange with gasket, nuts, and bolts is available.

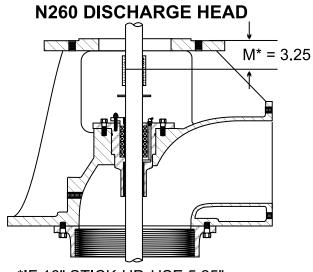
6. Contact factory for use with solid shaft drivers.



HEAD SHAFT LENGTHS

DRIVER "CD" + M + NUT ALLOWANCE

 \square



*IF 16" STICK-UP, USE 5.25" FOR N8, NL8, & N10

HI-PRO DISCHARGE HEAD

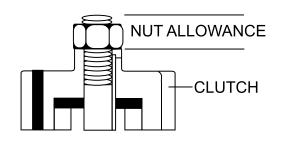
TOP SHAFT LENGTH OF 26" MUST BE ADDED TO THE HEAD SHAFT IF HEAD SHAFT IS TO EXTEND BELOW THE DISCHARGE HEAD BASE.

HD DISCHARGE HEAD

"HD" DISCHARGE HEAD TWO PIECE HEADSHAFT REQUIRES MOTOR STAND

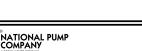
				3.12 5.75
1	6)	(1() = (15.50

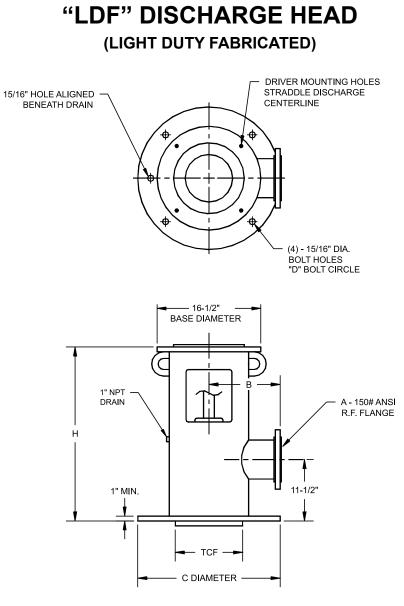
20 X 10 = 20.25 25 X 12 = 22.00



NUT ALLOWANCES FOR:

1" DIA. SHAFT = 2" 1-1/4" DIA. SHAFT = 2-1/2" 1-1/2" DIA. SHAFT = 2-1/2" 1-11/16" DIA. SHAFT = 3" 1-15/16" DIA. SHAFT = 3" 2-3/16" DIA. SHAFT = 3-1/2"





DIMENSIONS

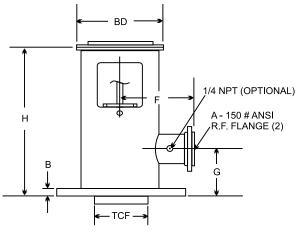
	DIMENSIONS IN INCHES												
DISCHARGE SIZE A	В	С	D	н	TCF	APPROX. WEIGHT							
4	10	20	15-3/8	27-1/2	7-1/2	242							
6	10	20	15-3/8	27-1/2	9-3/4	244							
8	10	20	15-3/8	27-1/2	11-1/4	252							
10	11	22	17-1/4	32	15-1/8	275							
12	12	24	19-1/4	32	17	295							

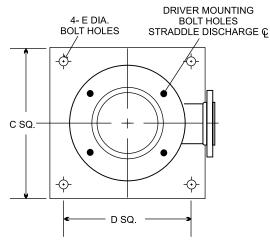
1. Dimensions are for standard construction. Special designs and dimensions are not available with this particular discharge head.

2. Standard construction heads are rated for 275 PSI working pressure. For higher pressure ratings, contact factory.



DIMENSIONS "NF" DISCHARGE HEAD





				DIME	NSIONS IN	INCHES						
DISCHARGE									H (1)			WEIGHT
SIZE A(2)	DRIVER BD	В	C (3)	D	E	F	G	H ₁	H ₂	H ₃	TCF	LBS.
3, 4	10 or 12	1-1/2	16	13	3/4	9	8	23	26	30	9	340
3, 4	16-1/2	1-1/2	19	16	7/8	11	8	23	27	31	9	410
5	10 or 12	1-1/2	16	13	3/4	10	9	24	27	31		360
5	16-1/2	1-1/2	19	16	7/8	12	9	24	28	32	10	430
6	10 or 12	1-1/2	16	13	3/4	10	10	26	29	33		380
0	16-1/2	1-1/2	19	16	7/8	12	10	26	30	34		430
	10 or 12	1-1/2	18	15	3/4	11	11	29	32	36		420
8	16-1/2	1-1/2	21	18	7/8	13	11	29	33	37	15	480
	20	1-1/2	25	22	7/8	14	11	29	33	37		570
	16-1/2	1-3/4	25	22	7/8	14	12	33	37	41		610
10	20	1-3/4	27	24	7/8	15	12	33	37	41		670
	24-1/2	1-3/4	28	25	1	19	12	33	39	43	17	730
	16-1/2	1-3/4	25	22	7/8	15	14	36	40	44		770
12	20	1-3/4	27	24	7/8	16	14	36	40	44		950
	24-1/2	1-3/4	30	27	1	20	14	36	42	46		970

- 1. "H" Standard dimension when shaft coupling as outlined below is used. This dimension may vary at factory option.
 - "H1" For standard headshaft with or without the threaded lineshaft coupling below hollow shaft driver. With threaded coupling and mechanical seal configuration, a lower steady bushing is required in the driver.
 - "H₂" For adjustable or rigid flanged coupling.
 - "H₃" For adjustable flanged spacer coupling
- 2. Victaulic or plain end discharge is available for no additional charge.
- 3. Dimensions are for standard construction. For special designs and dimensions, consult factory.

A. "NF" discharge head assemblies include the following:

<u>Product Lubricated:</u> Fab. steel head with square base, 416S.S. top shaft, C-1045 steel headshaft thru motor, Teflon packing, bronze gland and bearing, headshaft nut, lock screws, gibkey, threaded shaft coupling below motor, cast iron top column flange, bolts, nuts, and gaskets as required. Pre-lubrication system not included.

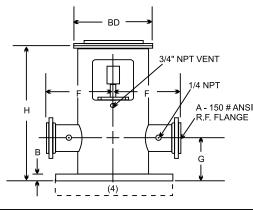
<u>Oil Lubricated:</u> Same as product lubricated except the stuffing box is replaced with a standard tube tension assembly and a manual oiler with oil pot. Head/topshaft is one piece or two piece steel with steel coupling; specify which is required when ordering.

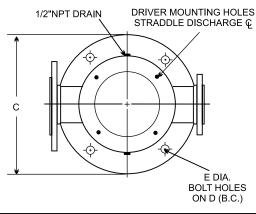
- B. Extra head height is required when using a solid shaft driver, flanged coupling, and/or mechanical seal.
- C. High pressure packing box is required when pressure at packing box exceeds 175 PSI.
- D. Plain end discharge or discharge with victaulic coupling groove available.
- E. Standard construction head is rated for 275 PSI working pressure. For higher pressure rating, contact factory.
- F. Manual pre-lubrication system, automatic pre-lubrication system, and automatic oil lubrication system available.

API COMPLIANCE FOR DISCHARGE HEADS AVAILABLE.



DIMENSIONS "NTF" DISCHARGE HEAD





				DIM	IENSION	S IN INCH	IES						
BARREL		DISCH.	SUCTION			D	Е				H (1)		APPROX WT
SIZE	DRIVER BD	SIZE DS	SIZE SS	B MIN.	C (3)	(B.C.)	QTY.	F	G	Η₁	H₂	H₃	
8-5/8	10 ar 12	3 or 4	4	1-1/8	13-1/2	11-3/4	7/8	10	6-1/2	22-1/2	26-1/2	31-1/2	240
0-0/0	10 or 12	4 or 6	6	1-1/0	13-1/2	11-3/4	8	10	8-1/2	26-1/2	28-1/2	33-1/2	263
10-3/4	10, 12 or	4 or 6	6	1-3/16	16	14-1/4	1	10	8-1/2	26-1/2	29-1/2	34-1/2	290
10-3/4	16-1/2	6 or 8	8	1-3/10	10	14-1/4	12		10-1/2	29-1/2	32-1/2	37-1/2	365
12-3/4	12 or 16-1/2	4 or 6	6	1-1/4	19	17	1	10	8-1/2	26 - 1/2	29-1/2	34-1/2	390
12-3/4	12 01 10-1/2	6 or 8	8	1-1/4	19	17	12	12	10-1/2	29 - 1/2	32-1/2	37-1/2	410
14	12, 16-1/2 or	4 or 6	6	1-3/8	21	18-3/4	1-1/8	10	8-1/2	26 - 1/2	29-1/2	34-1/2	410
	20	6 or 8	8	1-3/0	21	10-3/4	12	12	10-1/2	29 - 1/2	32-1/2	37-1/2	440
16	16-1/2 or 20	4 or 6	6	1-7/16	23-1/2	21-1/4	1-1/8		10-1/2	26-1/2	29-1/2	34-1/2	410
10	10-1/2 01 20	6 or 8	8	1-7/10	23-1/2	21-1/4	16	14	11-1/2	29-1/2	32-1/2	37-1/2	440
18	16-1/2, 20 or	6 or 8	8	1-9/16	25	22.2/4	1-1/4	10	10-1/4	29-1/4	32-1/4	37-1/4	440
	24-1/2	8 or 10	10	1-9/10	20	22-3/4	16	16	11-1/4	32-1/4	35-1/4	40-1/4	680
20	20, 24-1/2 or	6 or 8	8	1-11/16	27-1/2	25	1-1/4	10	10-1/4	29-1/4	32-1/4	37-1/4	680
20	30-1/2	8 or 10	10	1-11/10	27-1/2	25	20	16	11-1/4	32-1/4	35-1/4	40-1/4	780
24	20, 24-1/4 or	8 or 10	10	1 7/0	22	20 1/2	1-3/8	10	11-1/4	32-1/4	35-1/4	40-1/4	720
	30-1/2	10 or 12	12	1-7/8	32	29-1/2	20	18	13-1/4	36-1/4	39-1/4	45-1/4	898
30	20, 24-1/2 or	8 or 10	10	2-1/8		20	1-3/8		13	32	35	40	720
	30-1/2	10 or 12	12	2-1/0	38-3/4	36	38	22	14	36	39	45	898

1. "H" - Standard dimension when shaft coupling as outlined below is used. This dimension may vary at factory option.

- "H1" For standard headshaft with or without the threaded lineshaft coupling below hollow shaft driver. With threaded coupling and mechanical seal configuration, a lower steady bushing is required in the driver.
- "H₂" For adjustable or rigid flanged coupling.
- "H₃" For adjustable flanged spacer coupling
- 2. Standard construction is designed with the suction and discharge flanges on the same horizontal centerline and located 180° apart. Other locations may be furnished if required. Standard suction and discharge flanges are 150# A.N.S.I. flanges. Victaulic or plain end discharge is available for no additional charge.
- 3. Dimensions are for standard construction. For special designs and dimensions, contact the factory.

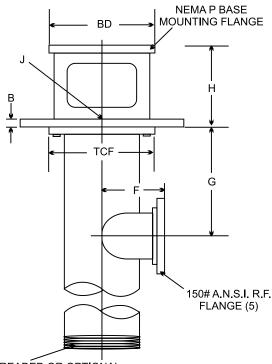
Type "NTF" discharge head assemblies include the following parts: Fabricated steel discharge head with 150# raised face suction and discharge flanges, standard stuffing box assembly with a bronze bearing, head shaft, head shaft nut, lock screws, gib key, threaded shaft coupling below motor. Also, bolts, nuts, and gaskets, as required.

- A. Standard construction head has 150# discharge flange (rated for 275 PSIG) 300# discharge flange is available. For higher pressure ratings, contact factory. Pressure ratings are based on A.N.S.I. flange rating for 20° to 100°f, water service.
- B. High pressure packing box assembly required when pressure at packing box exceeds 175 PSI. When pressure exceeds 300 PSIG, contact factory.
- C. Extra height required when using a solid shaft driver with a flanged coupling and/or mechanical seal.
- D. For larger shaft sizes contact factory.
- NOTE: Suction barrel must be selected for service and/or suction pressure.

API COMPLIANCE FOR DISCHARGE HEADS AVAILABLE.



DIMENSIONS "NUF" DISCHARGE HEAD



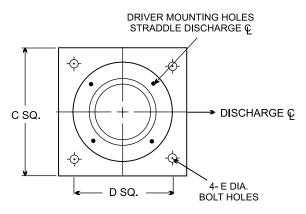
A- THREADED OR OPTIONAL FLANGED COLUMN BELOW TEE

A	В	C (1)	D	E	F	MIN. G (2)	J (3)	MAX. TCF	MIN. HOLE (4)	APPROX. WT. **
4	1-1/4	15	13	3/4	6	8	1/2	9	11	110
5	1-1/4	20	17	3/4	6	9	1/2	10	13	160
6	1-1/4	20	17	3/4	7	9-1/2	3/4	11	14-1/2	190
8	1-1/4	26	23	7/8	9	10	3/4	13-1/2	18	285
10	1-1/2	26	23	1	10-1/2	11	1	16	21	410
12	1-1/2	30	27	1	11-1/2	13	1	19	24	550

- "H" Standard dimension when shaft coupling as outlined below is used. This dimension may vary at factory option.
 - "H₁" -For standard headshaft with or without the threaded lineshaft coupling below hollow shaft driver. With threaded coupling and mechanical seal configuration, a lower steady bushing is required in the driver.
 - "H2" -"H3" -For adjustable or rigid flanged coupling.
 - For adjustable flanged spacer coupling
- 1. "C" is determined by the size of the column pipe except when "BD" required larger min. "C" as indicated.
- 2 Minimum for fabrication. Will probably increase due to mounting structure.
- N.P.T. for automatic air release valves.
- 4 Standard flanged discharge tee will pass through this diameter opening, IF lateral movement is possible during installation. All column above the tee must be flanged and may be

supplied smaller at factory option. Discharge size can not exceed column size at the tee.

5. Optional victaulic groove or plain end discharge available for no additional charge.



BD		H★		MIN.C	APPROX.
00	H_1	H_{2}	H_{3}	(1)	WT.*
10 OR 12	13	16	20	15	230
16-1/2	14	17	21	20	350
20	14	17	21	26	425
24-1/2	15	18	22	30	600

PEDESTAL

5 FT. COLUMN AND DISCHARGE ELBOW

1. "NUF" Type Underground Discharge Head Assemblies include the following:

Product Lubricated: Fabricated steel motor stand, standard stuffing box with bronze bearing, headshaft, headshaft nut, lock screws, gibkey, threaded shaft coupling below motor, bolts, nuts, and gaskets, as required. 150# discharge flange welded into the column as required (6). Pre-lubrication system not included (7).

Oil Lubricated: Same as product lubricated except the stuffing box is replaced with a standard tube tension assembly and a manual oiler with oil pot (7).

Extra height required when using a solid shaft driver with a flanged coupling. High pressure stuffing box required when pressure at the box exceeds 175

- PSI. Standard steel fabrications are rated for 275 PSI working pressure. 3. Automatic air release valves are required on all "NUF" heads. 1/2" and 3/4"
- are 150 PSI; 1" is 300 PSI.
- 4. Optional Plain end discharge or victaulic groove available for no additional charge..
- 5. Manual pre-lube system, Automatic pre-lube system and Automatic oil lube system available.

NOTE: All column above discharge head tee must be welded/flanged column pipe.

API COMPLIANCE FOR DISCHARGE HEADS AVAILABLE.

2



SUCTION BARREL SIZE SELECTION

RECOMMENDED CAPACITY IN USGPM*

NOMINAL					B	ARREL SIZ	Έ				
BOWL SIZE	8	10	12	14	16	18	20	24	30	36	42
6	340	780									
7	180	625	1160								
8		440	980	1370							
10			540	925	1620	2420					
11			280	670	1360	2160					
12				385	1085	1880	2775				
14					450	1240	2140	4420	7895		
16						510	1400	3480	6325		
18							570	2795	6330		
20									5800	10700	
24										8600	14200

*Recommended Capacity Based on a Fluid Velocity of 5 Ft./Sec.

- ▶ If flanged column is used, the flange diameter should not be larger than the bowl diameter.
- If a suction fitting on the suction barrel is located below the bowl assembly, the above chart can be disregarded. Use the barrel size next larger than the bowl assembly.

SUCTION BARREL WALL THICKNESS

BARREL SIZE		G RATING L SHELL		IG RATING _ SHELL	720-1440 PSIG RATING BARREL SHELL			
0.D.	I.D.	WALL	I.D.	WALL	I.D.	WALL		
8-5/8	8.071	0.277	7.981	0.322	7.439	0.593		
10-3/4	10.020	0.365	10.020	0.365	9.314	0.718		
12-3/4	12.000	0.375	11.750	0.500	11.064	0.843		
14	13.250	0.375	13.0000	0.500	12.126	0.937		
16	15.250	0.375	14.312	0.844	13.564	1.218		
18	17.250	0.375						
20	19.250	0.375						
24	23.250	0.375						
30	29.000	0.500						
36	35.000	0.500						
42	40.875	0.562						

FOR LARGER BARREL SIZES THAN SIZES SHOWN, CONTACT THE FACTORY.

FORMULA TO CALCULATE VELOCITY OF FLUID THROUGH BARREL:

- V = Velocity of flow, Ft./Sec. (recommended to be less than 5 Ft./Sec.) Example: 500 GPM, H7HC Bowl Assembly, 10" Barrel
- V = Q/A
 - Q = Capacity, Ft^3 /Sec. (GPM x 0.002228 = Ft^3 /Sec.)
 - A = Non-Restricted flow area, Ft^3

V = Q/A

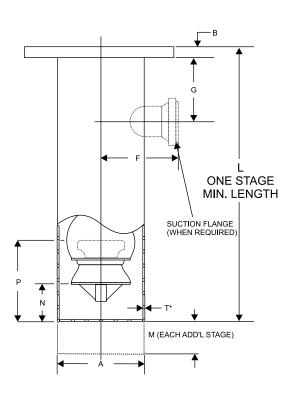
V = 500/Area (Barrel I.D.) - Area (bowl O.D.) V = 1.114 $Ft^3/Sec./(.548 Ft^2 - .279 Ft^2)$ V = 4.1 Ft./Sec.

Velocity does not exceed 5 Ft./Sec. - OK

API COMPLIANCE FOR BARRELS AVAILABLE.

DIMENSIONS SUCTION BARREL

BOWL	DIMENSIONS IN INCHES										
SIZE	L	М	N	Р							
L6	15	3.75	3.84	8.38							
M6	15-1/2	4	3	10							
E6	18	6-1/2	3	10							
J6	16-3/4	4-3/4	4	10							
H7	20	6-3/4	3-1/2	12							
K8	18-1/2	6-1/2	6-1/2	12-1/2							
M8	18-1/2	7-1/4	4	10							
J8	24-1/2	8-7/8	4	14							
M9	19-1/4	8	4	11							
M10	23-1/2	9-5/8	5-1/4	12							
H10	24-1/2	9-5/8	5	13							
J10	24-7/8	9-3/4	5-1/2	13-1/4							
K10	24-1/4	8-7/8	6-7/8	15-3/8							
E10	25-1/4	9-5/8	6	17							
M11	25-1/4	10	6	16-3/4							
J11	24-3/4	9-7/8	6	16-3/4							
E12	25-1/4	10-1/2	6	13							
K12	25-1/4	11-5/16	6	13							
M12	26-1/4	10-1/2	6	13							
H12	32-3/4	12-1/2	6	18							
J12	31-1/4	12-3/8	7	19							
M14	29	13-1/4	7	14							
H14	30-1/2	14-1/8	7	14							
E18	36-1/2	15	9	20							
K20	K20 40		11-1/4	23							
H24	45	21-3/4	18-1/2	23-1/4							



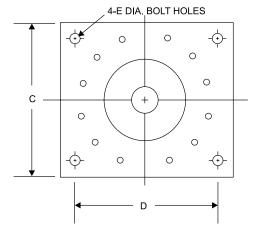
DO NOT USE FOR CONSTRUCTION PURPOSES UNLESS CERTIFIED.

BARREL	WALL			DIMENSION	N IN INCHES			APPROX.
SIZE A	THICKNESS T*	В	С	D	Е	F	G	WT.
8-5/8	0.322	1-1/2	16	14	3/4	10	8	25
10-3/4	0.365	1-1/2	18	16	3/4	10	9	41
12-3/4	0.375	1-1/2	20	17	7/8	12	11	50
14	0.375	1-1/2	23	20	7/8	12	12	55
16	0.375	1-1/2	25	22	7/8	14	13	63
18	0.375	1-3/4	26	23	7/8	16	14	71
20	0.375	1-3/4	29	26	7/8	16	15	79
24	0.375	1-3/4	33	30	1-1/8	18	17	95
30	0.500	2	41	37	1-1/8	22	20	157

1. *Standard barrel wall thickness. For heavier wall construction, consult the factory.

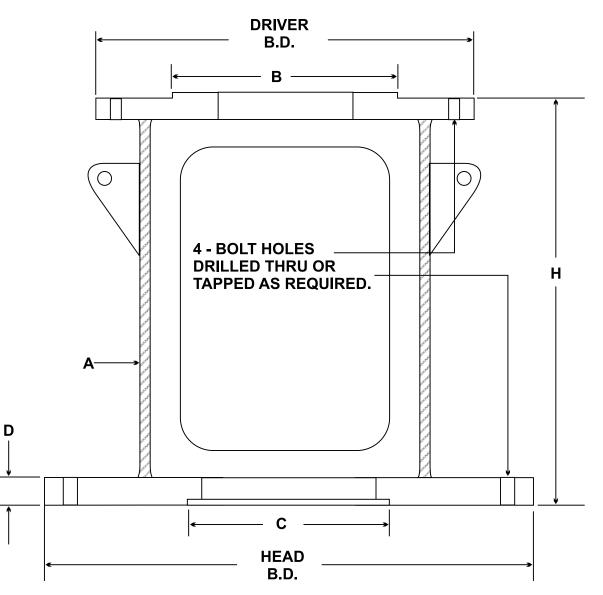
- 2. Pressure rating 275 PSIG for standard construction. Based on temperature range from -20° to 100° F.
- 3. Gaskets will be furnished as standard for pressure ratings not exceeding 275 PSIG.
- 4. O" rings will be furnished as standard for pressure ratings exceeding 275 PSIG.
- Suction barrel includes: barrel with mounting plate (drilled and tapped to match discharge flange bolting -- 150# A.N.S.I.), gasket, and bolts for mounting discharge head. Foundation bolts not included.
- 6. Maximum height of barrel above the floor mounting plate is 5'. For additional height, contact the factory.
- 7. Flanged suction includes: A.N.S.I. raised face flange with nipple welded to the above suction barrel, if required.
- 8. Plain end suction nipple or suction nipple with victaulic coupling groove available.

API COMPLIANCE FOR BARRELS AVAILABLE.





MOTOR STANDS



	DIMENSIONS														
DRIVER	HEAD			н						APPROX.					
B.D.	B.D.	STD. H	MIN.	MAX.	Α	В	С	D	Е	WT.					
10, 12	10, 12	12	4	18	A.R.	8-1/4	8-1/4	7/8	7/8	66					
10,12	16-1/2	12	4	18	A.R.	8-1/4	13-1/2	7/8	1	90					
16-1/2	16-1/2	12	4	24	A.R.	13-1/2	13-1/2	1	1	104					
16-1/2	20	12	4	24	A.R.	13-1/2	13-1/2	1	1	147					
20	20	12	4	24	A.R.	13-1/2	13-1/2	1	1	203					
20	24-1/2	12	4	24	A.R.	13-1/2	13-1/2	1	1-1/8	290					
24-1/2	24-1/2	24	6	30	A.R.	13-1/2	13-1/2	1-1/8	1-1/8	378					
24-1/2	30-1/2	24	6	30	A.R.	13-1/2	22	1-1/8	1-3/8	481					
30-1/2	30-1/2	24	6	30	A.R.	22	22	1-3/8	1-3/8	584					

NOTE: A.R. = AS REQUIRED

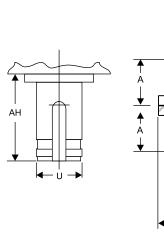
API COMPLIANCE FOR DISCHARGE HEADS AVAILABLE.

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NATIONAL PUMP



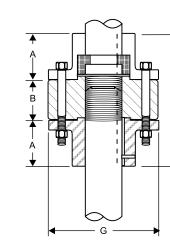
RIGID FLANGE COUPLINGS FOR SOLID SHAFT MOTORS

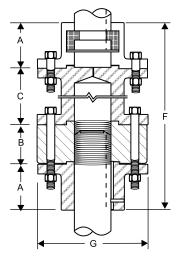




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"AF" COUPLING (2) "AFS" COUPLING (3)





COUPLING	HP@ 1770	HP@ 3550	THRUST CAP.	NEM/	A STD.	DIMENSIONS IN INCHES						
SIZE	RPM	RPM	LBS.	AH	U	Α	В	C*	D	Е	F	G
1	74.34	149.10	4500	2-3/4	1-1/8	2	1-1/4	4-5/16	4	5-1/8	9-9/16	3
2	184.08	369.20	11000	4-1/2	1-5/8	2-1/4	1-1/2	4-5/16	4-1/2	6	10-5/16	3-7/8
3	823.05	1650.75	31000	4-1/2	2-1/8	2-11/16	1-3/4	4-5/16	5-3/8	7-1/8	11-7/8	5
4	920.40		31000	5	2-3/8	2-15/16	3-1/2	4-5/16	5-7/8	9-3/8	13-11/16	5-3/4
5	969.96		31000	5	2-5/8	3-7/16	3-1/2	4-5/16	6-7/8	10-3/8	14-11/16	6-1/4
6	1490.34		41000	6	3-1/8	4	3-1/2	4-5/16	8	11-1/2	15-13/16	6-3/4
7	3274.50		73000	7-1/2	3-7/8	4-3/8	4	4-5/16	9-1/4	13-1/4	17-9/16	8-15/16

*Standard spacer length; however, length may vary upon application or customer request. "F" dimension will vary accordingly; contact factory.

- "RF" Coupling Rigid Flanged Coupling A rigid flanged ("RF" type coupling, non-adjustable, is used when a flanged coupling is required but not an adjustment feature. One could be used between a combination R.A.G.D. and a vertical hollow shaft motor.
- "AF" Coupling Adjustable Flanged Coupling An adjustable flanged ("AFT") type coupling is used with solid shaft driver. Coupling is complete with adjusting nut used for adjusting (raising or lowering) the pump shaft.
- "AFS" Coupling Adjustable Flanged Spacer Coupling An adjustable flanged spacer ("AFS") type coupling is identical to the "AF" type coupling, but also includes a removable spacer. This spacer allows the installation and removal of a mechanical seal without removing the driver (usually solid shaft).
- **NOTE:** Extra head height is required by the use of these couplings for all fabricated and cast iron discharge heads. Cast iron discharge heads will require a motor stand.

DO NOT USE FOR CONSTRUCTION PURPOSES UNLESS CERTIFIED.



MECHANICAL SEAL

NATIONAL PUMP COMPANY CAN PROVIDE MECHANICAL SEALS FROM ANY MANUFACTURE, INCLUDING BUT NOT LIMITED TO:

- AESSEAL
- CHAMPION
- CHESTERTON
- EAGLEBURGMANN
- FLOWSERVE
- JOHN CRANE

THE FOLLOWING IS A LIST AND BASIC PRODUCT INFORMATION ON SEVERAL JOHN CRANE SEAL TYPICALLY PROVIDED BY NATIONAL PUMP COMPANY.

TYPE 4610:

SELF ALIGNING CARTRIDGE SEAL RECOMMENDED FOR USE WITH HOLLOW SHAFT MOTOF WITH STEADY BUSHING

SHAFT SIZE	SEAL SIZE	MAX. PRESSURE
1.00	1.00	
1.19	1.25	
1.25	1.25	225
1.50	1.50	
1.69	1.75	

STANDARD = CARBON VS SILICON CARBIDE OPTIONAL = SILICON CARBIDE VS. SILICON CARBIDE FLUID = WATER

MAX. TEMP = 150F

TYPE 5610 (DUAL O-RING) / 5611 (ELASTOMER BELLOWS SELF ALIGNING CARTRIDGE SEAL

SHAFT SIZE	SEAL SIZE	MAX. PRESSURE
1.00	1.00	
1.19	1.25	
1.25	1.25	225
1.50	1.50	
1.69	1.75	
1.94	2.00	200
2.19	2.25	185
2.44	2.50	160
2.69	2.75	140

STANDARD = CARBON VS SILICON CARBIDE OPTIONAL = SILICON CARBIDE VS. SILICON CARBIDE FLUID = WATER MAX. TEMP = 175F

SHAFT SIZE	SEAL SIZE	MAX. PRESSURE
1.00	1.13	
1.19	1.50	
1.25	1.50	825
1.50	1.75	020
1.69	2.00	
1.94	2.25	
2.19	2.50	780
2.44	2.75	750
2.69	3.00	675

STANDARD = CARBON VS SILICON CARBIDE FLUID = WATER MAX. TEMP = 175F

TYPE 48

TVDE 0D1

HIGH PRESSURE SEAL THAT EXCEEDS THE RATING OF A 8B1

NON-API 682 HYDROCARBON MECHANICAL SEAL, SINGLE OR DUAL UNPRESSURIZED

TYPE 1648 & 2648

API 682 HYDROCARBON MECHANICAL SEAL, SINGLE OR DUAL UNPRESSURIZED

DISCHARGE HEAD TYPE AND SEAL USAGE

		N260	HI-	LDF	NF	NTF	NUF
			PRO				
4610		Y	Y	Y	Y	Y	Y
5610/56	11	Y	Y	Y	Y	Y	Y
8B1		Ν	N	Ν	Y	Y	Y
48		Ν	N	N	Y	Y	Y
1648/26	48	Ν	N	N	Y	Y	Y

NOTES:

[1] A STEADY BUSHING IS REQUIRED FOR ALL HOLLOW SHAFT MOTORS.

[2] A MOTOR STAND IS REQUIRED FOR N260, HI-PRO AND LDF DISCHARGE HEADS WHEN A SOLID SHAFT MOTOR AND AFS COUPLING IS REQUIRED.

UNLESS OTHERWISE SPECIFIED ALL MECHANICAL SEALS ARE PROVIDED WITH A PLAN 13 FLUSH.

API SECONDARY SEALING SYSTEMS AND FLUSH PLANS: PLAN 52 – SEAL RESERVOIR, UTILIZES A BUFFER FLUID TO REDUCE NET LEAKAGE RATES AND PROVIDE REDUNDANCY IN THE EVENT OF A FAILURE. PLAN 65 – LEAK DETECTOR, TYPICALLY USED ON SINGLE SEALS TO PROVIDE AN ALARM OR EQUIPMENT SHUT-DOWN WHEN EXCESSIVE LEAKAGE IS DETECTED. PLAN 76 – GAS CONTROL PANEL, UTILIZES A DRY RUNNING SECONDARY SEAL WHICH DIVERTS NON-CONDENSING PRIMARY SEAL LEAKAGE TO A FLARE OR VAPOR RECOVERY SYSTEM.

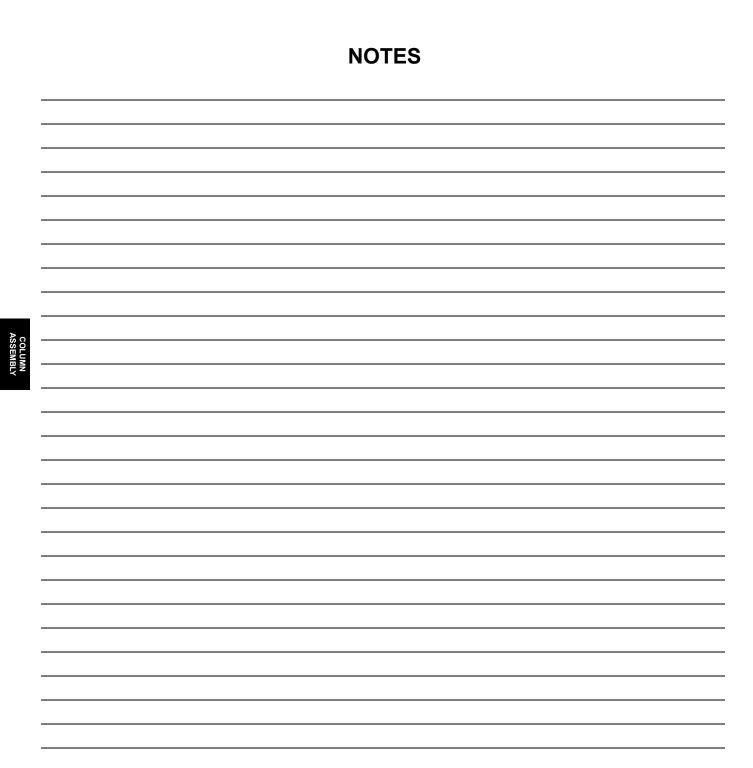


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DISCHARGE HEADS

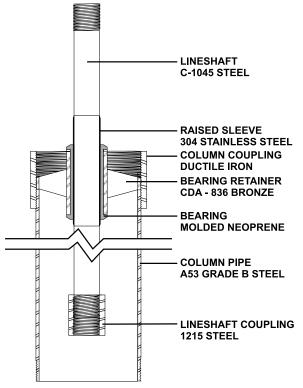




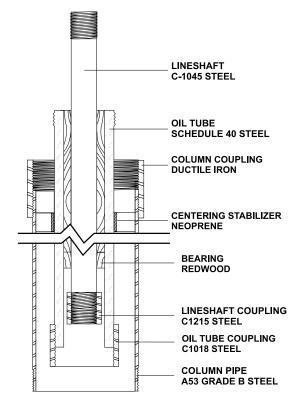
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THREADED COLUMN ASSEMBLY

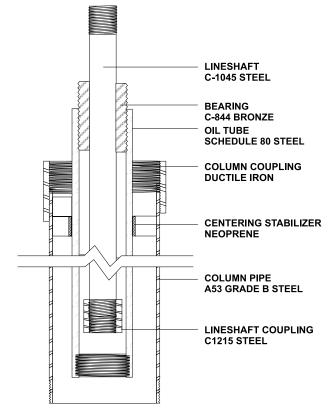
THREADED COLUMN ASSEMBLY PRODUCT LUBRICATED (PRL)



THREADED COLUMN ASSEMBLY REDWOOD OIL LUBRICATED (RWL)



THREADED COLUMN ASSEMBLY BRONZE BEARING OIL LUBRICATED (BZL)



PRODUCT LUBRICATED SHAFT THREADED COLUMN ASSEMBLY

- Complete column consists of steel column pipe, sleeve type couplings, C-1045 steel lineshaft with 304 S.S. sleeve at bearing journals, steel lineshaft couplings, bronze bearing retainer with neoprene bearing.
- Complete column consists of steel column pipe, sleeve type couplings 416 S.S. lineshaft, with 304 S.S. lineshaft couplings, bronze bearing retainer with neoprene bearings.

PRODUCT LUBRICATED SHAFT THREADED COLUMN ASSEMBLY - 5 FOOT BEARING SPACING

- Complete column consists of two 5-foot sections steel column pipe, sleeve type couplings, 10-foot C-1045 steel lineshaft with 304 S.S. sleeve at bearing journals, steel lineshaft couplings, two bronze bearing retainers with neoprene bearings.
- Complete column consists of two 5-foot sections steel column pipe, sleeve type couplings, 10-foot 416 S.S. lineshaft, with 304 S.S. lineshaft couplings, two bronze bearing retainers with neoprene bearings.

OIL LUBRICATED SHAFT THREADED COLUMN PIPE - BRONZE BEARING

- Complete column assembly consists of steel column pipe, sleeve type couplings, steel oil tube ASTM A-53 Grade A Sch. 80, with bronze bearings, carbon steel lineshaft and couplings, neoprene centering stabilizers at 20foot intervals. SPACING BASED ON 5-FOOT BEARING CENTERS.
- ▶ FOR SPEEDS HIGHER THAN 1800 RPM, CONTACT FACTORY.

OIL LUBRICATED THREADED COLUMN PIPE - REDWOOD OIL LUBRICATED

 Complete column assembly consists of steel column pipe, sleeve type column couplings, steel ASTM A-53 Grade A Sch. 40 oil tube, with oil impregnated redwood lined bearing, carbon steel lineshaft and coupling, neoprene centering stabilizers at 20-foot intervals.

ALTERNATE MATERIALS AVAILABLE UPON REQUEST.

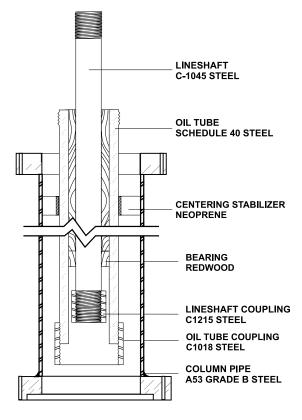


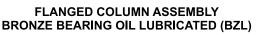
FLANGED COLUMN ASSEMBLY

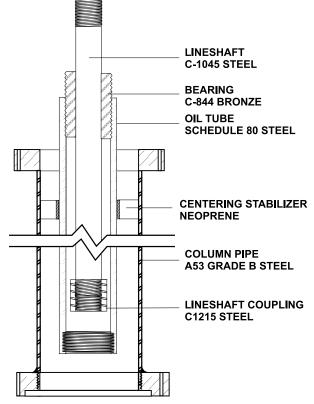
FLANGED COLUMN ASSEMBLY PRODUCT LUBRICATED (PRL)

LINESHAFT C-1045 STEEL RAISED SLEEVE 304 STAINLESS STEEL BEARING RETAINER CDA - 836 BRONZE BEARING MOLDED NEOPRENE COLUMN PIPE A53 GRADE B STEEL LINESHAFT COUPLING 1215 STEEL

FLANGED COLUMN ASSEMBLY REDWOOD OIL LUBRICATED (RWL)







PRODUCT LUBRICATED SHAFT FLANGED COLUMN ASSEMBLY

- 1. Complete column consists of flanged steel column pipe, C-1045 steel lineshaft with 304 S.S. sleeve at bearing journals, steel lineshaft couplings, bronze bearing retainer with neoprene bearing.
- Complete column consists of flanged steel column pipe, sleeve type couplings 416 S.S. lineshaft, with 304 S.S. lineshaft couplings, bronze bearing retainer with neoprene bearings.

PRODUCT LUBRICATED SHAFT FLANGED COLUMN ASSEMBLY - 5 FOOT BEARING SPACING

- Complete column consists of two 5-foot sections flanged steel column pipe, 10-foot C-1045 steel lineshaft with 304 S.S. sleeve at bearing journals, steel lineshaft couplings, two bronze bearing retainers with neoprene bearings.
- Complete column consists of two 5-foot sections flanged steel column pipe, sleeve type couplings, 10-foot 416 S.S. lineshaft, with 304 S.S. lineshaft couplings, two bronze bearing retainers with neoprene bearings.

OIL LUBRICATED SHAFT FLANGED COLUMN PIPE - BRONZE BEARING

 Complete column assembly consists of flanged steel column pipe, steel oil tube ASTM A-53 Grade A Sch. 80, with bronze bearings, carbon steel lineshaft and couplings, neoprene centering stabilizers at 20-foot intervals. SPACING BASED ON 5-FOOT BEARING CENTERS. FOR SPEEDS HIGHER THAN 1800 RPM, CONTACT FACTORY.

OIL LUBRICATED FLANGED COLUMN PIPE - REDWOOD OIL LUBRICATED

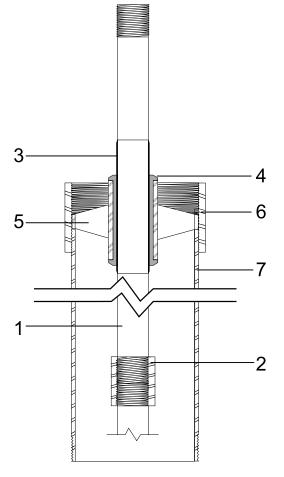
1. Complete column assembly consists of flanged steel column pipe, steel ASTM A-53 Grade A Sch. 40 oil tube, with oil impregnated redwood lined bearing, carbon steel lineshaft and coupling, neoprene centering stabilizers at 20-foot intervals.



COLUMN ASSEMBLY PRODUCT LUBRICATED TYPE FOR LINESHAFT TURBINE PUMPS

COLUMN SIZE SCH.		WEIGHT	IN LBS.	MAX. AWWA	O.D.	
WALL THICKNESS	SHAFT SIZE	5 FT.	10 FT.	RECMD. GPM	PIPE CPLG <u>.</u>	
4"	1"	71	139	150		
SCH. 40	1-3/16"	77	150	100	5.20"	
0.237"	1-1/4"	79	154	100	0.20	
	1"	95	182	325		
5"	1-3/16"	101	193	250	6.30"	
SCH. 40	1-1/4"	103	197	250	0.00	
0.258"	1-1/2"	113	216	225		
	1"	118	227	600		
6"	1-3/16"	124	238	500		
SCH. 40	1-1/4"	126	242	500	7.39"	
0.280"	1-1/2"	136	261	400	1.00	
	1-11/16"	144	277	400		
	1"	172	329	1350		
8"	1-3/16"	178	340	1300		
	1-1/4"	180	344	1300	9.63"	
SCH. 30 0.277"	1-1/2"	190	363	1150	0.00	
	1-11/16"	198	379	1150		
	1-15/16"	212	405	950		
	1"	245	461	2800		
	1-3/16"	251	472	2600		
10"	1-1/4"	253	474	2600	11.75"	
0.279"	1-1/2"	263	495	2450	11.70	
	1-11/16"	271	511	2450		
	1-15/16"	285	538	2000		
	1"	304	565	4700		
	1-3/16"	310	577	4300		
12"	1-1/4"	312	581	4300	14.00"	
SCH. 30	1-1/2"	322	602	4000	17.00	
0.330"	1-11/16"	330	616	4000		
	1-15/16"	344	642	3600		
	2-3/16"	359	671	3400		

THREADED COLUMN ASSEMBLY PRODUCT LUBRICATED (PRL)



TYPICAL COLUMN ASSEMBLY CONSISTS OF:

- 1. C-1045 STEEL LINESHAFT
- 2. 1215 STEEL SHAFT COUPLING
- 3. 304 STAINLESS SLEEVE
- 4. NEOPRENE LINESHAFT BEARING
- 5. CDA-836 BRONZE BEARING RETAINER
- 6. DUCTILE IRON PIPE COUPLINGS
- 7. A53 GRADE B STEEL PIPE

CONSULT THE FACTORY FOR MATERIAL AVAILABILITY AND PRICES OTHER THAN STANDARD.

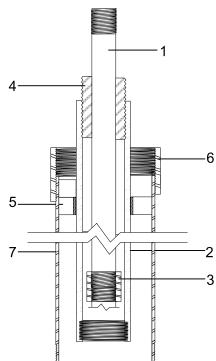


COLUMN

COLUMN ASSEMBLY OIL LUBE/BRONZE BEARING TYPE FOR LINESHAFT TURBINE PUMPS

COLUMN SIZE SCH.	0114 57	WE	IGHT IN	MAX. AWWA	O.D.	
WALL THICKNESS	SHAFT SIZE	5 FT.	10 FT.	20 FT.	RECMD.	PIPE CPLG.
4"	1" X 1-1/2"	92	182	358	150	
SCH. 40	1-3/16" X 2"	105	209	414	100	5.20"
0.237"	1-1/4" X 2"	108	212	417	100	
5"	1" X 1-1/2"	116	225	439	325	
Ũ	1-3/16" X 2"	129	252	495	250	6.30"
SCH. 40	1-1/4" X 2"	132	255	498	250	
0.258"	1-1/2" X 2-1/2"	157	305	596	225	
	1" X 1-1/2"	139	270	528	600	
6"	1-3/16" X 2"	152	297	584	500	
SCH. 40	1-1/4" X 2"	155	300	587	500	7.39"
0.280"	1-1/2" X 2-1/2"	180	350	685	400	
	1-11/16" X 2-1/2"	186	370	725	400	
	1" X 1-1/2"	175	311	649	1350	
8"	1-3/16" X 2"	188	338	705	1300	
	1-1/4" X 2"	191	341	708	1300	9.63"
SCH. 30 0.277"	1-1/2" X 2-1/2"	216	391	806	1150	0.00
0.277	1-11/16" X 2-1/2"	222	411	846	1150	
	1-15/16" X 3"	244	466	956	950	
	1" X 1-1/2"	221	413	794	2800	
	1-3/16" X 2"	234	440	850	2600	
10"	1-1/4" X 2"	237	443	853	2600	11.75"
0.279"	1-1/2" X 2-1/2"	262	493	951	2450	
0.213	1-11/16" X 2-1/2"	268	513	991	2450	
	1-15/16" X 3"	290	568	1101	2000	
	1" X 1-1/2"	298	553	1059	4700	
	1-3/16" X 2"	311	580	1115	4300	
12"	1-1/4" X 2"	314	583	1118	4300	14.00"
	1-1/2" X 2-1/2"	339	633	1216	4000	
SCH. 30	1-11/16" X 2-1/2"	345	653	1256	4000	
0.330"	1-15/16" X 3"	367	708	1366	3600	
	2-3/16" X 3-1/2"	394	768	1477	3400	

THREADED COLUMN ASSEMBLY BRONZE BEARING OIL LUBRICATED (BZL)



TYPICAL COLUMN ASSEMBLY CONSISTS OF:

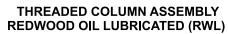
- 1. C-1045 STEEL LINESHAFT
- 2. SCH. 80 STEEL TUBING
- 3. 1215 STEEL SHAFT COUPLING
- 4. C-844 BRONZE LINESHAFT BRG.
- 5. RUBBER CENTERING STABILIZER (1 FOR EACH 40 FT.)
- 6. DUCTILE IRON PIPE COUPLINGS
- 7. A53 GRADE B STEEL PIPE

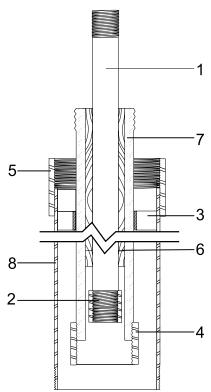
CONSULT THE FACTORY FOR MATERIAL AVAILABILITY AND PRICES OTHER THAN STANDARD.



COLUMN ASSEMBLY OIL LUBE/REDWOOD BEARING TYPE FOR LINESHAFT TURBINE PUMPS

COLUMN SIZE WALL THICKNESS/		WE		MAX. AWWA RECMD.	O.D.		
SCH.	SHAFT SIZE	5 FT.	10 FT.	20 FT.	GPM	PIPE CPLG.	
4"	1" X 1-1/2"	87	168	299	160		
SCH. 40	1-3/16" X 2"	98	190	375	100	5.20"	
0.237"	1-1/4" X 2"	100	194	382	100		
5"	1" X 1-1/2"	111	211	380	325		
	1-3/16" X 2"	122	233	455	250	6.30"	
SCH 40 0.258"	1-1/4" X 2"	124	237	463	250	0.00	
0.200	1-1/2" X 2-1/2"	146	278	542	225		
6"	1" X 1-1/2"	134	256	469	600		
	1-3/16" X 2"	145	278	544	500	7 00"	
SCH 40	1-1/4" X 2"	147	282	552	500	7.39"	
0.200	1-1/2" X 2-1/2"	169	323	631	400		
8"	1" X 1-1/2"	170	297	590	1350		
o i	1-3/16" X 2"	181	319	665	1300	0.00"	
SCH. 30	1-1/4" X 2"	183	323	673	1300	9.63"	
0.277"	1-1/2" X 2-1/2"	205	364	752	1150		
	1" X 1-1/2"	216	399	735	2800		
10"	1-3/16" X 2"	227	421	810	2600		
0.279"	1-1/4" X 2"	229	425	818	2600	11.75"	
	1-1/2" X 2-1/2"	251	466	897	2450		
	1" X 1-1/2"	293	539	1000	4700		
12"	1-3/16" X 2"	304	561	1075	4300		
	1-1/4" X 2"	306	565	1083	4300	14.00"	
SCH 30 0.330"	1-1/2" X 2-1/2"	328	606	1162	4000		
	1-11/16 X 2-1/2	334	619	1188	3900		





TYPICAL COLUMN ASSEMBLY CONSISTS OF:

- 1. C-1045 STEEL LINESHAFT
- 2. 1215 STEEL SHAFT COUPLING
- 3. RUBBER CENTERING STABILIZER (1 FOR EACH 40 FT.)
- 4. C-1018 STEEL TUBE COUPLING
- 5. DUCTILE IRON PIPE COUPLING
- 6. REDWOOD SHAFT BEARING
- 7. SCHEDULE 40 STEEL TUBING
- 8. A53 GRADE B STEEL PIPE

CONSULT THE FACTORY FOR MATERIAL AVAILABILITY AND PRICES OTHER THAN STANDARD.



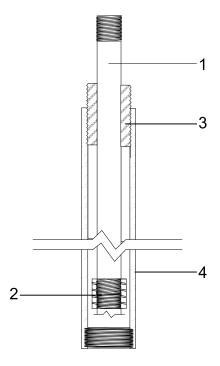
INNER COLUMN ASSEMBLY FOR LINESHAFT TURBINE PUMPS

BRONZE BEARING

	WE			
SIZE	5 FT.	10 FT.	20 FT.	O.D.TUBE
1" X 1-1/2"	34	70	138	1.900
1-3/16" X 2"	47	97	194	2.375
1-1/4" X 2"	50	100	197	2.375
1-1/2" X 2-1/2"	75	150	295	2.875
1-11/16" X 2-1/2"	81	170	335	2.875
1-15/16" X 3	103	225	445	3.500
2-3/16" X 3-1/2"	130	285	556	4.000

TYPICAL INNER COLUMN ASSEMBLY CONSISTS OF:

- 1. C-1045 STEEL LINESHAFT
- 2. 1215 STEEL SHAFT COUPLING
- 3. C-844 BRONZE LINESHAFT BEARING
- 4. SCH. 80 STEEL OIL TUBE

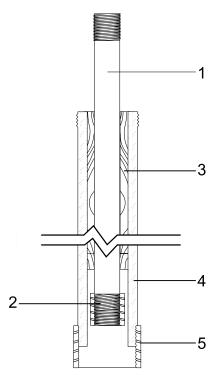


REDWOOD BEARING

	WE			
SIZE	5 FT.	10 FT.	20 FT.	O.D.TUBE
1" X 1-1/2"	29	56	79	2.25
1-3/16" X 2"	40	78	154	2.75
1-1/4" X 2"	40	78	154	2.75
1-1/2" X 2-1/2"	64	123	241	3.25
1-11/16" x 2-1/2"	70	136	267	3.25

TYPICAL INNER COLUMN ASSEMBLY CONSISTS OF:

- 1. C-1045 STEEL LINESHAFT
- 2. 1215 STEEL SHAFT COUPLING
- 3. REDWOOD SHAFT BEARING
- 4. SCH. 40 STEEL OIL TUBE
- 5. C-1018 STEEL TUBE COUPLING

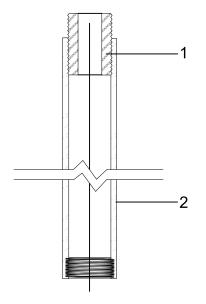




TUBE LINE WITHOUT SHAFT FOR LINESHAFT TURBINE PUMPS

BRONZE BEARING

	WE			
SIZE	5 FT.	10 FT.	20 FT.	O.D.TUBE
1" X 1-1/2"	18	36	72	1.900
1-3/16" X 2"	25	50	100	2.375
1-1/4" X 2"	25	50	100	2.375
1-1/2" X 2-1/2"	38	76	152	2.875
1-11/16" X 2-1/2"	38	76	152	2.875
1-15/16" X 3	51	102	204	3.500
2-3/16" X 3-1/2"	66	157	300	4.000



TYPICAL INNER COLUMN ASSEMBLY CONSISTS OF:

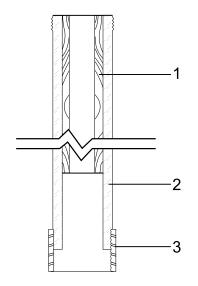
- 1. C-844 BRONZE LINESHAFT BEARING
- 2. SCH. 80 STEEL OIL TUBE

	WE			
SIZE	5 FT.	10 FT.	20 FT.	O.D.TUBE
1" X 1-1/2"	15	29	57	2.25
1-3/16" X 2"	21	40	78	2.75
1-1/4" X 2"	21	40	78	2.75
1-1/2" X 2-1/2"	33	62	120	3.25
1-11/16" X 2-1/2"	32	60	115	3.25

REDWOOD BEARING

TYPICAL INNER COLUMN ASSEMBLY CONSISTS OF:

- 1. REDWOOD SHAFT BEARING
- 2. SCH. 40 STEEL OIL TUBE
- 3. C-1018 STEEL TUBE COUPLING





SHAFT OIL LUBE & PRODUCT LUBE TYPE FOR LINESHAFT TURBINE PUMPS

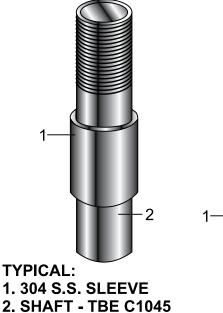
SHAFT/C-1045 TBE OIL LUBE TYPE

	WEIGHT				
SIZE	5 FT.	10 FT.	20 FT.		
1"	14	27	54		
1-3/16"	19	38	76		
1-1/4"	21	42	84		
1-1/2"	30	60	120		
1-11/16"	38	76	152		
1-15/16"	50	100	200		
2-3/16"	64	128	256		
2-7/16"	80	159	318		
2-11/16"	97	194	387		

TYPICAL: SHAFT - TBE C1045 CARBON STEEL

SHAFT/C-1045 TBE PRODUCT LUBE TYPE & SHAFT/416 S.S. TBE PRODUCT LUBE TYPE

	WEIGHT				
SIZE	5 FT.	10 FT.	SLEEVE O.D IN.		
1"	15	28	1.25		
1-3/16"	19.5	38.5	1.50		
1-1/4"	21.5	42.5	1.375		
1-1/2"	31	61	1.6875		
1-11/16"	39	77	1.9375		
1-15/16"	51	101	2.1875		
2-3/16"	65	129	2.4375		
2-7/16"	82	161	2.6875		
2-11/16"	99	196	2.9375		



CARBON STEEL

TYPICAL: 1. 304 S.S. SLEEVE 2. SHAFT - TBE 416 STAINLESS STEEL

SHAFT COUPLINGS

SIZE	CARBON	416 S.S.	304 S.S.	O.D.
1"	0.50	0.50	0.50	1.38
1-3/16"	0.75	0.75	0.75	1.62
1-1/4"	1.00	1.00	1.00	1.62
1-1/2"	1.75	1.75	1.75	2.06
1-11/16"	2.00	2.00	2.00	2.13
1-15/16"	4.25	4.25	4.25	2.63
2-3/16"	6.10	6.10	6.10	2.75

BRONZE LINESHAFT BEARINGS

TUBE AND SHAFT SIZE	WEIGHT.
1" X 1-1/2"	1.00
1-3/16" X 2"	2.00
1-1/4" X 2"	2.00
1-1/2" X 2-1/2"	4.00
1-11/16" X 2-1/2"	3.75
1-15/16" X 3"	6.00
2-3/16" X 3-1/2"	8.50

TUBE COUPLING REDWOOD TYPE

TUBE SIZE	WEIGHT.	O.D.
1-1/2"	1.25	2.25
2"	1.75	2.75
2-1/2"	2.50	3.25

COLUMN PIPE COUPLING 8 TPI - R.H.

PIPE SIZE	WEIGHT.
4"	4
5"	9
6"	10
8"	17
10"	31
12"	45



TYPICAL SHAFT COUPLING 1215 STEEL



TYPICAL LINESHAFT BEARING C-844 BRONZE



TYPICAL REDWOOD COUPLING C-1018 STEEL

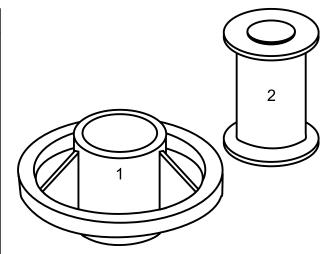


TYPICAL COLUMN PIPE COUPLING DUCTILE IRON



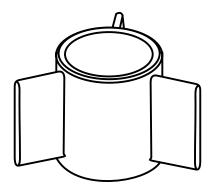
CENTERING STABILIZERS PRODUCT LUBE & OIL LUBE TYPE FOR LINESHAFT TURBINE PUMPS

			WEI	ЭНТ
PIPE SIZE	SHAFT SIZE W.L.	TUBE SIZE O.L.	PRODUCT LUBE	OIL LUBE
	1"	1-1/2"	1.6	0.4
4"	1-3/16"	2"	1.5	0.5
	1-1/4"	2"	1.4	0.5
	1"	1-1/2"	2.7	0.5
5"	1-3/16"	2"	2.6	0.5
Ŭ	1-1/4"	2"	2.6	0.5
	1-1/2"	2-1/2"	3.3	0.9
	1"	1-1/2"	3.3	0.8
	1-3/16"	2"	3.2	0.8
6"	1-1/4"	2"	3.2	0.8
Ŭ	1-1/2"	2-1/2"	3.3	0.9
	1-11/16"	2-1/2"	3.2	0.9
	1"	1-1/2"	4.6	0.9
	1-3/16"	2"	4.4	1.1
8"	1-1/4"	2"	4.4	1.1
Ŭ	1-1/2"	2-1/2"	4.8	1.3
	1-11/16"	2-1/2"	4.7	1.3
-	1-15/16"	3"	4.6	1.4
	1"	1-1/2"	7.8	1.4
	1-3/16"	2"	7.7	1.5
10"	1-1/4"	2"	7.7	1.5
	1-1/2"	2-1/2"	7.5	1.5
	1-11/16"	2-1/2"	7.5	1.5
	1-15/16"	3"	7.4	1.6
	1"	1-1/2"	10.8	2.1
	1-3/16"	2"	10.7	2.6
12"	1-1/4"	2"	10.7	2.6
	1-1/2"	2-1/2"	10.6	2.9
	1-11/16"	2-1/2"	10.5	2.9
	1-15/16"	3"	10.4	3.2
	2-3/16"	3-1/2"	10.4	3.3



TYPICAL PRODUCT LUBE CENTERING STABILIZER CONSISTS OF:

- 1. CDA 875 BRONZE BEARING RETAINER
- 2. MOLDED NEOPRENE BEARING



TYPICAL OIL LUBE CENTERING STABILIZER CONSISTS OF:

1. RUBBER CENTERING SPIDER

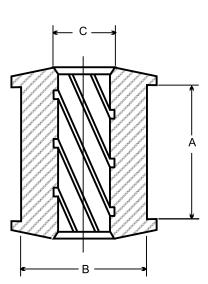


304 STAINLESS SLEEVES & NEOPRENE BEARING INSERTS

304 S.S. SLEEVE	WEIGHT OUNCES
1" X 1-1/4"	14
1-3/16" X 1-3/8"	8
1-1/4" X 1-3/8"	8
1-1/4" X 1-1/2"	9
1-1/2" X 1-11/16"	14
1-11/16" X 1-15/16"	16
1-15/16 X 2-3/16"	18
2-3/16" X 2-7/16"	20

7.00"

SHAFT SLEEVE	BEARING HUB	А	В	с	WEIGHT OUNCES
1" X 1-1/4"	1.38	2.75	1.39	1.28	5
1" X 1-1/4"	2.00	3.13	2.01	1.28	4
1" X 1-1/4"	3.00	4.50	3.01	1.28	10
1-3/16" X 1-3/8"	1.75	2.75	1.76	1.405	5
1-3/16" X 1-3/8"	2.00	3.125	2.01	1.405	4
1-3/16" X 1-3/8"	3.00	4.50	3.01	1.405	10
1-1/4" X 1-3/8"	1.75	2.75	1.76	1.405	5
1-1/4" X 1-3/8"	2.00	3.125	2.01	1.405	4
1-1/4" X 1-3/8"	3.00	4.50	3.01	1.405	10
1-1/4" X 1-1/2"	1.75	2.75	1.76	1.535	5
1-1/4" X 1-1/2"	2.00	3.125	2.01	1.535	4
1-1/4" X 1-1/2"	3.00	4.50	3.01	1.535	10
1-1/2" X 1-11/16"	2.50	3.625	2.51	1.722	6
1-1/2" X 1-11/16"	3.00	4.50	3.01	1.722	8
1-11/16" X 1-15/16"	2.50	3.625	2.51	1.972	6
1-11/16" X 1-15/16"	3.00	4.50	3.01	1.972	10
1-15/16" X 2-1/8"	2.50	3.625	2.51	2.155	6
1-15/16" X 2-1/8"	3.00	4.50	3.01	2.155	10
2-3/16" X 2-7/16"	3.00	4.50	3.01	2.4675	8

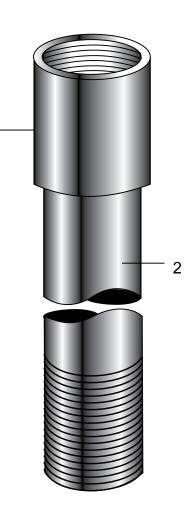




COLUMN PIPE - T & C OIL LUBE & PRODUCT LUBE TYPE FOR LINESHAFT TURBINE PUMPS

COLUMN PIPE - T & C OIL LUBE TYPE

			WEIGHT		
PIPE SIZE	WALL SIZE	5 FT.	10 FT.	20 FT.	COUPLING O.D.
4"	.237*	58	112	220	5.20
5"	.258*	82	155	301	6.30
6"	.250	95	180	350	7.39
6"	.280*	105	200	390	7.39
8"	.219	115	214	410	9.63
8"	.250	129	241	464	9.63
8"	.277*	141	261	511	9.63
8"	.322	160	303	588	9.63
10	.250	171	311	592	11.75
10"	.279*	187	343	656	11.75
10"	.307	202	373	716	11.75
10"	.365	233	436	841	11.75
12"	.250	212	379	713	14
12"	.330*	264	483	921	14



1

* STANDARD WALL PIPE

COLUMN PIPE - T & C PRODUCT LUBE TYPE

		WEIGHT		
PIPE SIZE	WALL SIZE	5 FT.	10 FT.	COUPLING O.D.
4"	.237*	57	111	5.20
5"	.258*	81	154	6.30
6"	.250	94	179	7.39
6"	.280*	104	199	7.39
8"	.219	113	212	9.63
8"	.250	127	239	9.63
8"	.277*	139	263	9.63
8"	.322	158	301	9.63
10	.250	169	309	11.75
10"	.279*	185	341	11.75
10"	.307	199	370	11.75
10"	.365	230	433	11.75
12"	.250	209	376	14
12"	.330*	261	480	14

* STANDARD WALL PIPE

TYPICAL COLUMN PIPE WITH COUPLING CONSISTS OF:

1. DUCTILE IRON COUPLING

2. A53 GRADE B STEEL



A.N.S.I. PIPE SCHEDULES

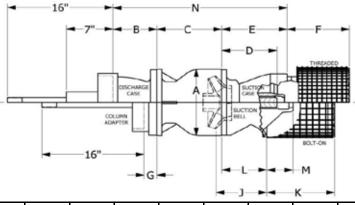
PIPE SIZE	O.D. IN INCHES	10	20	30	40	STD	60	80 (E.H.)
1-1/2	1.900	.109			.145	.145		.200
		2.085			2.718	2.718		3.631
2	2.375	.109			.154	.154		.218
		2.638			3.653	3.653		5.022
2-1/2	2.875	.120			.203	.203		.276
		3.531			5.793	5.793		7.661
3	3.5	.120			.216	.216		.300
		4.332			7.576	7.576		10.25
3-1/2	4.0	.120			.226	.226		.318
		4.973			9.109	9.103		12.51
4	4.5	.120			.237	.237	.281	.337
		5.613			10.79	10.79	12.66	14.98
4-1/2	5.0					.247		.375
						12.53		20.78
5	5.563	.134			.258	.258		.432
		7.770			14.62	14.62		28.57
6	6.625	.134			.280	.280		.500
		9.289			18.97	18.97		43.39
7	7.625					.301		.593
						23.57		64.33
8	8.625	.148	.250	.277	.322	.322	.406	.387
		13.40	22.36	24.70	28.55	28.55	35.64	88.51
9	9.625					.342		.750
						33.90		106.1
10	10.75	.165	.250	.307	.365	.365	.500	.843
		18.70	28.04	34.24	40.48	40.48	54.74	136.5
11	11.75					.375		.937
						45.55		170.8
12	12.75	.180	.250	.330	.406	.375	.562	1.031
		24.20	33.38	43.77	53.53	49.56	73.16	208.9
14	14.0	.250	.312	.375	.437	.375	.593	1.218
		36.71	45.68	54.57	63.37	54.57	84.91	296.4
16	16.0	.250	.312	.375	.500	.375	.656	
		42.05	52.36	62.58	82.77	62.58	107.5	
18	18.0	.250	.312	.437	.562	.375	.750	
L		47.39	59.03	82.06	104.8	70.59	138.2	
20	20.0	.280	.375	.500	.593	.375	.812	
L		42.73	78.60	104.1	122.9	78.60	166.4	
24	24.0	.250	.375	.562	.689	.375	.968	
		63.41	94.62	140.8	171.2	94.62	238.1	

LIGHT FIGURES = Wall Thickness

BOLD FIGURES = Weight per Foot



LINESHAFT BOWL ASSEMBLY DIMENSIONS



													B.S.	B.S.
	(0)												LGTH.	LGTH.
MODEL	A ⁽⁹⁾	В	С	D	E	F	G	J	К	L	М	Ν	P.L.	0.L.
L6	5.50	N/A	3.75	4.75	N/A	N/A	2.69	3.19	N/A	3.00	3.38	N/A	27.19	N/A
M6	5.50 ⁽⁶⁾	2.69	4.00	3.69	7.06	4.75	2.69	N/A	N/A	N/A	N/A	15.00	26.38	26.38
E6	5.63	3.94	6.19	3.69	7.06	4.75	2.69	N/A	N/A	N/A	N/A	17.19	28.57	29.82
H7	7.00(7)	5.50	6.75	6.38	8.25	6.56	1.12	8.75	N/A	N/A	N/A	20.50	30.25	34.63
K8-SC	7.63	5.53	6.50	6.50	8.38	6.31	0.94	6.00	N/A	N/A	N/A	20.41	29.94	34.53
K8-SB	7.63	5.53	6.50	6.31	N/A	N/A	0.94	N/A	6.13	5.62	2.50	N/A	29.75	34.34
M8	8.13	5.53	7.25	6.31	8.38	6.31	1.12	6.00	6.13	5.62	2.50	21.16	30.68	35.09
J8	7.75	8.56	8.88	6.00	9.25	6.63	2.06	N/A	N/A	N/A	N/A	26.69	32.94	39.44
M9-SC	9.00	5.53	8.00	6.31	8.38	6.31	1.12	6.50	5.13	6.62	2.50	21.91	31.43	35.84
M9-BL	9.00	5.53	8.00	6.94	8.38	6.31	1.12	6.50	5.13	6.62	2.50	21.91	32.06	36.47
L10	9.83	N/A	6.50	6.61	N/A	N/A	1.43	4.00	N/A	4.13	3.75	N/A	30.54	N/A
M10	10.13	5.19	9.63	9.25	10.69	7.56	1.43	7.50	8.12	7.00	3.19	25.51	36.31	40.07
K10	9.75	5.50	8.88	9.25	8.19	10.06	1.56	8.50	8.12	7.00	3.13	22.26	35.69	39.63
H10-SC	9.75	5.19	9.63	6.44	8.19	7.56	1.43	8.50	N/A	N/A	N/A	23.01	33.50	37.26
H10-BL	9.75	5.19	9.63	9.25	8.19	7.56	1.43	8.50	N/A	N/A	N/A	23.01	36.31	40.07
J10	9.63	5.19	9.75	6.31	8.19	7.56	1.56	8.50	N/A	N/A	N/A	23.13	33.62	37.25
E10	9.75	5.19	9.63	6.50	8.19	9.44	1.43	10.62	N/A	N/A	N/A	23.01	33.56	37.32
J11-SC	11.13	6.81	9.88	8.44	10.00	9.44	1.56	10.75	N/A	N/A	N/A	26.69	35.88	41.13
J11-BL	11.13	6.81	9.88	9.69	N/A	N/A	1.56	10.75	10.06	7.25	3.75	N/A	37.13	42.38
M12-SC	12.13	6.94	11.31	9.92	11.38	8.72	1.56	8.00	N/A	N/A	N/A	29.63	38.79	44.17
M12-BL	12.13	6.94	11.31	9.56	N/A	N/A	1.56	8.00	10.06	7.25	3.75	N/A	38.43	43.81
E12	11.62	4.56	10.50	9.56	10.88	9.44	1.56	8.25	10.06	7.25	3.50	25.94	37.62	40.62
K12-SC	11.50	6.06	10.50	9.92	10.88	9.44	1.31	8.25	N/A	N/A	N/A	27.44	37.73	42.48
K12-BL	11.50	6.06	10.50	9.56	N/A	N/A	1.31	8.25	10.06	7.25	3.50	N/A	37.37	42.12
H12	11.63	6.06	12.50	10.94	12.50	11.25	1.31	13.50	N/A	N/A	N/A	31.06	40.75	45.50
J12	11.75	5.81	12.38	8.12	10.00	11.25	1.63	N/A	N/A	N/A	N/A	28.44	38.13	42.31
M14	14.13	5.44	13.25	8.12	10.00	11.25	0.56 ⁽⁸⁾	7.25	12.06	6.88	2.75	28.69	37.93	42.81
H14	14.13	6.44	14.13	9.12	12.25	11.25	0.56 ⁽⁸⁾	8.75	12.06	7.38	2.81	32.82	39.81	45.69
H16	15.63	6.44	14.69	11.00	N/A	N/A	1.81	12.00	15.97	9.97	2.26	N/A	CF	CF
E18	17.50	6.44	15.00	11.25	N/A	N/A	0.81	11.25	14.13	10.25	2.50	N/A	43.06	48.69
K20	19.25	6.44	18.25	11.75	N/A	N/A	1.81	11.25	13.88	10.50	3.25	N/A	47.81	52.44
H24	23.25	10.50	21.75	15.00	N/A	N/A	0.81	11.75	15.25	11.75	5.63	N/A	53.56	63.25

NOTES

1. 7" & 16" REPRESENTS National Pump standard stick-up.

2. Threaded suction/strainer engagement per ASA B2.1 (L1+L2)

3. All dimensions are rounded off to a 2 place decimal.

4. B.S. Lgth. (Bowl Shaft Length) given is for single stage pumps only. For each additional stage, add one "C" dimensions.

5. Use discharge case dimension for oil lube pumps (O.L.). Use column adapter dimensions for product lube pumps (P.L.).

6. Dimension shown for threaded bowl, flanged bowl has a dimension of 7.00.

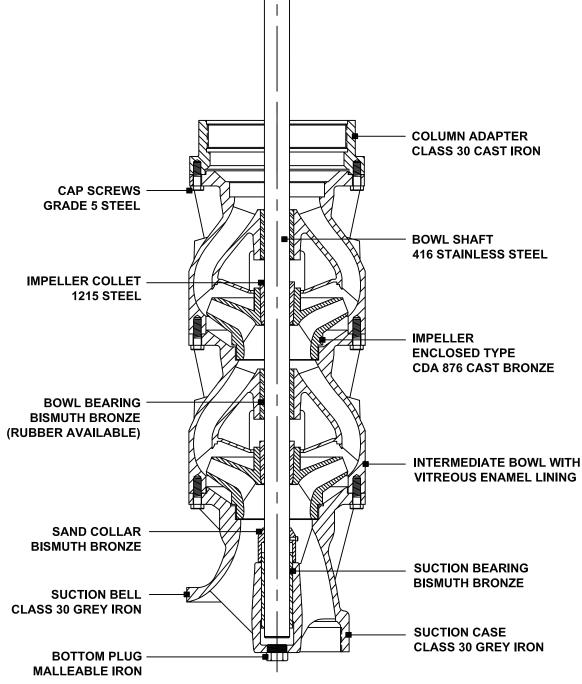
7. Dimension shown for 5" suction/discharge case, 6" suction/discharge case has a dimension of 7.25.

8. Dimension shown for 10" discharge, 12" discharge has a dimension of 1.81.

9. Refer to the suction strainer dimension page for information on the suction strainer diameter. The diameter of the strainer is typcially larger than the dimension "A" listed above.



BOWL ASSEMBLY PRODUCT LUBRICATED OPEN LINESHAFT, FLANGED CONSTRUCTION



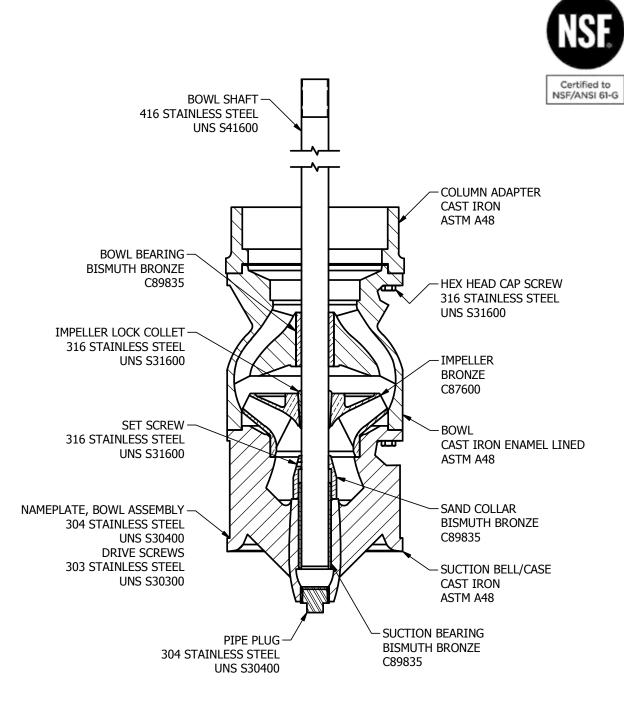
STANDARD MATERIALS OF CONSTRUCTION: Cast iron enameled bowls, bronze impellers, steel collets, 416 stainless steel bowl shaft, bronze bearings.

ALTERNATE MATERIALS AVAILABLE



BOWL ASSEMBLY NSF61 CERTIFIED - PRODUCT LUBRICATED

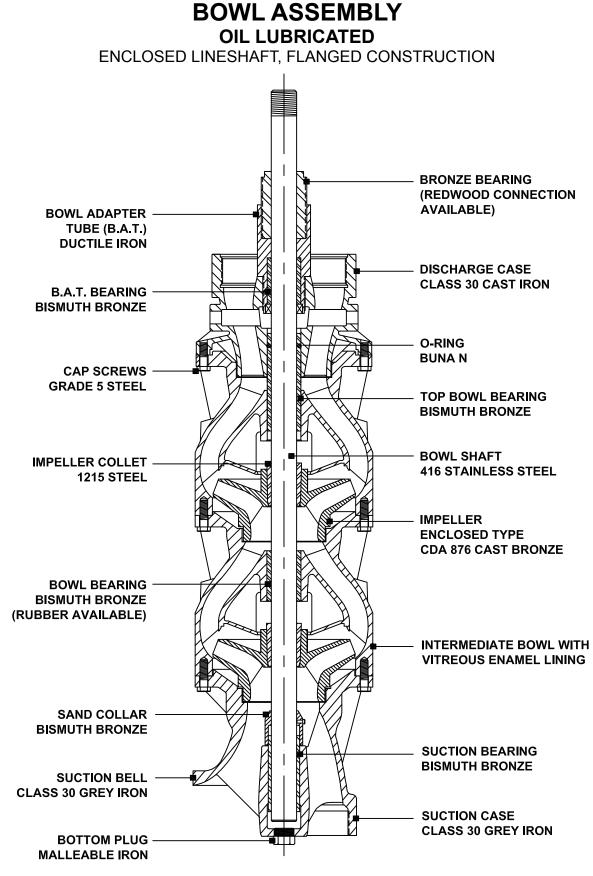
OPEN LINESHAFT, FLANGED CONSTRUCTION



NSF 61 LISTING INFORMAITON: PRODUCT TYPE: SUBMERSIBLE PUMP - PUMP ENDS TRADE DESIGNATION: SUBMERSIBLE BOWL ASSEMBLY (W)(XX)(Y)(Z) W: HYDRAULIC DESIGN (M, K, J, E, H) XX: SIZE, IN INCHES (6, 8, 9, 10, 11, 12, 14, 16, 18, 20, 24, 30) Y: DROP-IN BEARING RETAINERS & BEARINGS (4, 6, 8, 10, 12) - COLUMN SIZE Z: COATING OPTIONS (C, U)

ALTERNATE MATERIALS NOT AVAILABLE





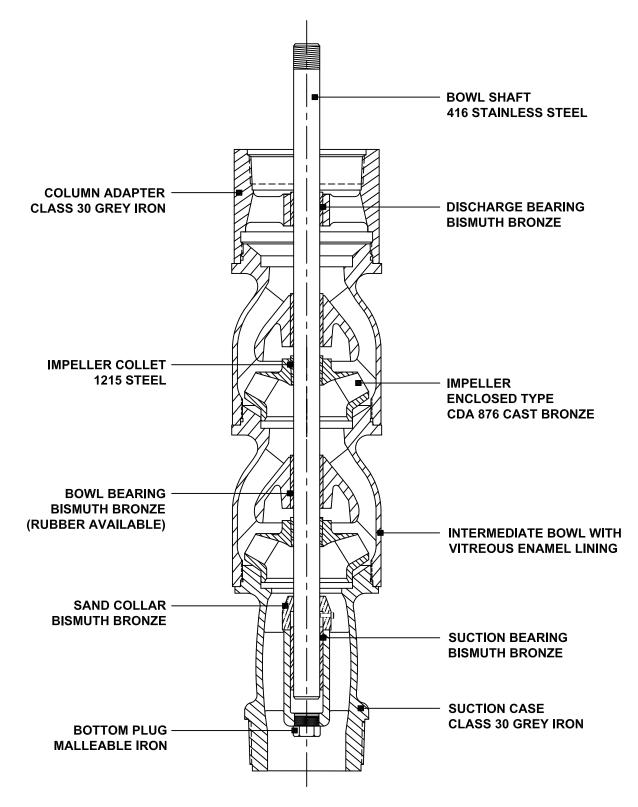
STANDARD MATERIALS OF CONSTRUCTION: Cast iron enameled bowls, bronze impellers, steel collets, 416 stainless steel bowl shaft, bronze bearings.

ALTERNATE MATERIALS NOT AVAILABLE



BOWL ASSEMBLY PRODUCT LUBRICATED

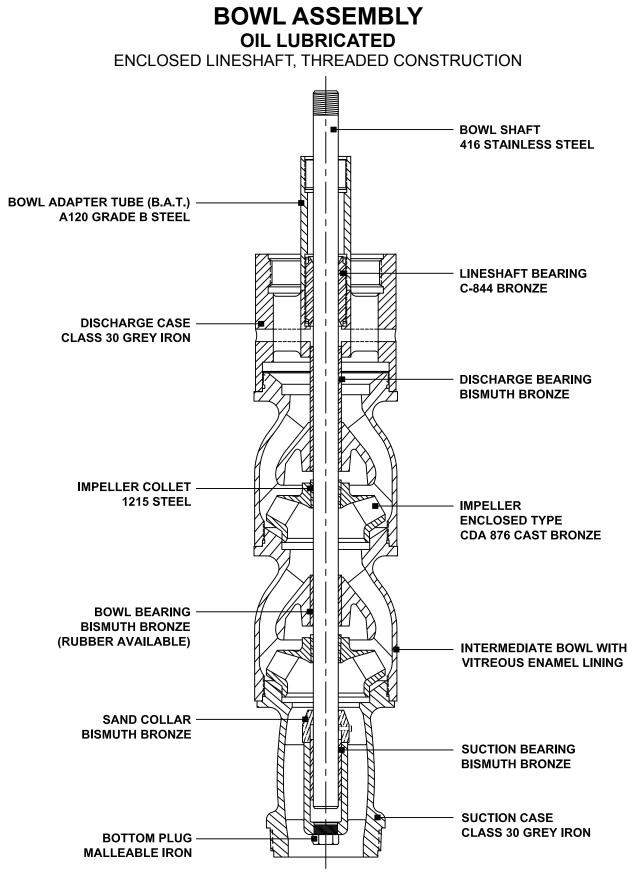
OPEN LINESHAFT, THREADED CONSTRUCTION



STANDARD MATERIALS OF CONSTRUCTION: Cast iron enameled bowls, bronze impellers, steel collets, 416 stainless steel bowl shaft, bronze bearings.

ALTERNATE MATERIALS AVAILABLE





STANDARD MATERIALS OF CONSTRUCTION: Cast iron enameled bowls, bronze impellers, steel collets, 416 stainless steel bowl shaft, bronze bearings.

ALTERNATE MATERIALS AVAILABLE



SPECIAL BOWL ASSEMBLY MATERIALS

STANDARD CLASSIFICATION		MATERIALS						
	BOWL	IMPELLER	BOWL SHAFT	COLLET	BEARING	B.S. CPLG	BOLTING (1)	
STD. BRONZE FITTED	CL. 30 C.I.E.	CDA876 BRONZE	416 S.S.	STEEL	BISMUTH BRONZE	STEEL	STEEL	
ALL IRON	CL. 30 C.I.E.	CL. 30 C.I.	416 S.S.	STEEL	C.I.	STEEL	STEEL	
IRON-316 S.S. TRIM	CL. 30 C.I.E.	CL. 30 C.I.	316 S.S.	316 S.S.	C.I.	316 S.S.	316 S.S.	
CLASS 45 C.I BRONZE FITTED	CL. 45 C.I.	CDA876 BRONZE	416 S.S.	STEEL	BISMUTH BRONZE	STEEL	STEEL	
DUCTILE IRON- BRONZE FITTED	DUCTILE IRON	CDA876 BRONZE	416 S.S.	STEEL	BISMUTH BRONZE	STEEL	STEEL	
STEEL-BRONZE FITTED	STEEL	CDA876 BRONZE	416 S.S.	STEEL	BISMUTH BRONZE	STEEL	STEEL	
CDA876 BRONZE	CDA876 BRONZE	CDA876 BRONZE	416 S.S.	416 S.S.	BISMUTH BRONZE	416 S.S.	303 S.S.	
SAE 63 ZINCLESS BRONZE	SAE 63 BRONZE	SAE 63 BRONZE	316 S.S.	316 S.S.	BISMUTH BRONZE	316 S.S.	316 S.S.	
TYPE II NI- RESIST	NI- RESIST	NI-RESIST	316 S.S.	316 S.S.	BISMUTH BRONZE	316 S.S.	316 S.S.	
316 S.S.	316 S.S.	316 S.S.	316 S.S.	316 S.S.	CARBON GRAPHITE	316 S.S.	316 S.S.	
#20 S.S.	#20 S.S.	#20 S.S.	#20 S.S.	#20 S.S.	CARBON GRAPHITE	#20 S.S.	#20 S.S.	

- 1. M6, E6 and J8 bowls are threaded construction only for standard construction. NOTE: E6 and J8 bowl assemblies are available in standard threaded construction. M6 bowl assembly is available in threaded and flanged construction (Flange Diameter is 7.25").
- 2. When pressure exceeds standards listed on Bowl Assy., Page 34, double bolting will be required. Also, "O" ring construction is recommended when pressure exceeds 250 P.S.I. or lower for certain materials. Contact factory.
- 3. When special materials are used, see Special Material Pressure Ratings on Page 35.
- 4. Special materials change performance. Refer to correction factor chart, Page 109.
- 5. Bowl shaft material and/or diameter may have to be changed to obtain adequate H.P. carrying capacity. Contact factory.
- 6. Contact factory for all special material requirements.



PERFORMANCE MULTIPLIERS FOR SPECIAL BOWL ASSEMBLY MATERIALS

	BOWLS ONLY			IMPELLERS ONLY (1)		
MODEL	C.I. NO ENAMEL	ANY BRONZE	STEEL NI-RESIST ST. STEEL	C.I. ENAMEL	C.I. NO ENAMEL	STEEL NI-RESIST ST. STEEL
				HEAD & GPM ONLY (2)		
L6LC	.95	.97	.95	.91	.91	.90
M6LC	.95	.97	.95	.91	.91	.90
M6MC-M6HC-E6XHC	.96	.97	.95	.93	.95	.91
H7XLC-H7HC	.96	.97	.96	.93	.94	.93
H7LC-M8XLC-K8LC-K8HC	.97	.98	.97	.93	.96	.95
M8MC-M8HC	.97	.98	.97	.93	.97	.95
H7XHC-M8XHC-J8XHC	.98	.98	.98	.94	.97	.97
M10LC-M10HC-M9MC	.98	.98	.98	.94	.97	.96
H10MC-H10HC-J10HC	.98	.99	.98	.94	.98	.97
M11LC-M11MC M11HC-J11LC-J11MC-J11HC	.98	.99	.98	.95	.98	.98
M12LC-M12MC M12HC-E12LC-E12XMC-E12MC- E12HC	.98	.99	.98	.95	.98	.97
E10HC-H12MC H12HC-J12XHC-K12HC	.99	.99	.99	.96	.98	.98
M14MC-M14HC M14XHC-M14XXHC	.99	.99	.98	.97	.99	.97
H14MC-H14XHC-E18LC-E18HC	.99	.99	.99	.97	.99	.98
K20LC-K20MC-K20HC	.99	.98	.99	1.00	1.00	.98
H24LC-H24MC-H24XHC	1.00	.99	.99	1.00	1.00	.98

1. No change in performance with any type bronze impeller.

2. No efficiency change with cast iron enameled impeller.

Example: Peak bowl performance of M12MC - 1770 RPM - full diameter impeller in standard materials is 925 GPM - 73 feet head - 82% - 1.0 specific gravity.

To correct for stainless steel bowl and impeller:

925 x .98 x .97 = 879 S.S. GPM 73' x .98 x .97 = 69.4 S.S. Head 82% x .98 x .97 = 77.9 S.S. Eff. (minus staging deduct)



LINESHAFT AND SUBMERSIBLE PERFORMANCE TEST & SERVICES

- Performance tests are performed with customer's bowl assembly (provided pump shaft has National standard shaft threads and projection). Test will cover normal operating range utilizing laboratory short column, laboratory discharge head and laboratory driver (motor - 3 phase, 60 hertz and 230/460). The test will be in accordance with Hydraulic Institute or API standards and (AWWA E103).
- 2. Pump test set-up and duration longer than one hour may be possible.
- 3. Witness test by customer permitted. Witness test by independent witness or impartial witness also permitted.
- 4. Included are five copies of the test results. Additional copies available.
- Additional tests that can be performed (refer to factory for full details): (A) Test with job motor, (1000 HP capacity);
 (B) Test bowl assembly with shaft threads and projection different than National standard; (C) Test complete pump unit; (D) Test NPSH; (E) Test mechanical run; (F) Test vibration.
- 6. Factory start-up or installation supervision available.

TEST FACILITIES LIMITATIONS MAXIMUM HORSEPOWER AVAILABLE WITH LABORATORY TEST MOTORS

RPM	3600	1800	900	RPM	3600
HORSEPOWER	100	350	450	HORSEPOWER/SUBMERS	IBLE 100

7. Pumps sold at 50 hertz speed will be tested at 60 hertz and test data converted to job speed.

MAXIMUM RATE OF FLOW (Capacity) AND HEAD

Rate of Flow U.S.G.P.M.	13,000
Head in Feet	1,664

8. Rate of flows shown are maximum for flow meters.

ELECTRICAL POWER

Voltage - Phase (\varnothing)	230 - 3	460 - 3	4160 - 3
Maximum Horsepower	75	600	1000

SUPPORT EQUIPMENT

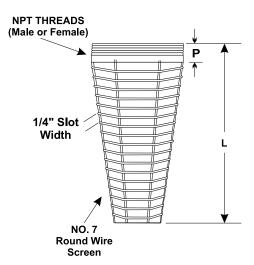
MEASUREMENT EQUIPMENT

Head	. Bourdon tube type gauges - dead weight calibration.
Rate of Flow (capacity)	. Magnetic flow meters.
Speed	. Electronic counter.
Power	. Calibrated factory test motors.

- 9. When the horsepower, rate of flow, or pressure exceed test facility limits, a test at reduced speed or reduced number stages will be performed.
- 10. Special consideration must be given to pumps sold on services with LESS than 1.0 specific gravity when tested with water at 1.0 specific gravity.



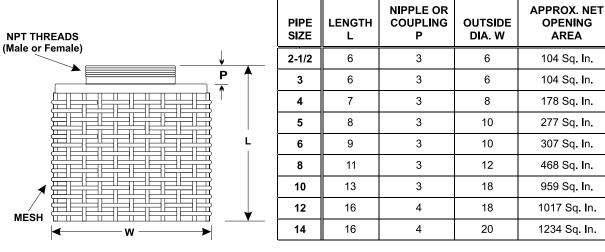
DIMENSIONS SUCTION STRAINERS



CONE TYPE STRAINER

PIPE SIZE	LENGTH L	NIPPLE OR COUPLING P	APPROX. NET OPENING AREA	WT. LBS.
2-1/2	11-1/4	1-1/2	20 Sq. In.	4
3	11-1/4	1-1/2	30 Sq. In.	4
4	11-1/2	1-3/4	50 Sq. In.	5-1/2
5	12-3/4	2	80 Sq. In.	10
6	15-3/4	2	115 Sq. In.	14
8	22-1/4	2-1/4	200 Sq. In.	26
10	30	3	315 Sq. In.	45
12	32-1/2	3	455 Sq. In.	50
14	41-1/2	3	720 Sq. In.	70

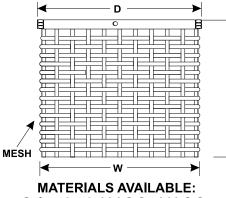
THREADED BASKET TYPE STRAINER



BOWL

L6





MESH

K8, M8 - M9 8-3/4 9-3/4 6 210 Sq. In. L 11-3/4 M10, H10 8 10-3/4 345 Sq. In. J11, M11 12-5/8 11-5/8 10 370 Sq. In. 14-1/8 M12, E12, K12 13-1/8 515 Sq. In. 10 15-3/4 H14 & M14 12 14-3/4 710 Sq. In. 21-1/2 E18 & K20 14 18-1/8 1270 Sq. In. 27 16 26 1420 Sq. In. H24

LENGTH L

Galvanized, 304 S.S., 316 S.S., **Brass and Zincless Bronze**

MESH SIZE AVAILABLE						
ches	1/4	3/8	1/2	3/4	1	

Mesh - Inches	1/4	3/8	1/2	3/4	1	1-1/2
Gauge of Wire	14	14	14	13	10	10

NOTE: "Mesh" is the term used to describe the distance from the center of one wire to the center of the next. ALL DIMENSIONS ARE IN INCHES. DO NOT USE FOR CONSTRUCTION UNLESS CERTIFIED.



WT.

LBS.

4-3/4

5

7-1/2

12 - 1/2

13

21-1/2

42

50

63

WT.

8-1/2

10

10-3/4

17

21

40

45

APPROX. NET

DIA. W CAP SCREWS OPENING AREA LBS.

PLEASE CONSULT FACTORY

TRIMMING IMPELLERS LINESHAFT TURBINE PUMP

It is sometimes necessary to trim impellers to meet design conditions. This is usually not required with the smaller units since the head developed per stage is not high, and it is usually possible to choose a number of stages that will approximately equal or exceed the design conditions. However, the larger pumps have higher heads per stage so it is sometimes necessary, or desirable to modify the impellers by trimming to reduce the head or horsepower developed by each stage.

The exact trim diameters for new units should always be provided by the factory engineering department, who will have available tests of units with similarly trimmed impellers. The following is presented as general information and will provide good results for field trimming, if necessary, providing the amount of trim does not exceed those listed on the published curve. The factory will need design head, capacity, and driver horsepower along with any limitations or special requirements to provide units with impellers properly trimmed (if required).

In general, at a given speed, the capacity pumped by a specific impeller is dependent principally on the width of the blades, or vanes, while the Head generated depends upon the outer diameter of the impeller. It is not practical to alter the width, but, within reasonable limits, the diameter may be trimmed to reduce the head generated.

The effect of changing the outer diameter is to decrease the peripheral speed of the impeller, and that has exactly the same effect as reducing the rotative speed without altering the diameter; the effect is to change the head generated in proportion to the square of the speed, or the square of the diameter, according to the fundamental formula:

 $V^2 = 2GH$

G = gravity = 32.2 feet per second H = the head generated, in feet

However, when the peripheral speed is changed, the velocity of the fluid flowing through the impeller is also changed, in direct proportion, and that changes the quantity of fluid delivered, so both changes must be considered when trimming an impeller.

There is still a third factor to be considered. Assuming there is not a major change in the speed, with the capacity in direct proportion to the diameter, and the head in proportion to the square of the diameter, the work done, which is the power required, will be the product of the two, which is in proportion to the cube of the diameter.



EXAMPLE

An impeller of 11.563 diameter is rated to deliver 1600 GPM at 100 foot head, and requires 48 BHP to drive it. (Data taken from catalog curve). What will be the effect of changing the diameter to 11.000 inches?

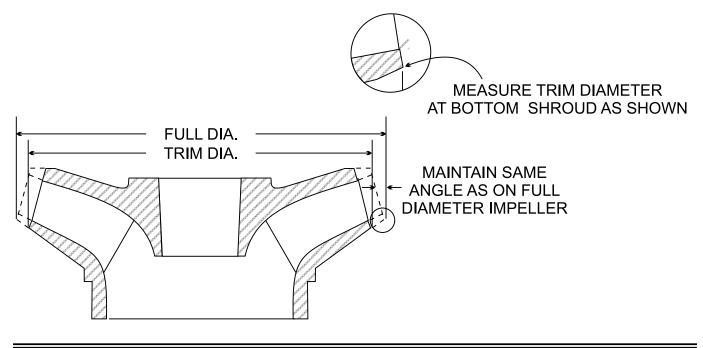
MODEL M14MC

The direct ratio of diameters will be:	<u>11.000</u> 11.563	=	.951
The trimmed capacity will be:	.951 x 1600	=	1522 GPM
The square of the ratio will be:	.951 x .951	=	.904
The trimmed head will be:	.904 x 100	=	90 feet
The cube of the ratio will be:	.951 x .951 x .951	=	.860
Trimmmed power will be:	.860 x 48	=	41 BHP

The efficiency is still another factor to be considered, but it is not seriously altered for small changes in diameter.

On multistage units it is necessary to figure one impeller only, then multiply its new head by the number of stages, for the entire pump. The capacity, and efficiency, however will be as calculated for the single impeller (corrected for number of stages as indicated on catalog curve) as all will perform the same in series.

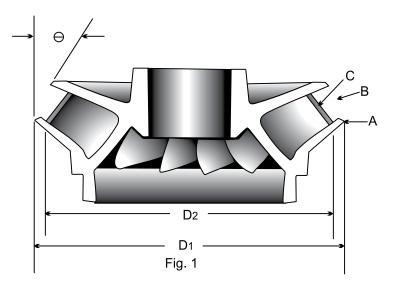
The procedure applies in the same way to semi-open and enclosed impellers.





HOW PUMP PERFORMANCE IS AFFECTED BY IMPELLER TRIMMING AND VANE TIP FILING

When the head and capacity of a pump are to be reduced, the usual procedure is to reduce the impeller diameter. This is commonly called trimming or cutting the impeller. The performance of a trimmed impeller can be approximated by the affinity laws. These laws state: (a) capacity varies as the diameter ratio; (b) developed head varies as the diameter ratio squared; (c) brake horsepower varies as the cube of the diameter ratio; and (d) efficiency remains approximately constant, though BEP (Best Efficiency Point) moves in position approximately as capacity changes.



In Fig. 1, D₁ represents a full diameter impeller and D₂ the diameter of a trim, thus the ratio of the diameters is $\frac{D_2}{D_1}$. Since capacity varies as the diameter ratio, the new capacity Q2 = Q1 $\left(\frac{D_2}{D_1}\right)$ The new head, H₂ = H₁ $\left(\frac{D_2}{D_1}\right)^2$; and HP₂ = HP₁ $\left(\frac{D_2}{D_1}\right)^3$

For smaller diameter reductions, the efficiency will remain nearly constant. For greater trims, a reduction in efficiency will result. This is caused by several factors. (1) Generally the impeller vane tapers in cross-section toward its outer tip. As the impeller is cut, blunt vane tips result which cause greater turbulence as the fluid leaves the discharge openings. This condition can be largely eliminated by proper filing of the vane tips as will be discussed later. (2) A trimmed impeller leaves a longer path for the fluid to travel between the impeller vane and the bowl vane. This also results in greater turbulence which means loss of power and consequently lower efficiency. (3) Another reduction in efficiency results from mechanical losses. The bearing and packing box losses remain the same while power output is reduced as the cube of the diameter ratio.

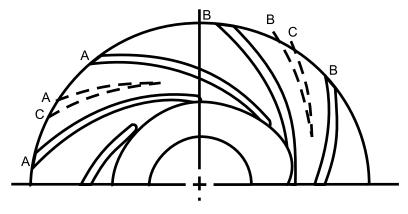


While the affinity laws closely approximate "trimmed" performance certain factors are present which account for the deviation. For impeller types as show in Fig. 1 the diameter is measured at the lower shroud, point A. The effective diameter could be said to be between the upper and lower shrouds, on point B. Using this theory, the affinity laws would be based on the diameters at points B & C. This method would not be recommended however, as obviously it would be difficult to measure, especially with impellers having an odd number of vanes.

It should be brought out that the machine angle O (Fig. 1) of the impeller discharge will affect pump performance. An increase in this angle will produce results similar to a trim even though the diameter D1 is held constant. At the factory this angle is usually held constant as the diameter is reduced.

Another factor which also accounts for inaccuracy is the reduction of vane overlap (also called solidity) with trimming. As the diameter is reduced, the sweep angle of the vane is reduced. This effectively reduces the water guidance as it travels through the impeller resulting in reduced performance.

In summary, small impellers do not trim as far proportionally as do the larger ones. However, since most small pumps are multistaged, it is seldom necessary to trim these impellers severely. Also all impeller types do not trim similarly. Only by a series of tests in a closely controlled laboratory test with successive trims can reliable information be accumulated. It is from such data as this used for a reference, that proper selections are made on each other as it reaches the factory.





Pump performance is also affected by the filing at the tip of the vane. For any pump type, high capacity impellers will usually have more vanes than low capacity impellers, and since the former had a lesser sweep angle, the relative path C (Fig. 2) will be more nearly radial. In (Fig. 2) A represents "under-filing" when B represents "top-filing". The effect of underfiling is to move the relative path toward A' or to increase the head. Under-filing in general will tend to increase the efficiency or to minimize the efficiency reduction resulting from trimming.

Top-filing of the vane acts to move the relative path toward B and to depress the head. This type of filing is not used too frequently, and should be done with extreme caution as performance is unpredictable if not based on laboratory performance tests.

Examining new impellers will more clearly show the physical features of underfiling. Again it should be emphasized that the true performance from diameter reductions and vane tip filing can only be accurately obtained in a test laboratory.



SPEED CHANGES

Pumps are quite often driven by devices which operate at speeds other than those of the published catalog curves or are capable of operating at different speeds. Variable speed electric motors, engines and turbines are examples. Catalog performance curves are usually published at standard electric motor operating speeds and therefore it is sometimes necessary to calculate the performance of pumps at speeds other than published.

The effect of trimming impellers (reducing the outside diameter of the impeller) and the effect of reducing (or increasing) the operating speed (RPM) is the same. Therefore, the following rules outline the change in performance when the operating speed is changed:

- 1. The capacity varies in direct proportion to the speed.
- 2. The head varies in direct proportion to the square of the speed.
- 3. The horsepower required varies in direct proportion to the cube of the speed.

EXAMPLE:

An impeller operating at 1760 RPM is rated to deliver 1600 GPM at 100 foot head, and requires 48 BHP to drive it (Data taken from catalog curve Model M14MC). What will be the effect of changing the speed to 1160?

The direct ratio of speeds will be:	<u>1160</u> 1760	=	.659
1160 RPM capacity will be:	.659 x 1600	=	1057 GPM
The square of the ratio will be:	.659 x .659	=	.434
1160 RPM head will be:	.434 x 100	=	43.4 feet
The cube of the ratio will be:	.659 x .659 x .659	=	.286
1160 RPM power will be:	.286 x 48	=	13.7 BHP

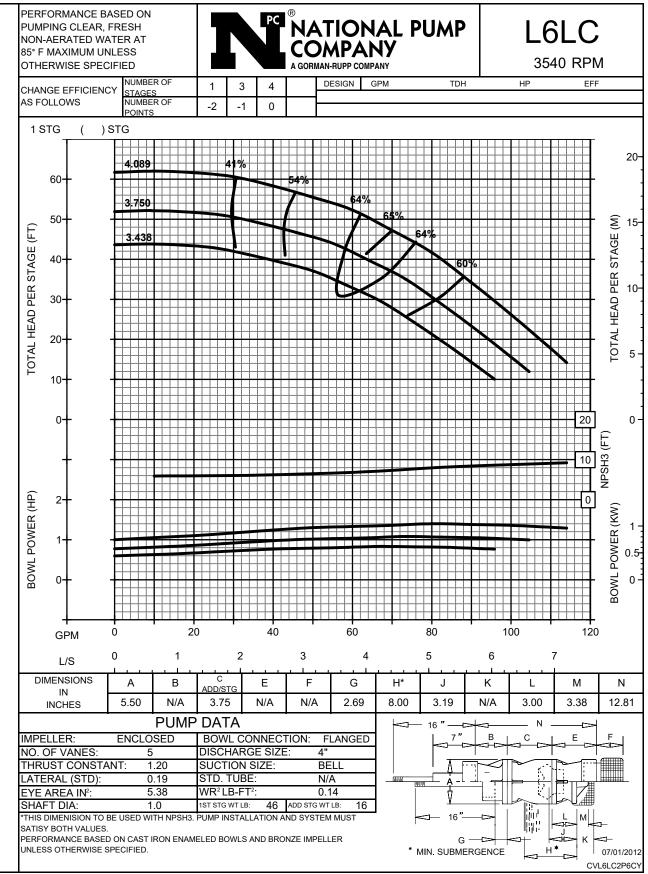
The efficiency is still another factor to be considered, but it is not seriously altered for small changes in speed. If the above pump had an efficiency of 84% at 1600 GPM when operating at 1760 RPM, the efficiency would still be approximately 84% at 1055 GPM when operating at 1160 RPM.

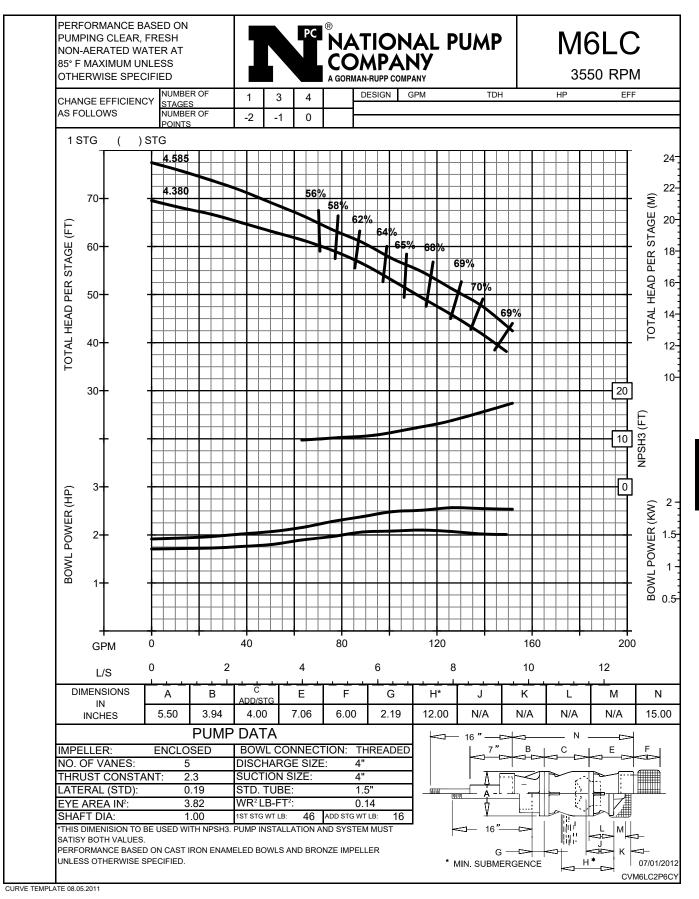


NOTES

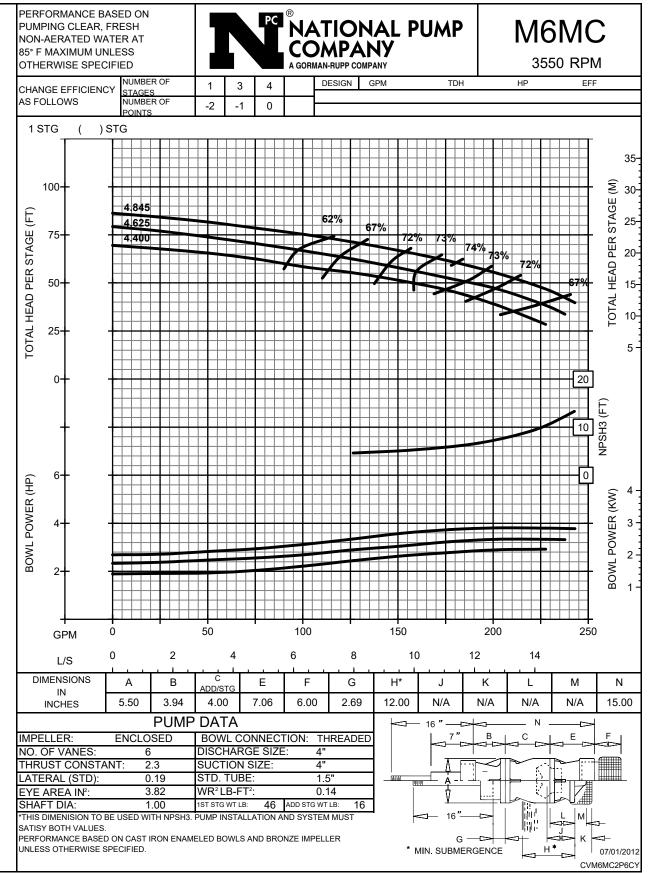
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BOWL ASSEMBLY

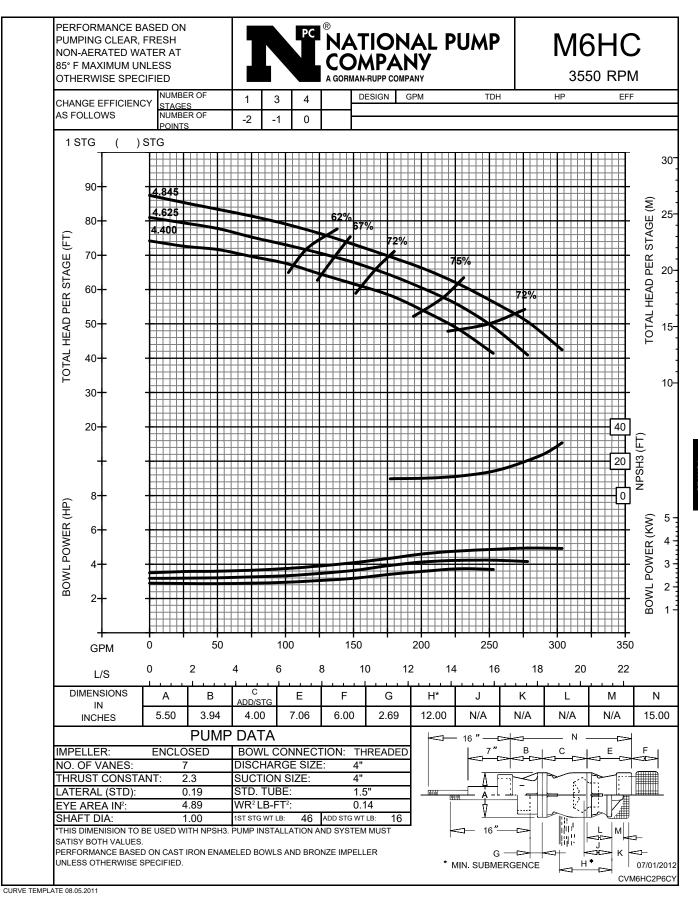




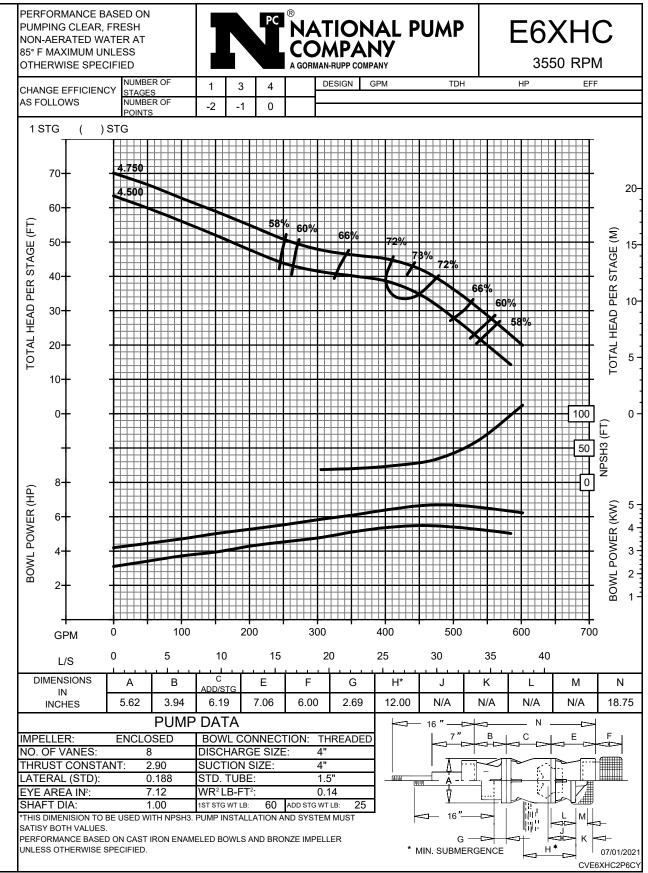
URVES



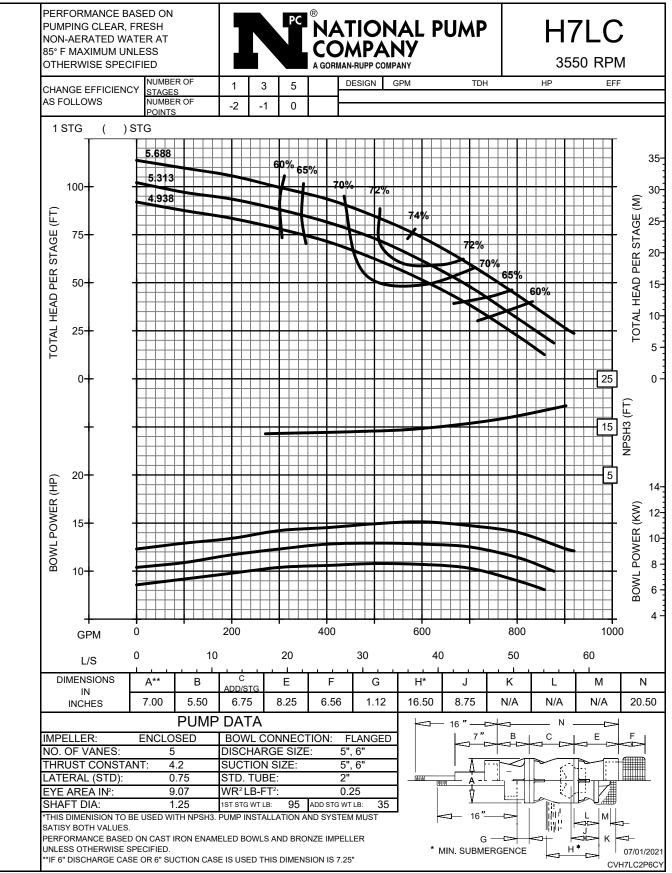




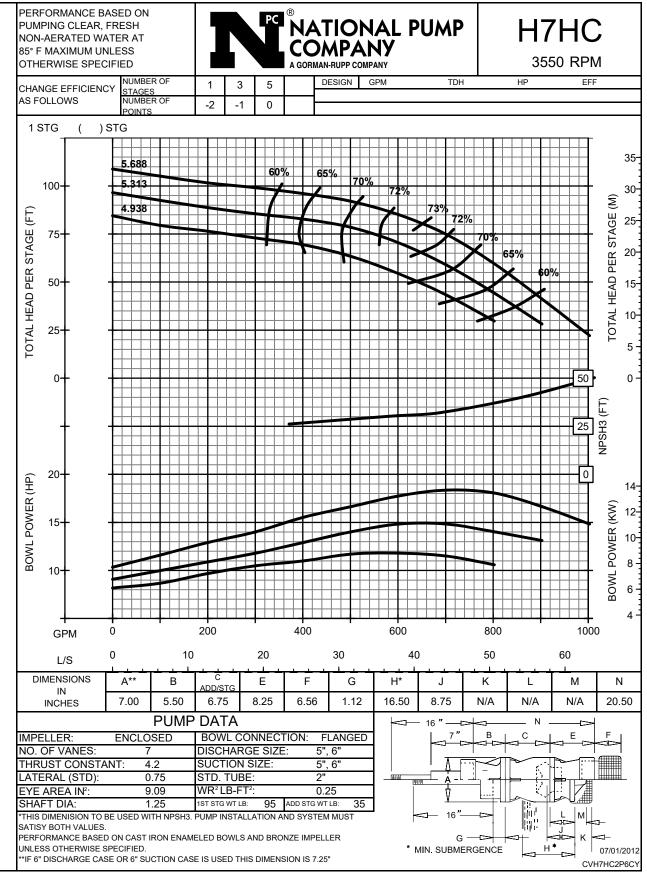
URVES



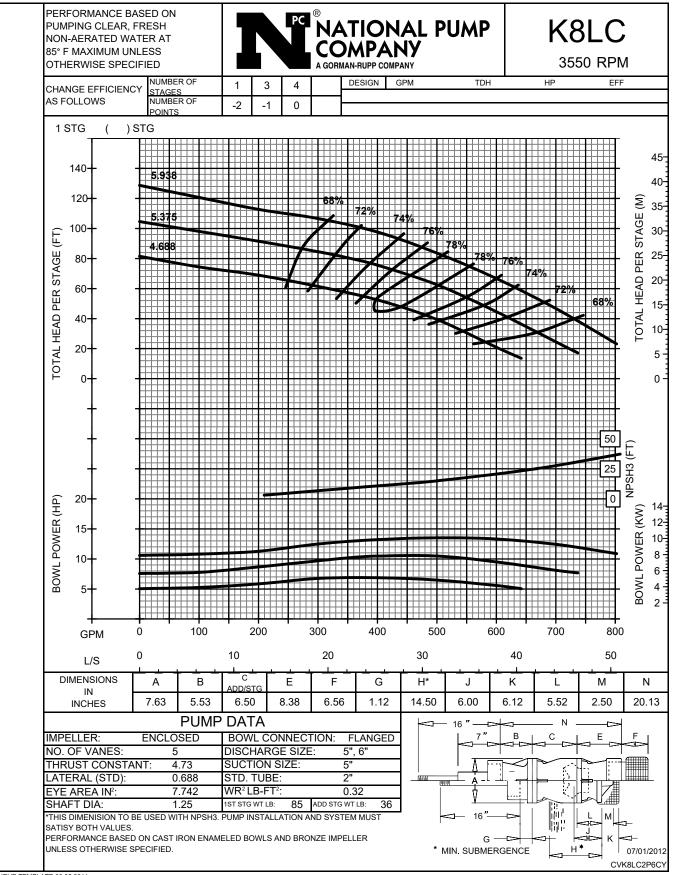




3500 URVE

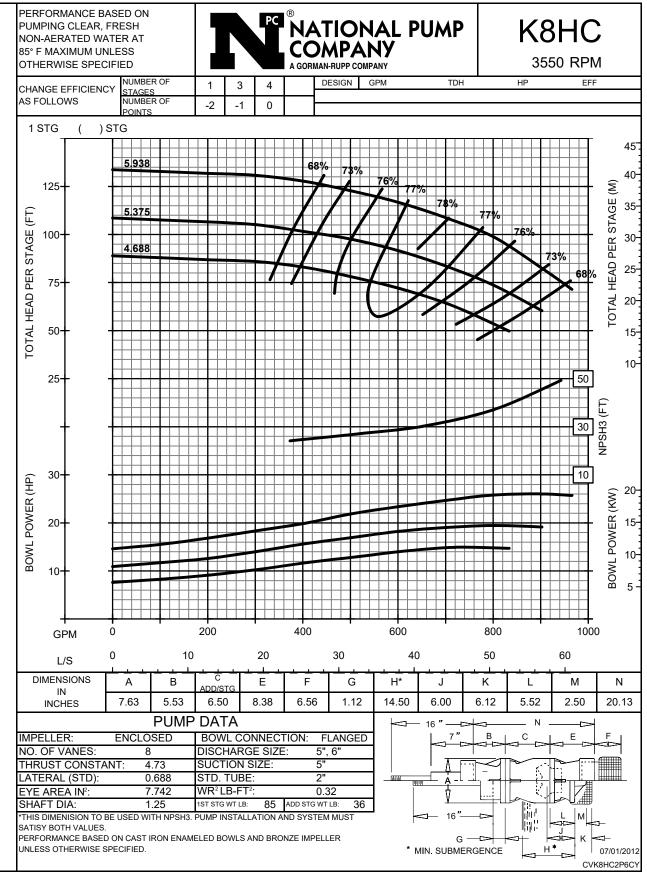






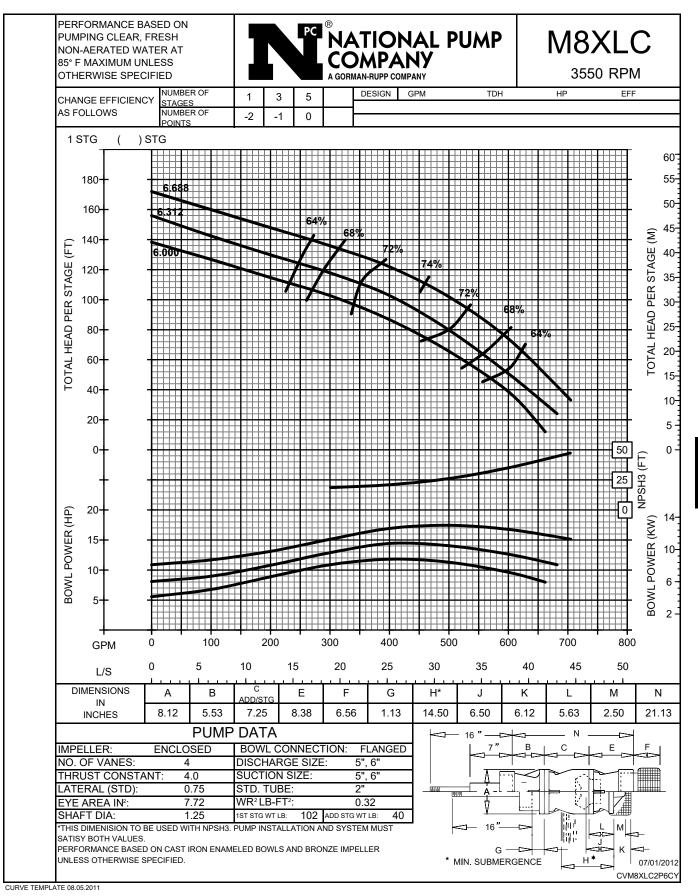
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3500 URVF

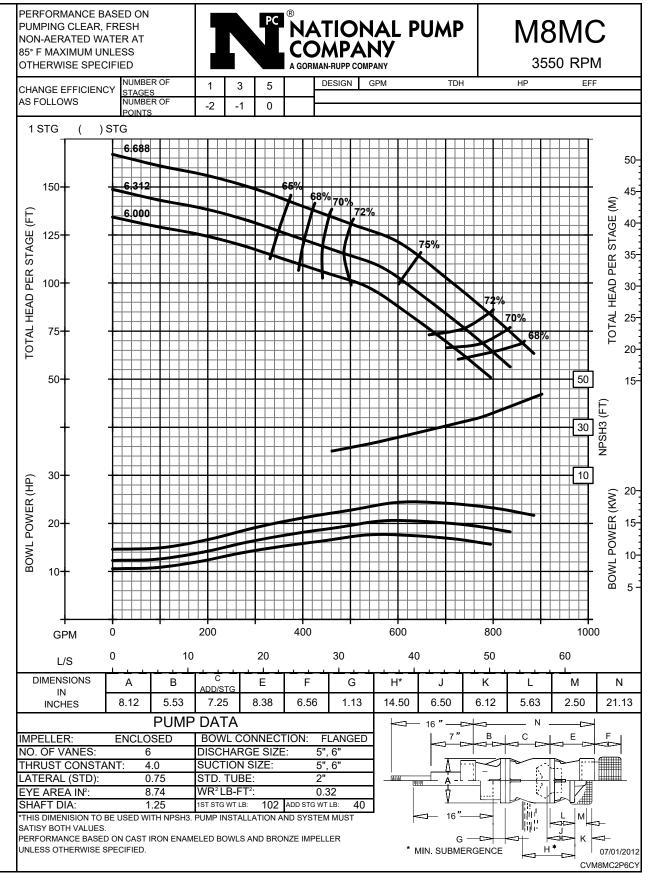




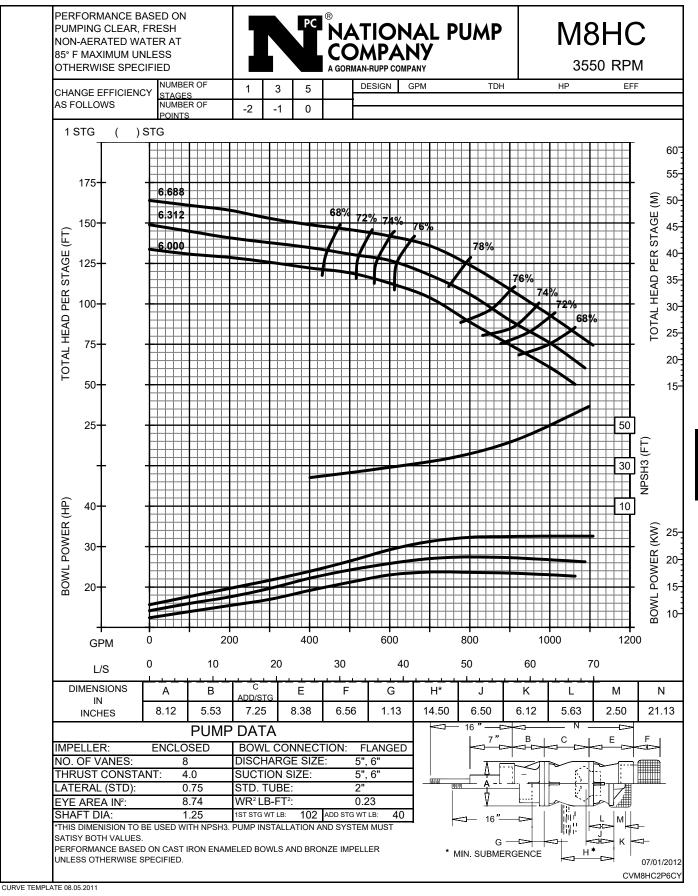




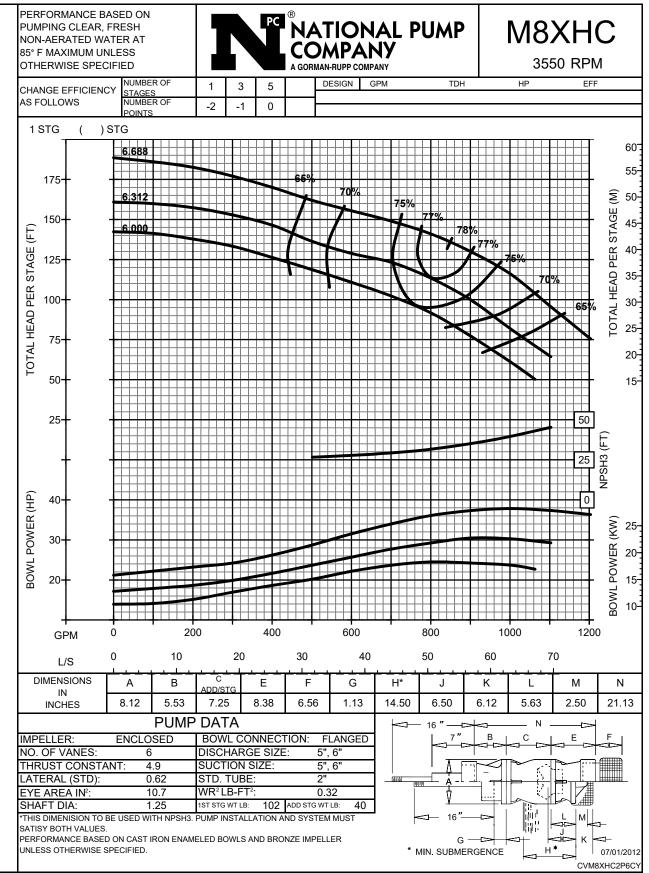
CURVE





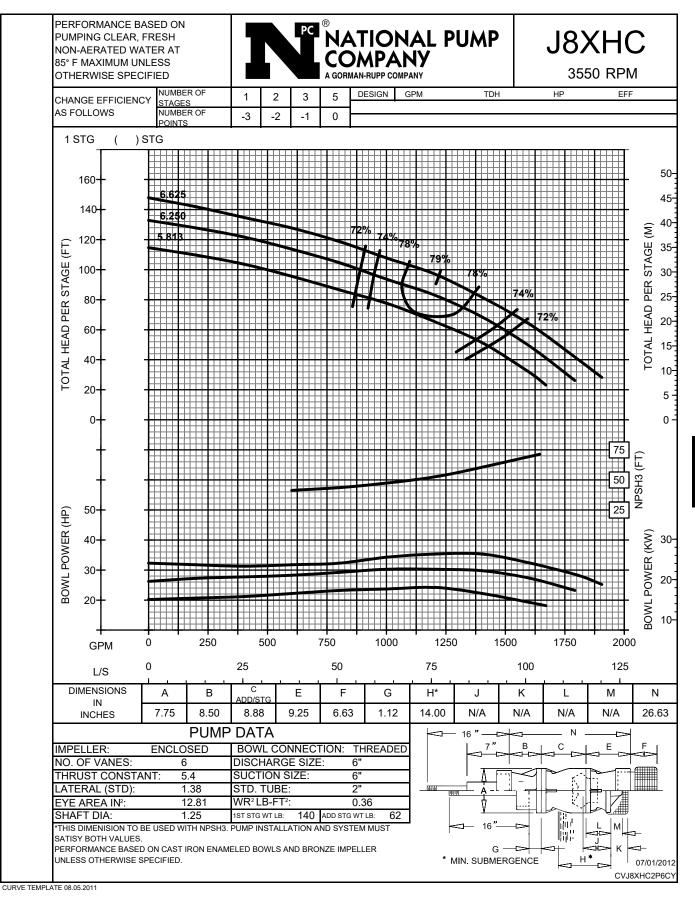


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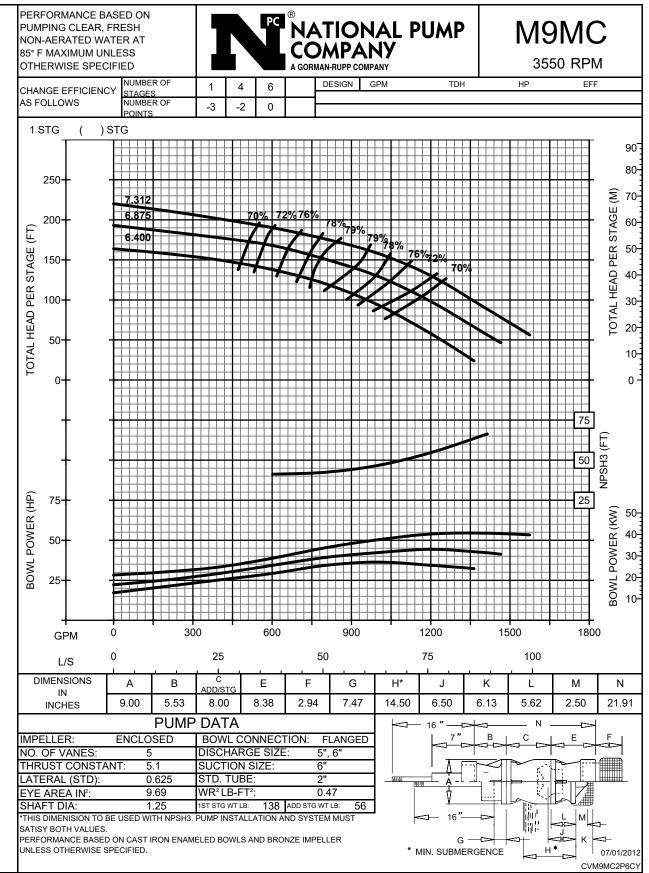


130

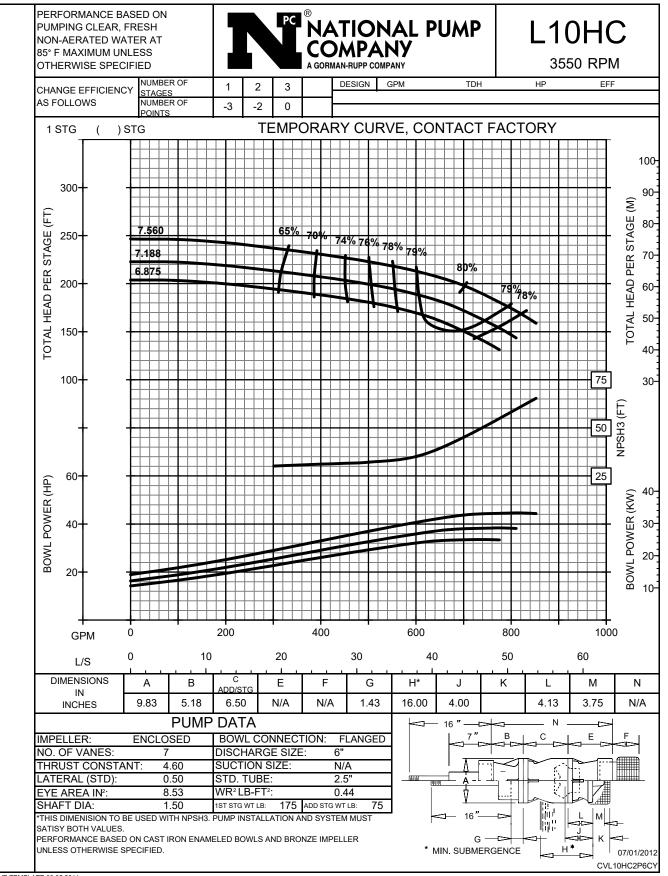




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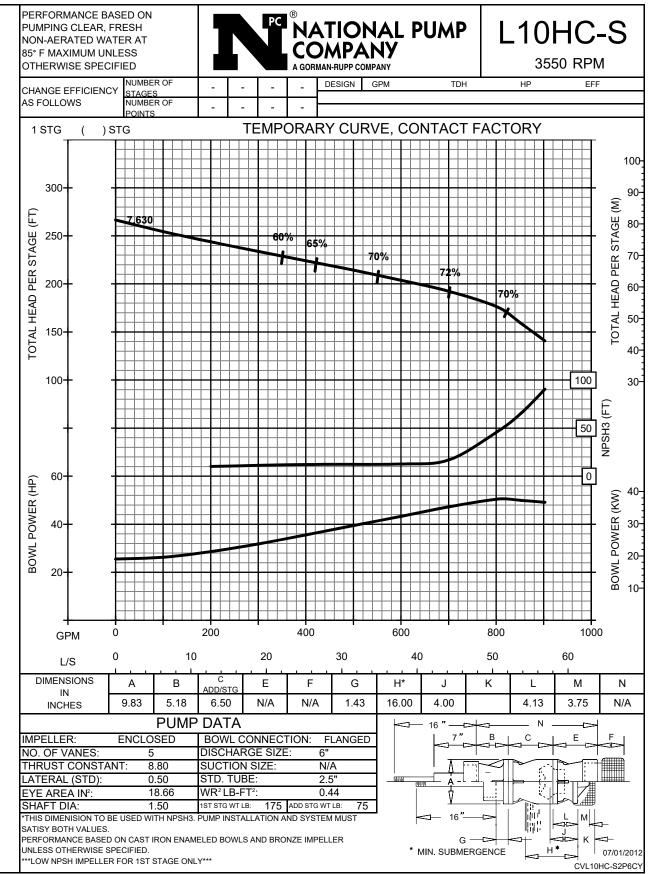




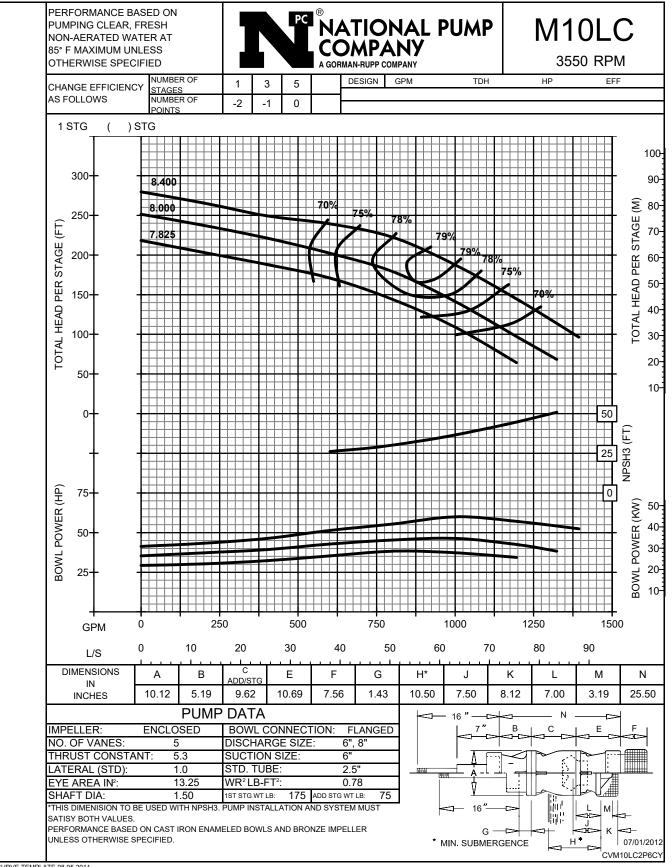


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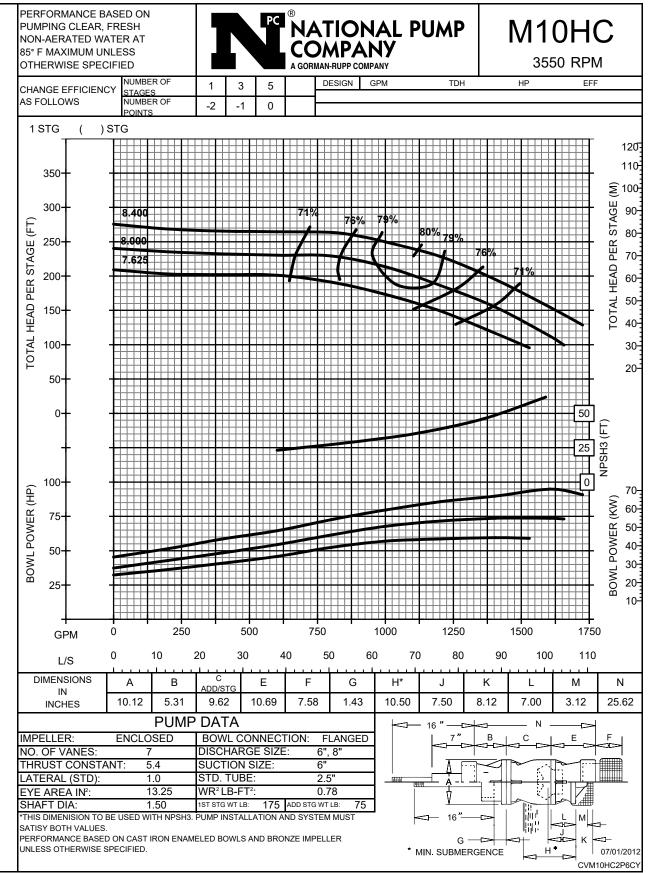
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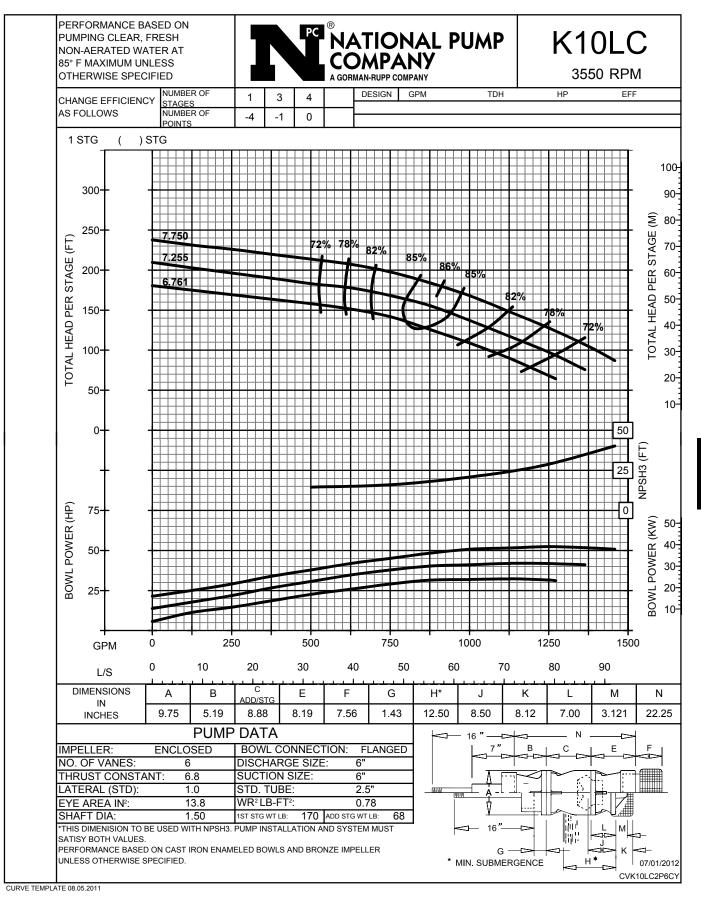




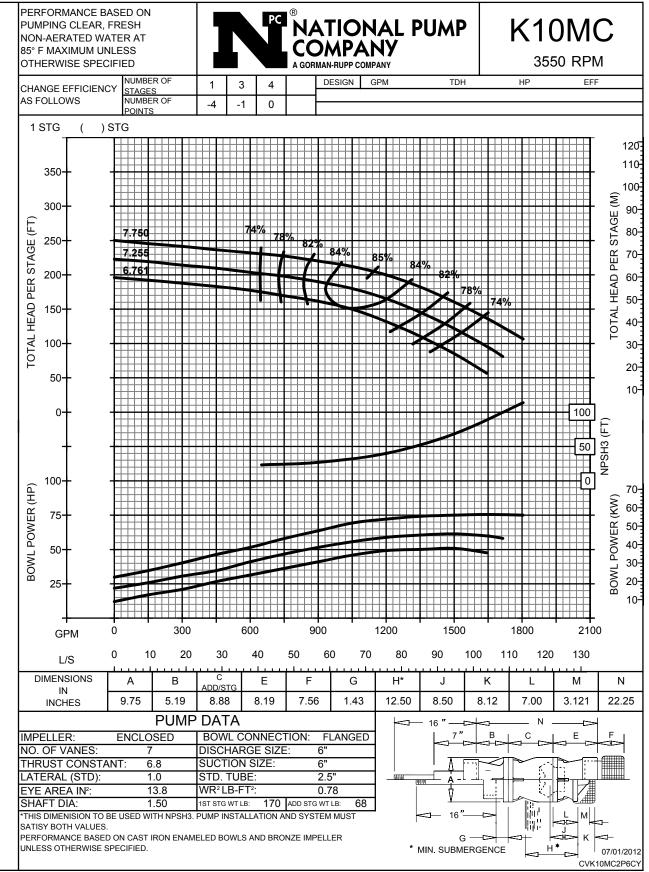
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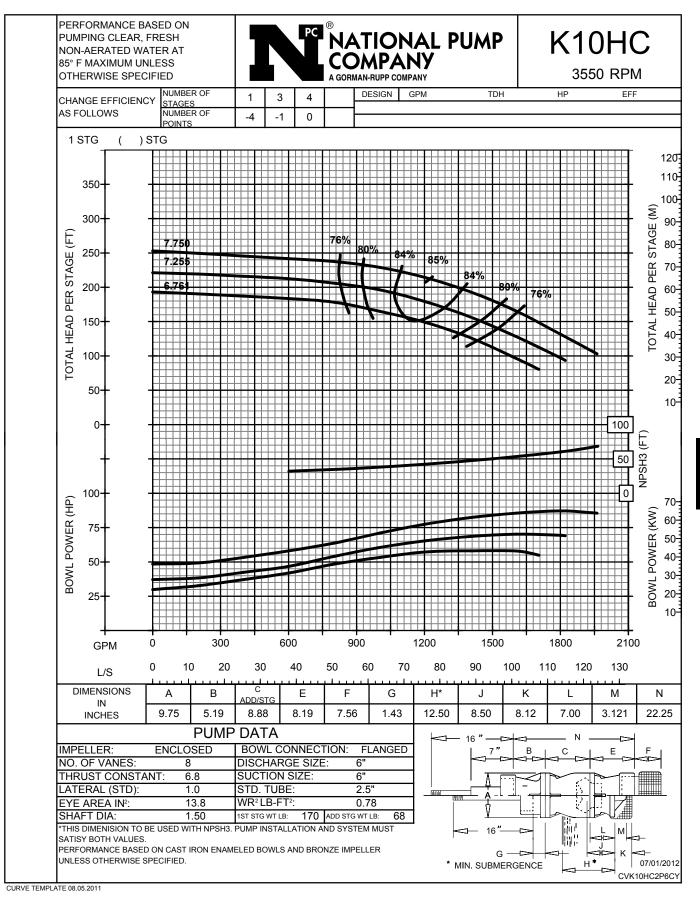




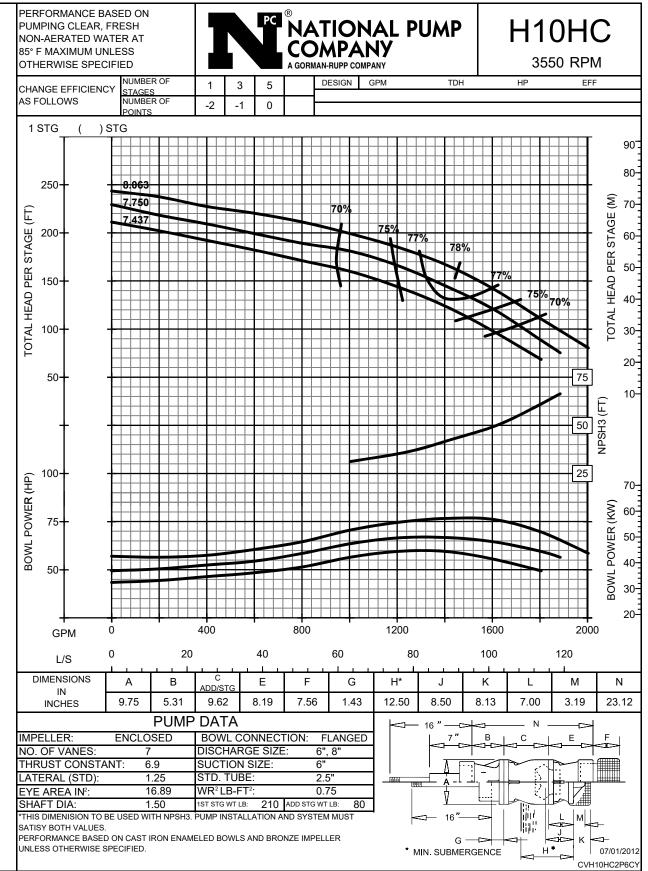


CURVES



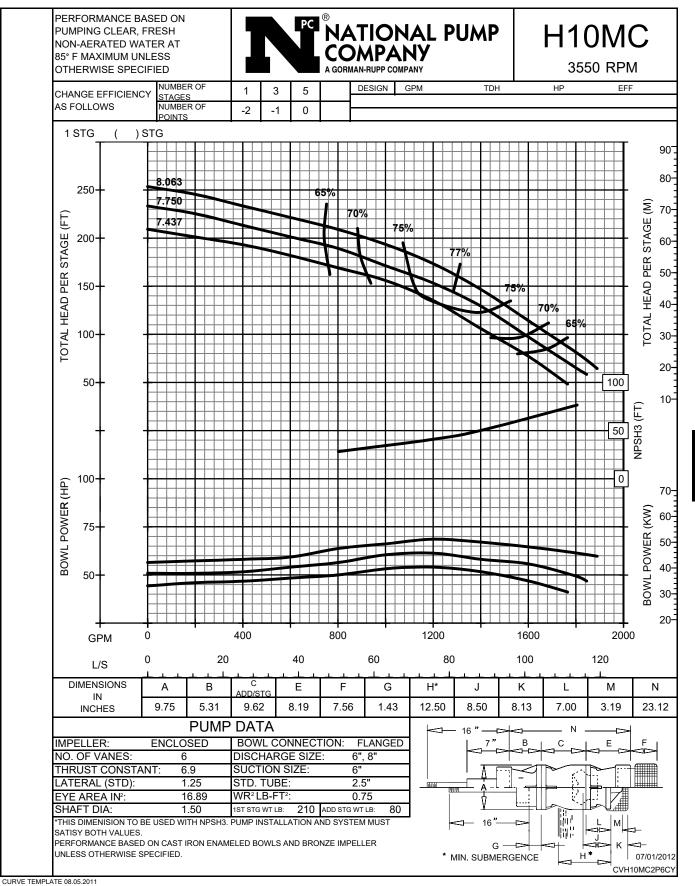


CURVES

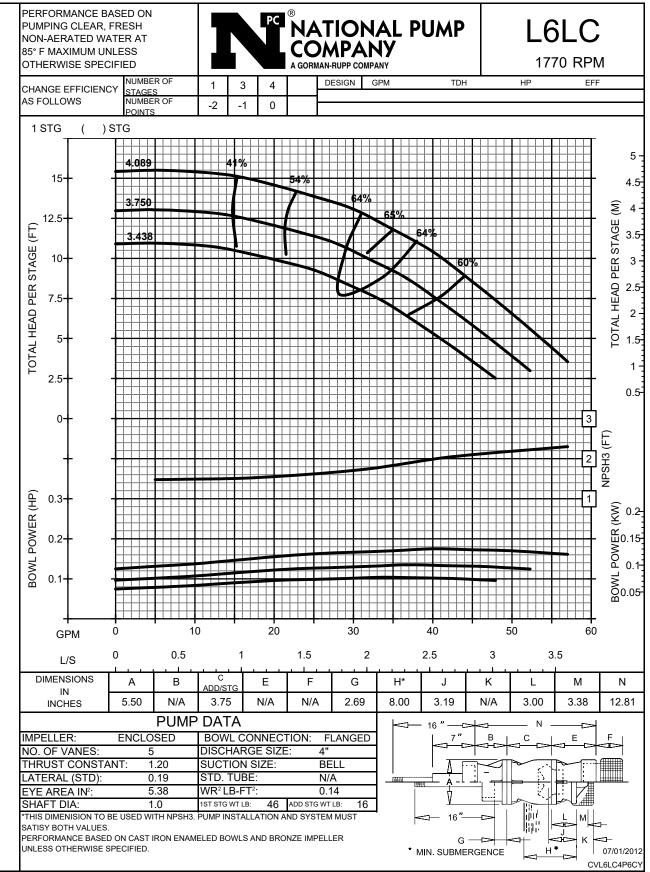


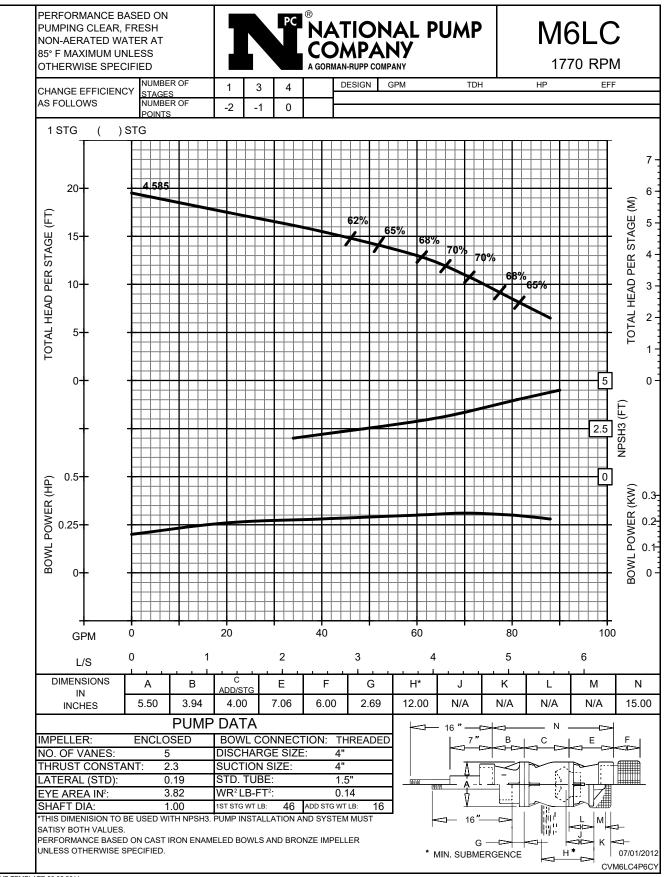




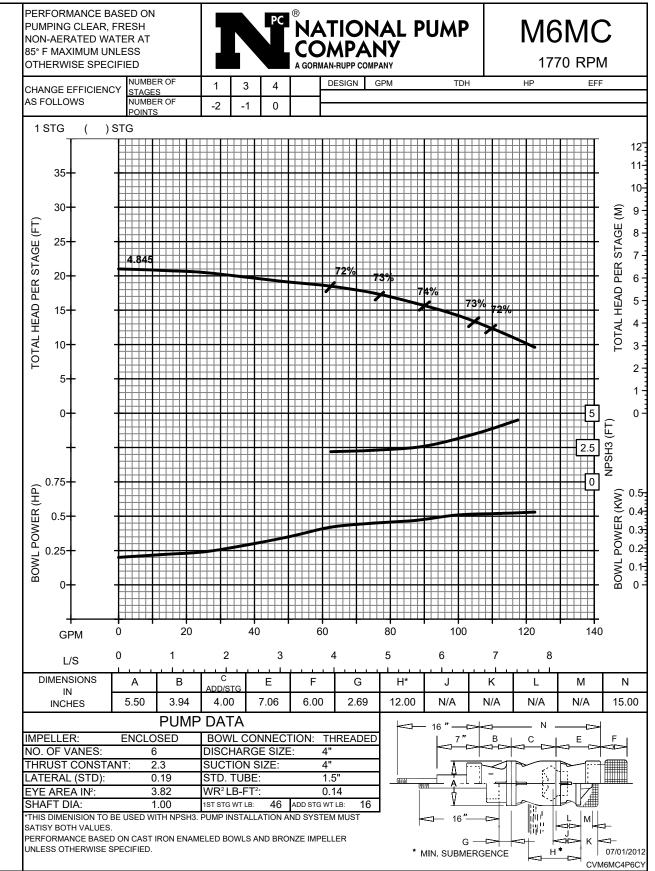


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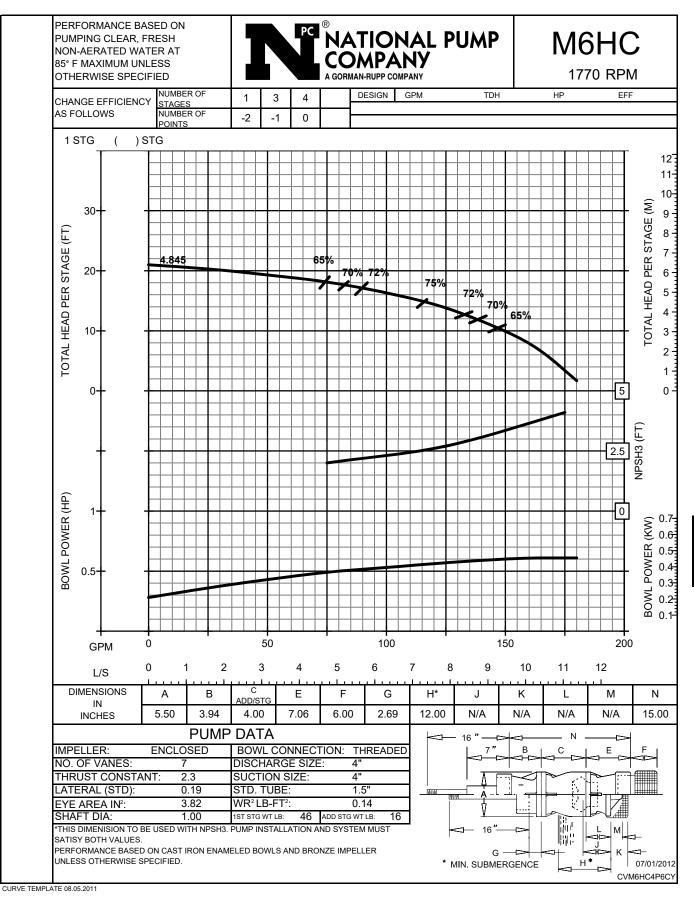


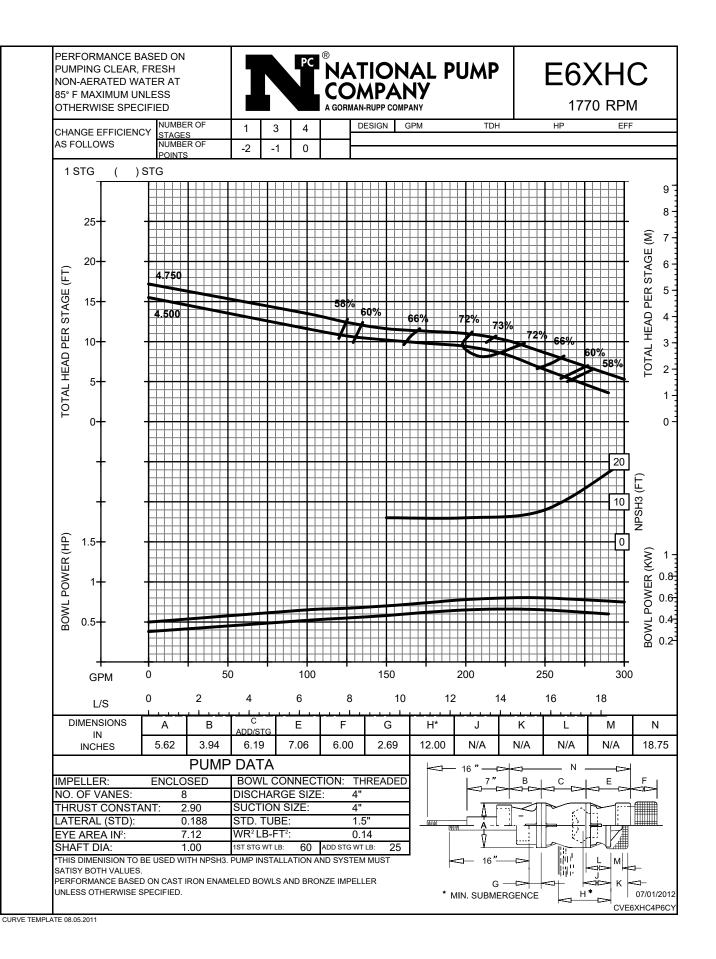


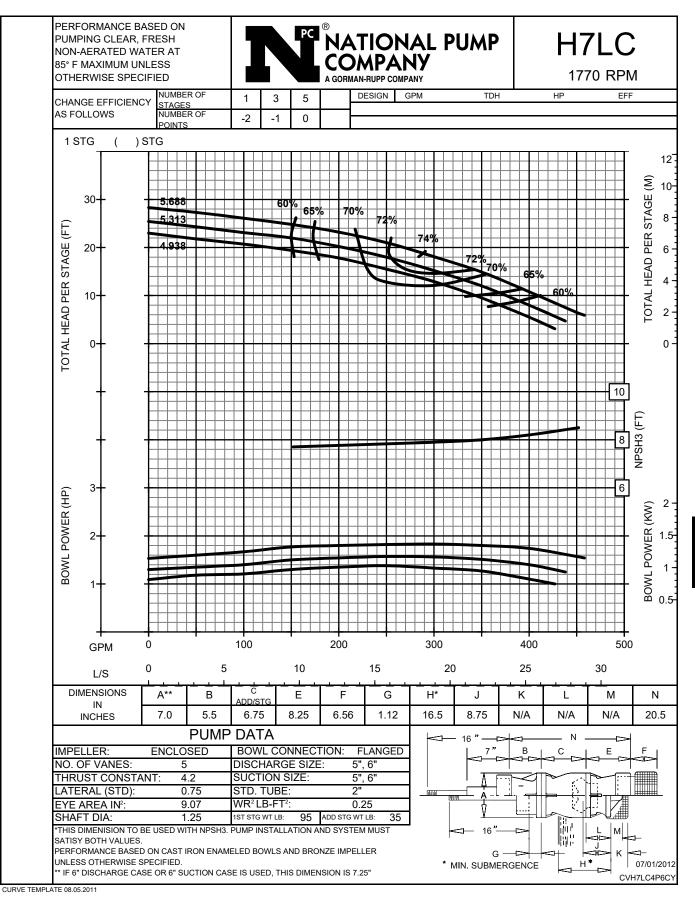
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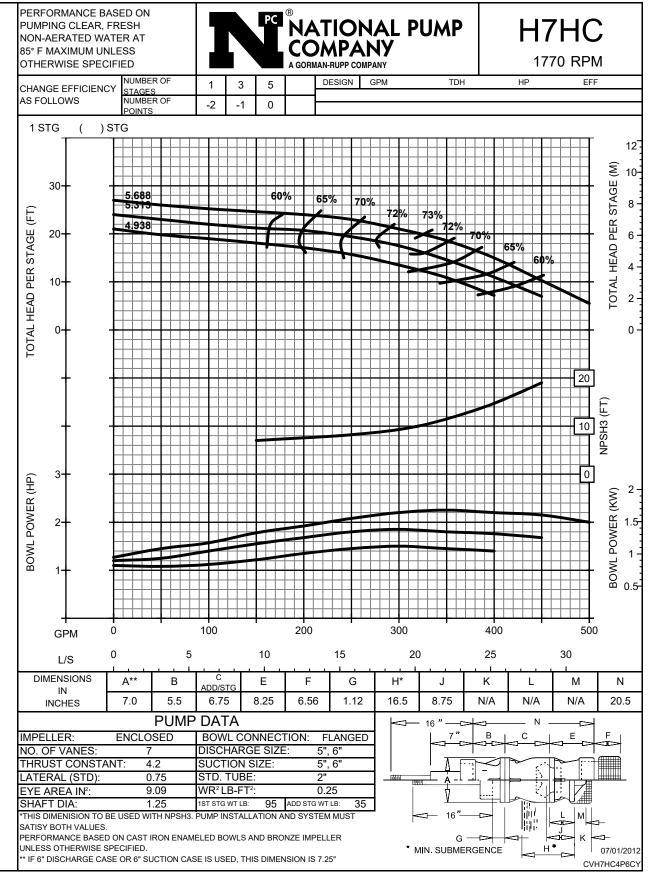


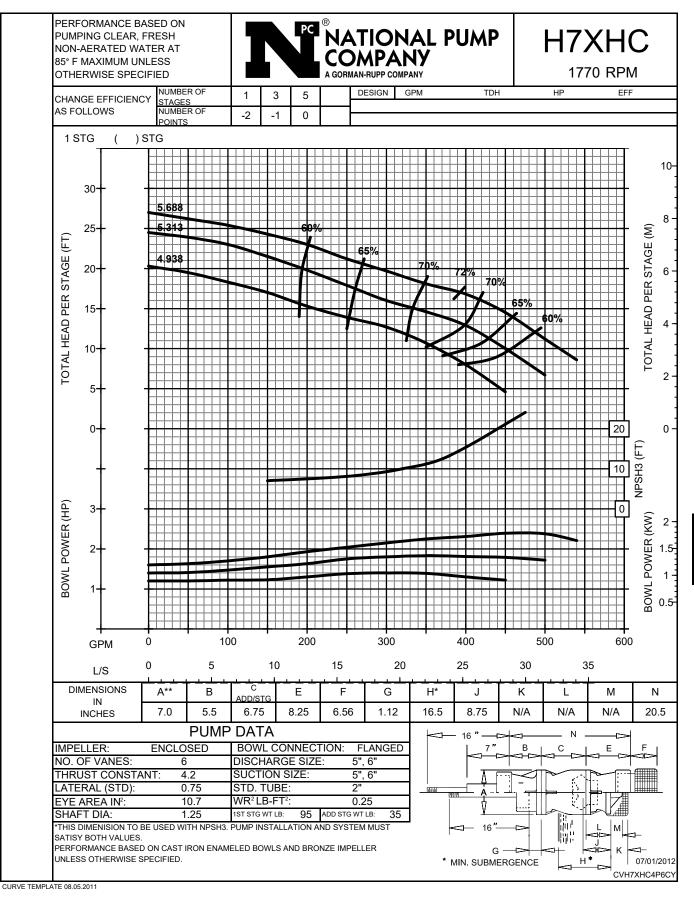


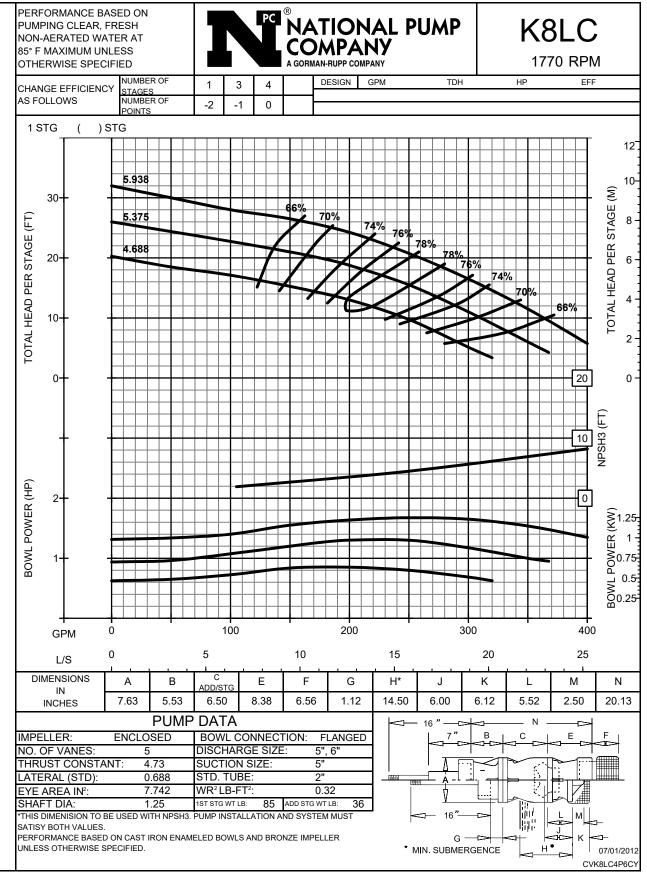


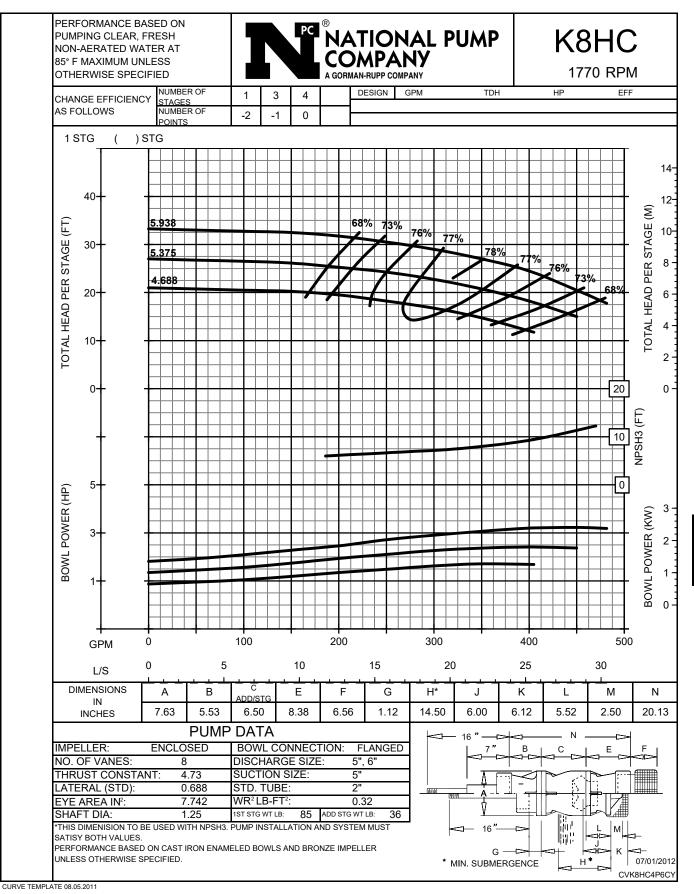


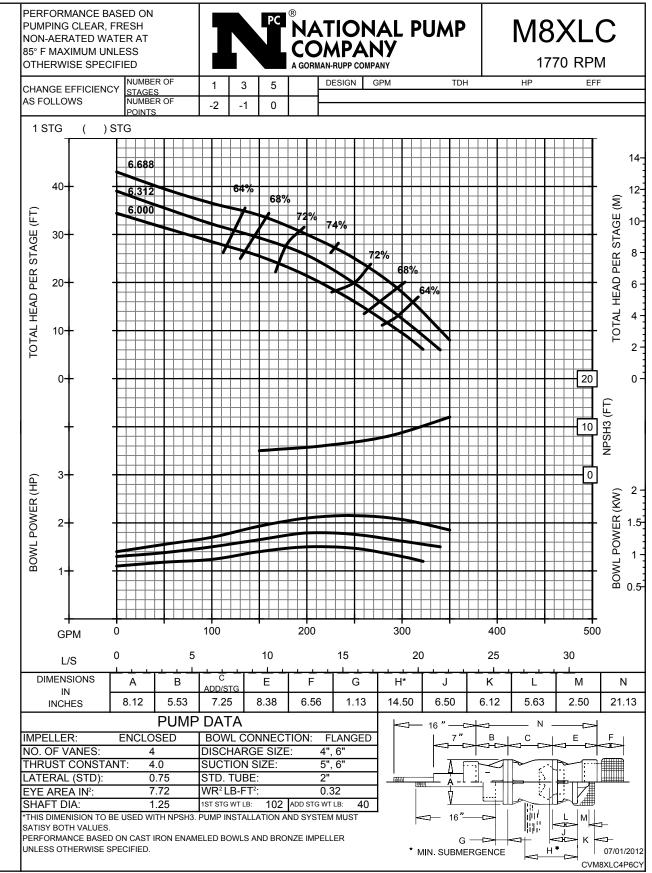




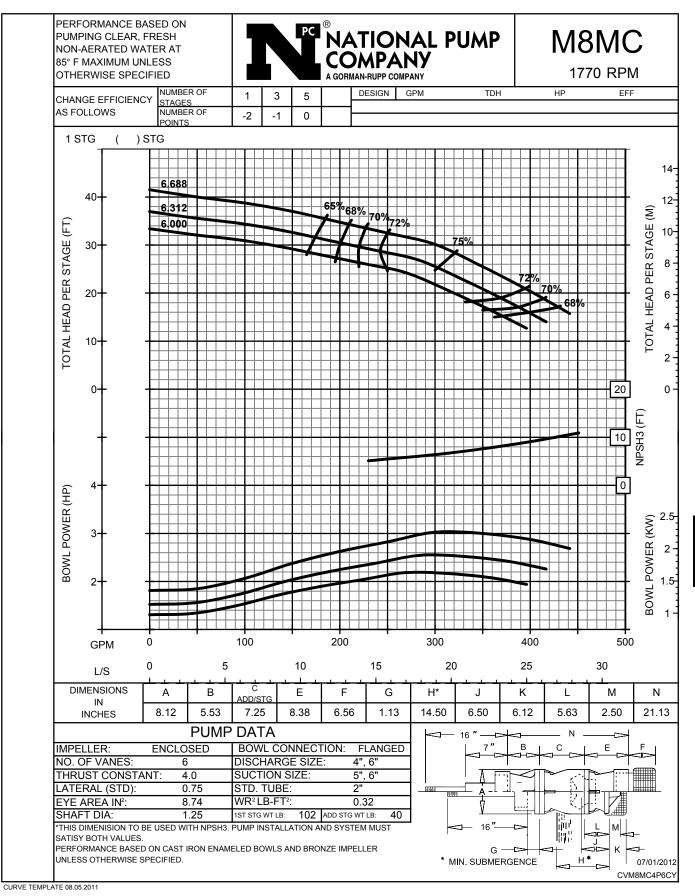


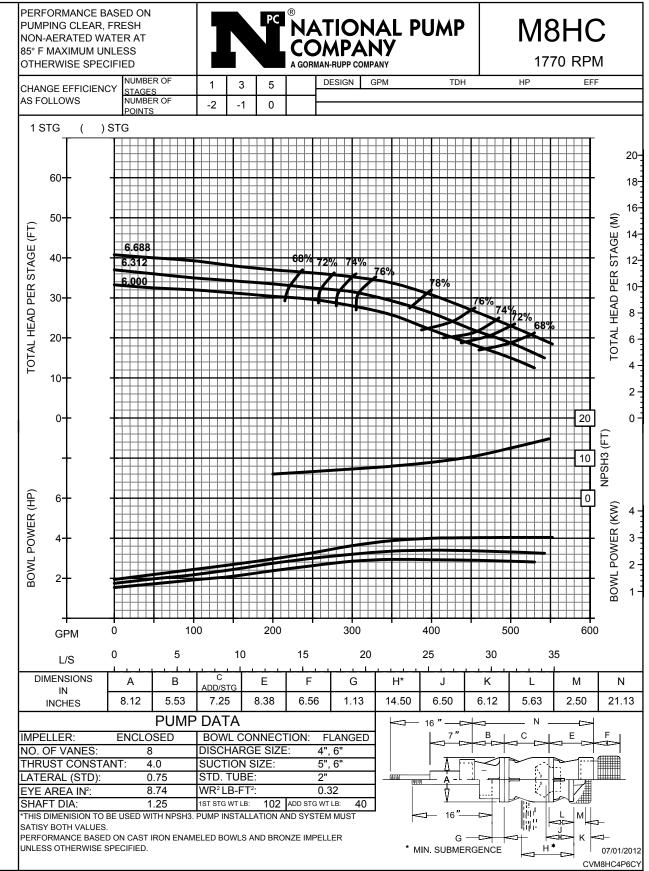


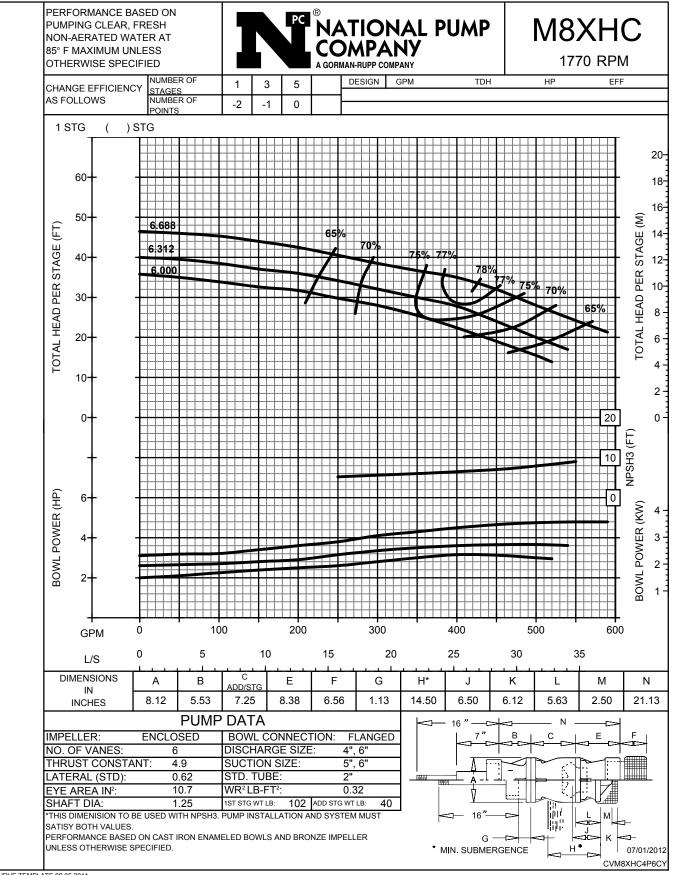


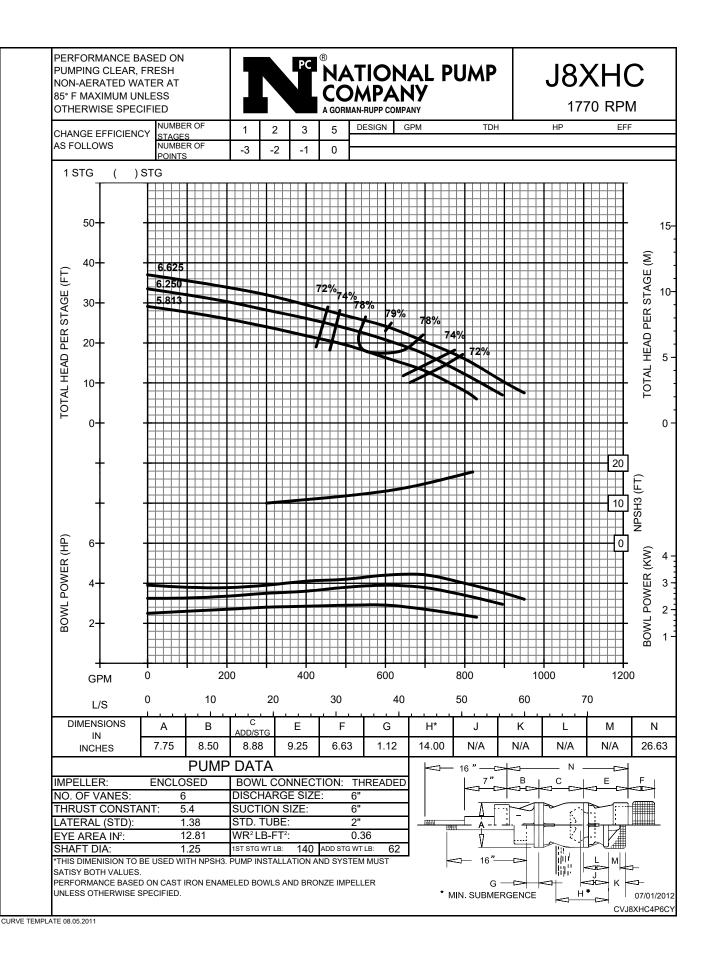


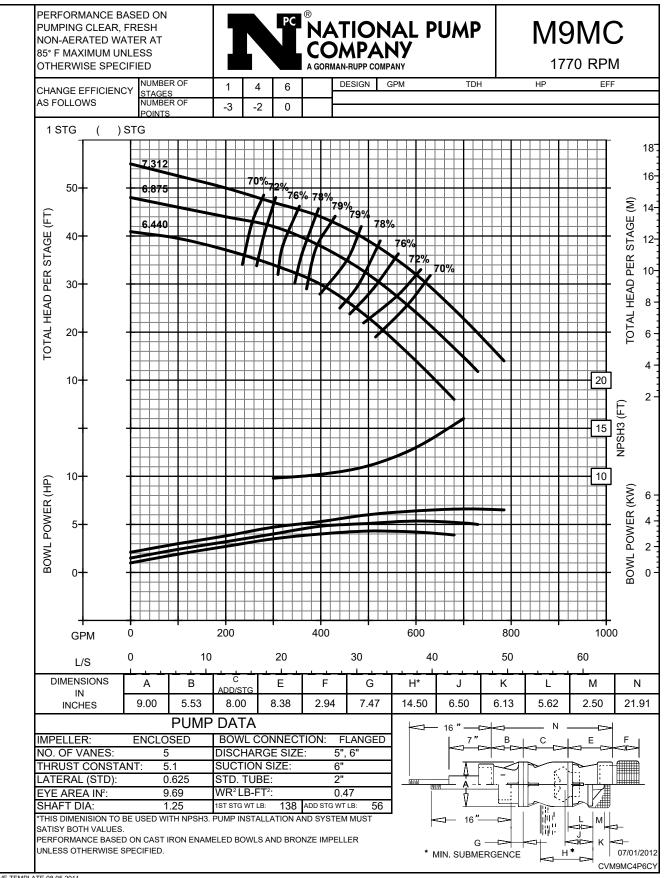




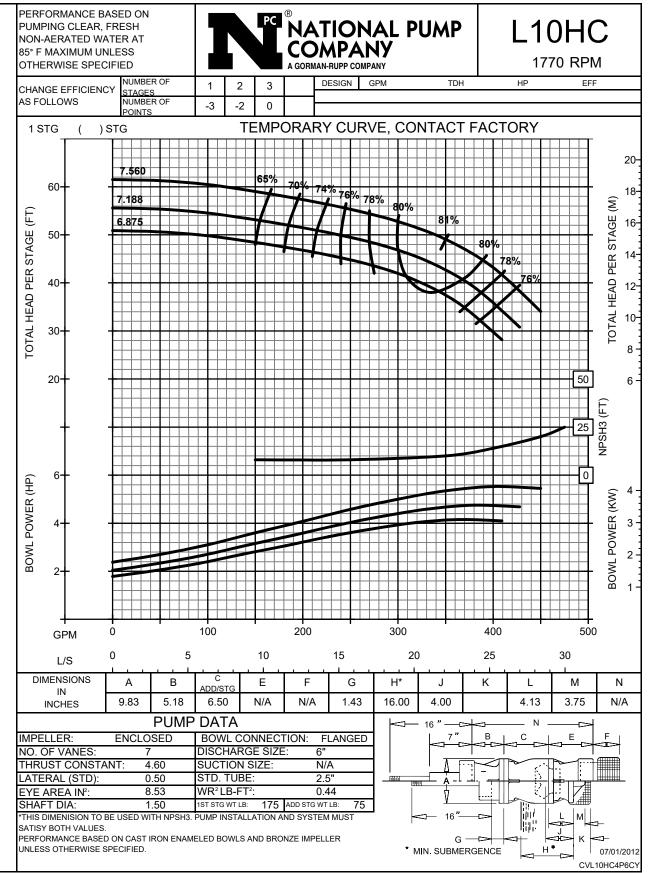




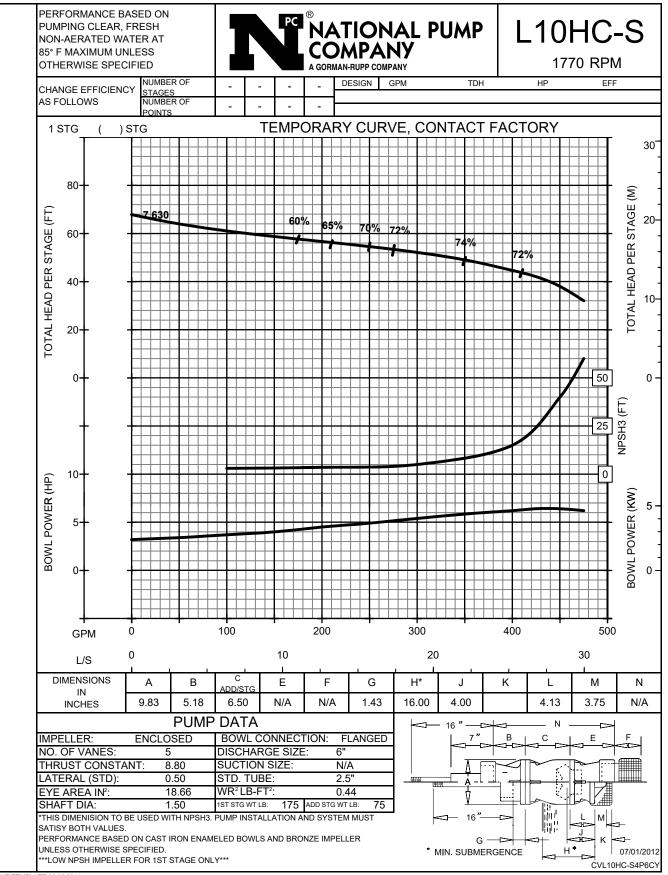




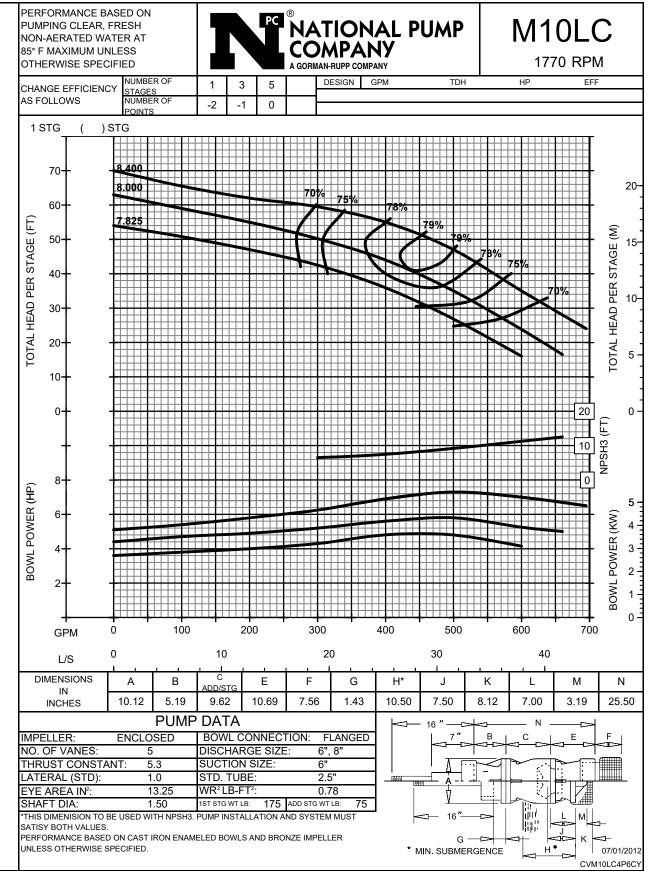
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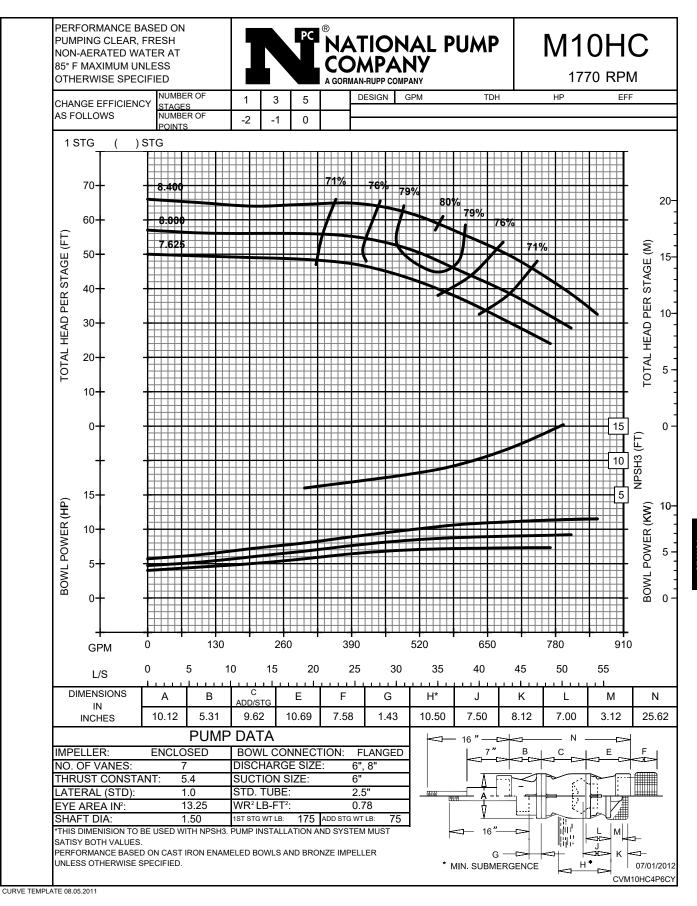


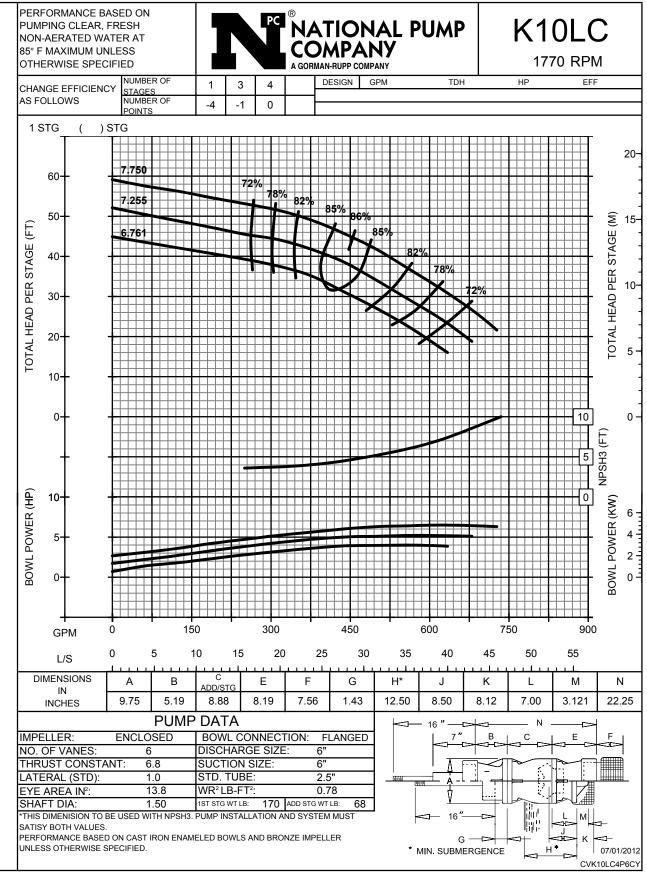


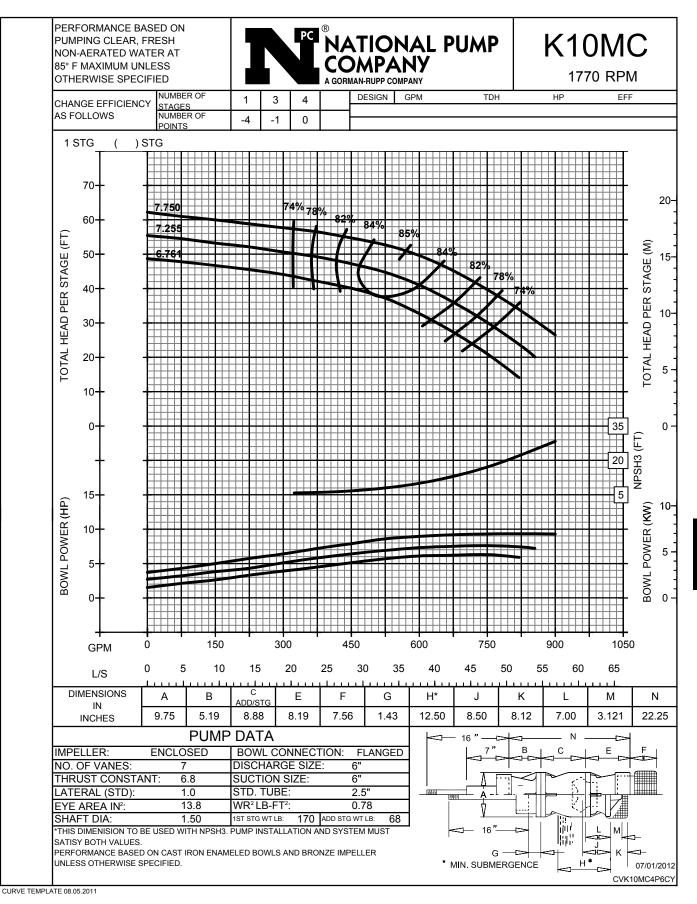


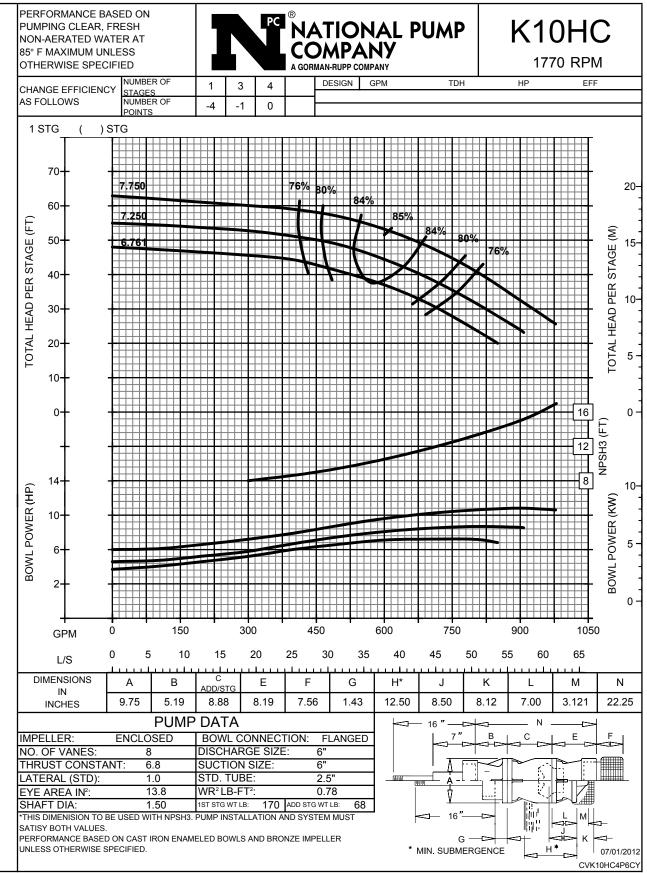
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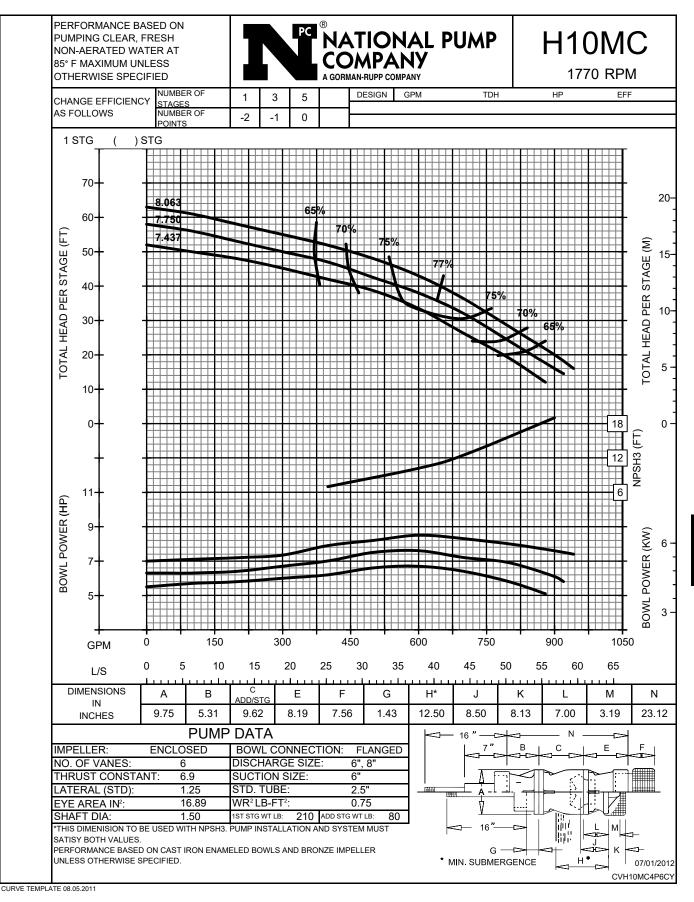




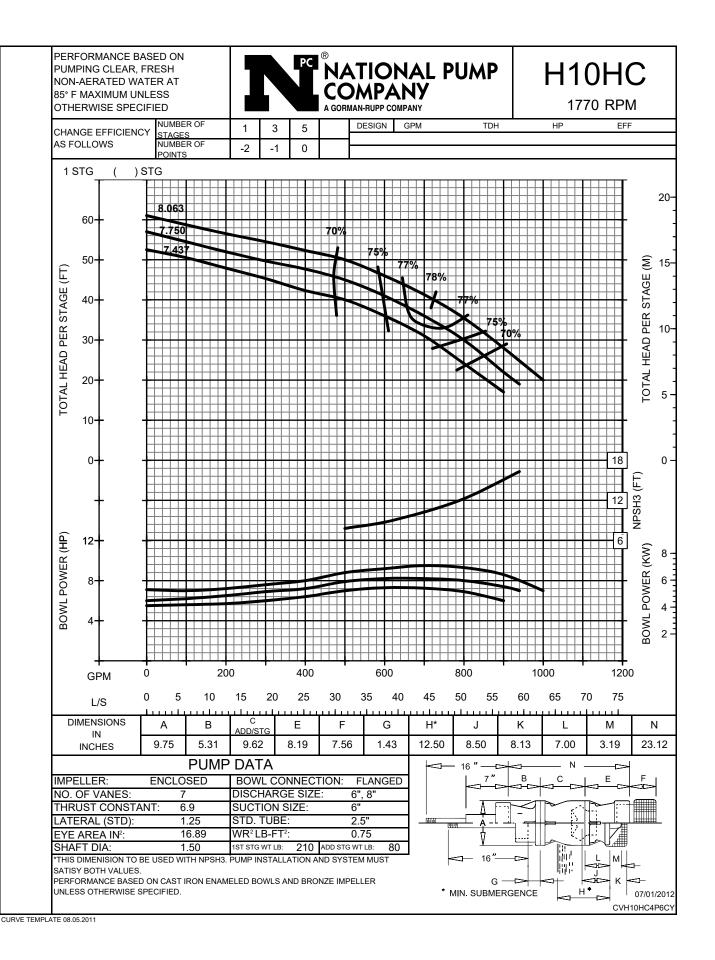


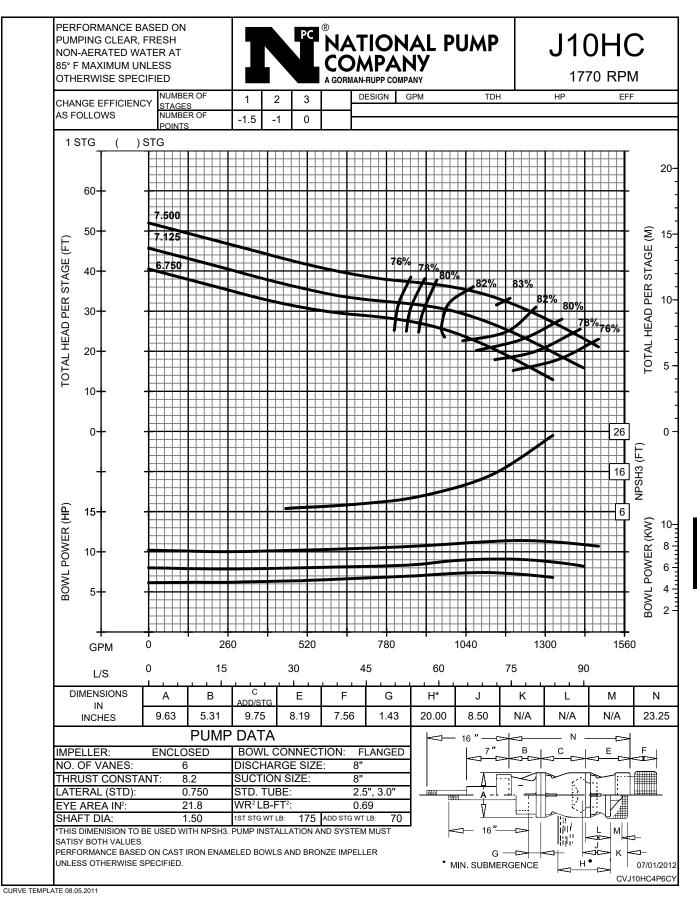


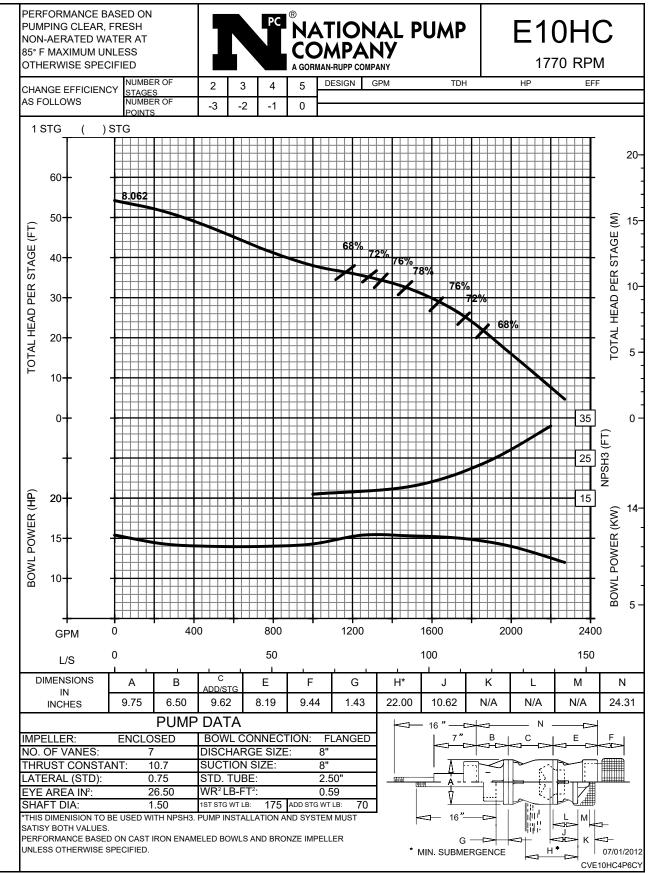


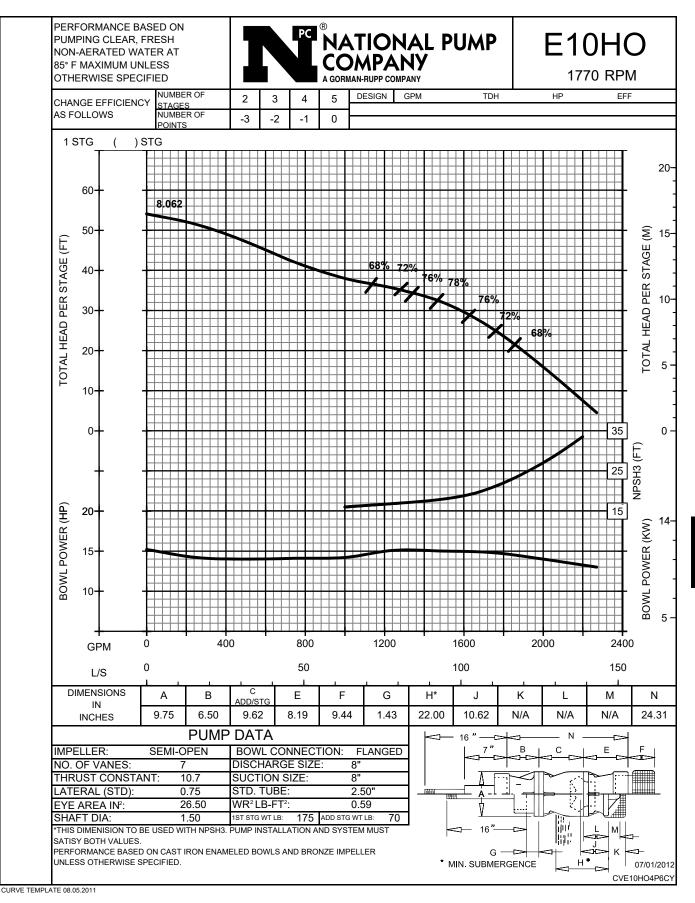


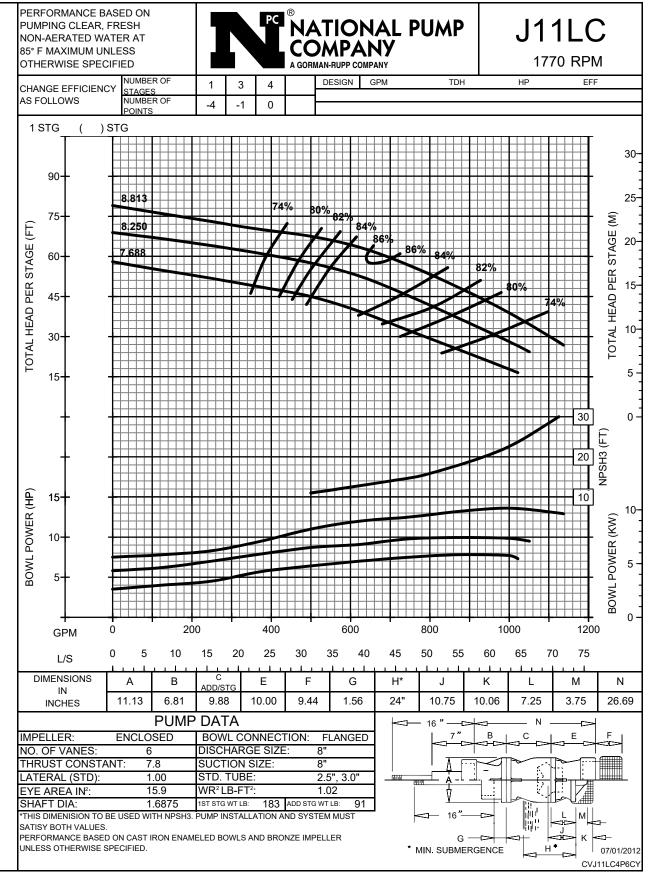


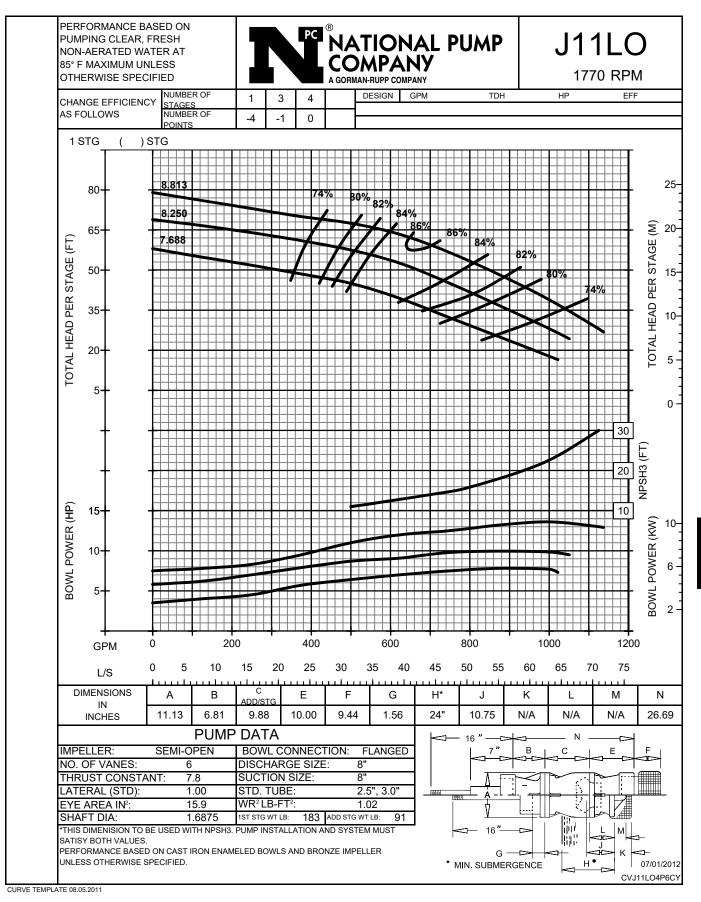


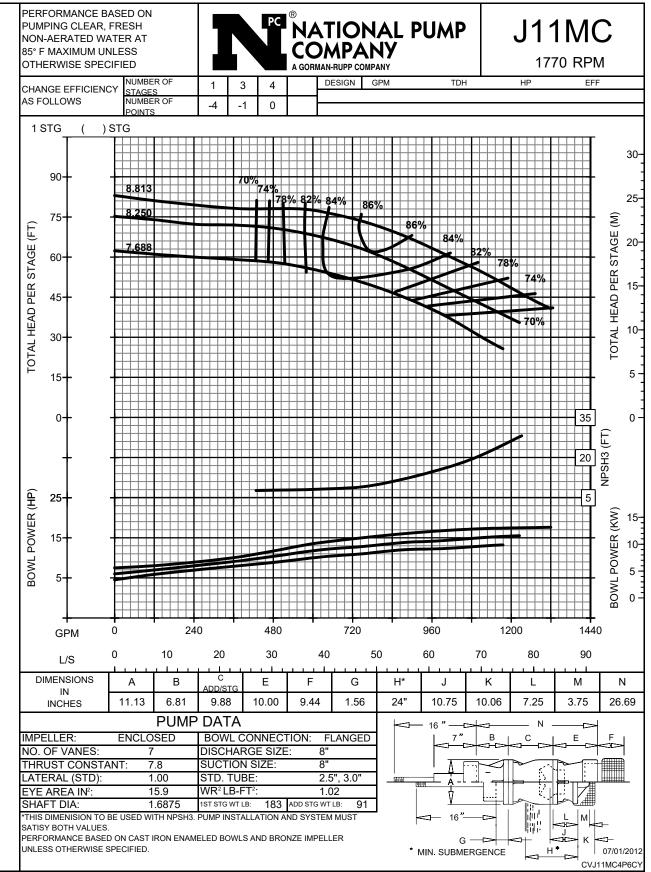


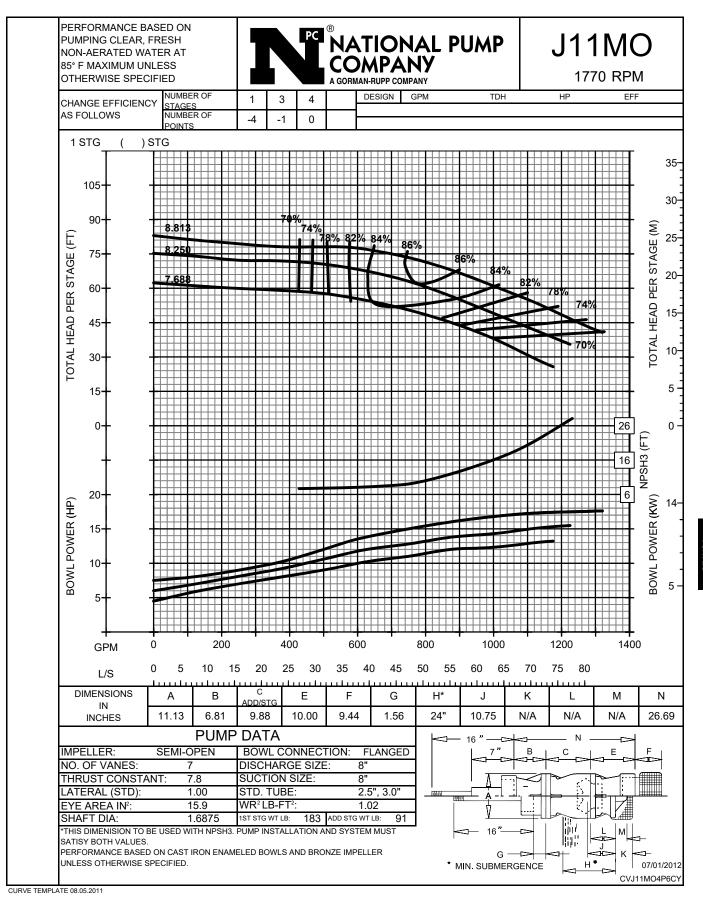


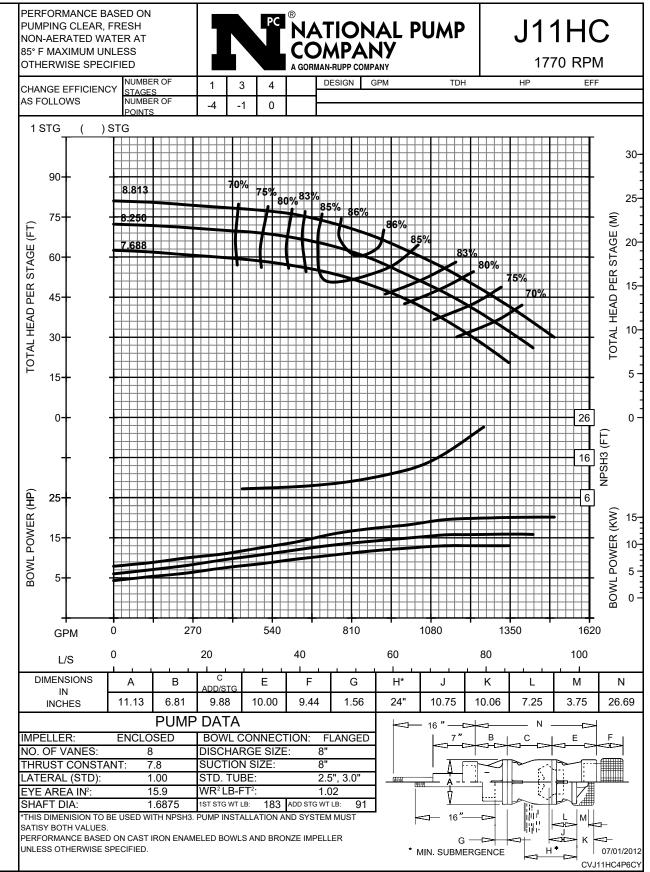


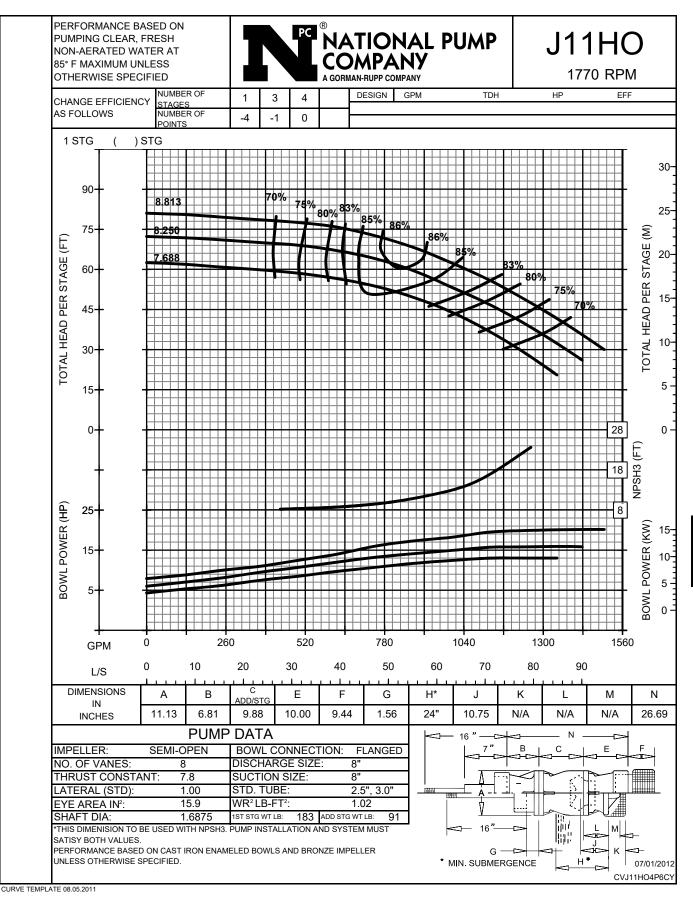


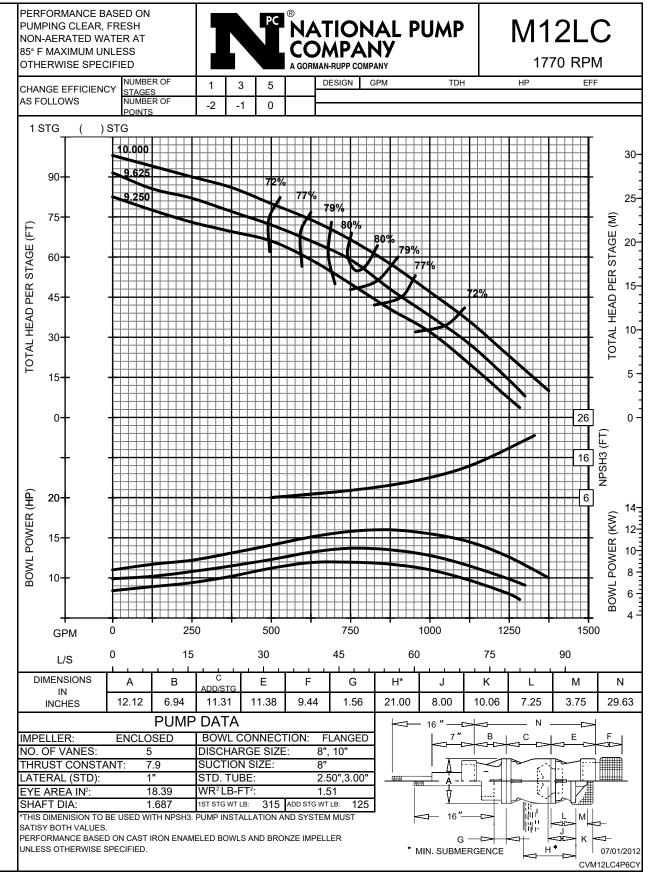


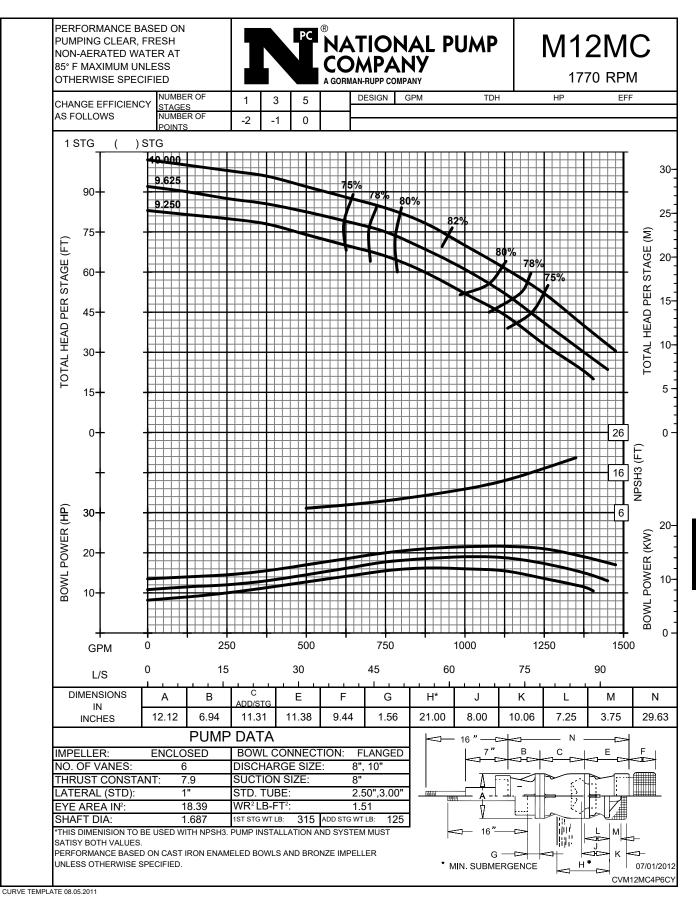


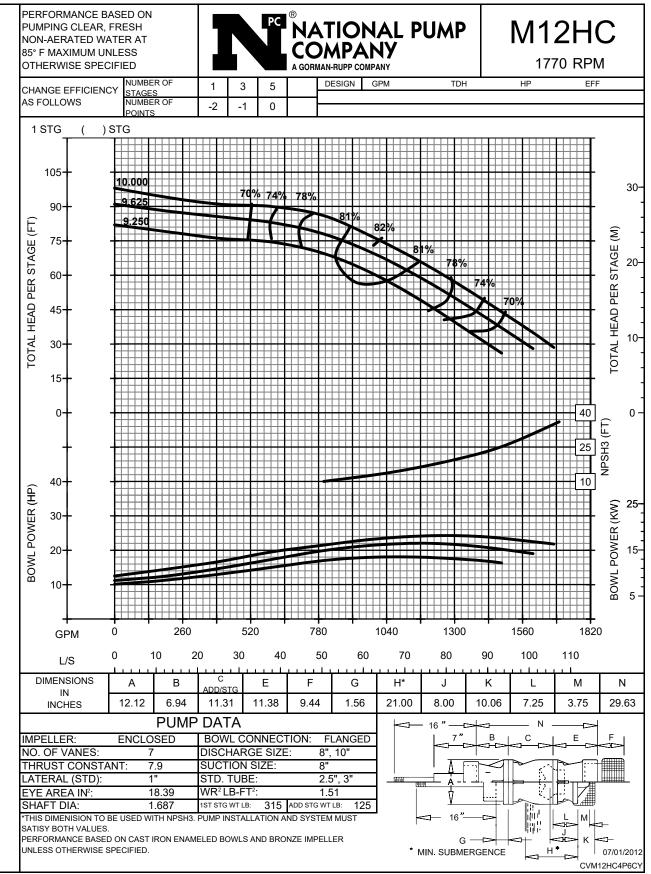


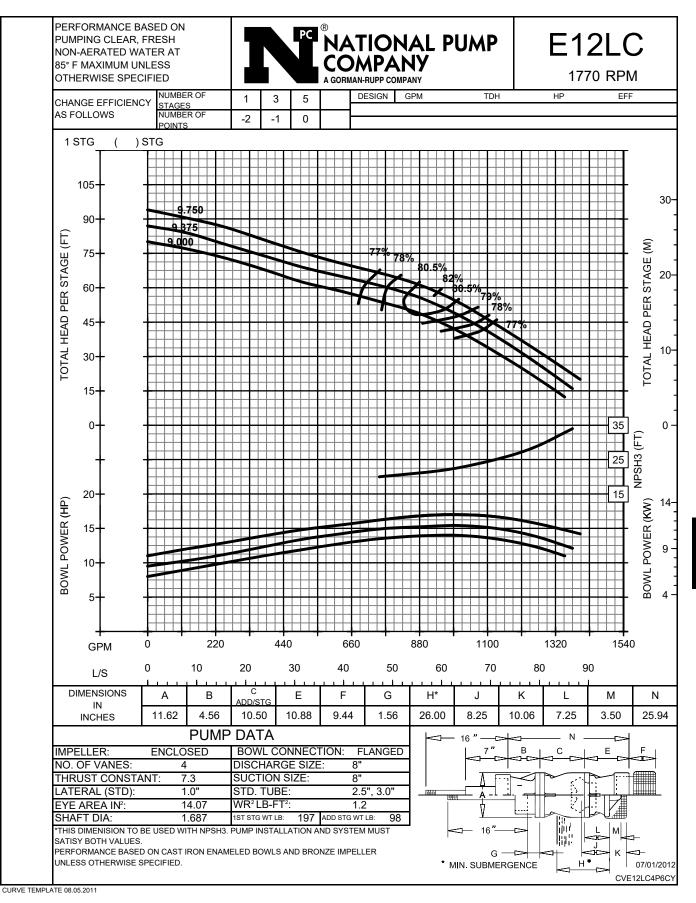


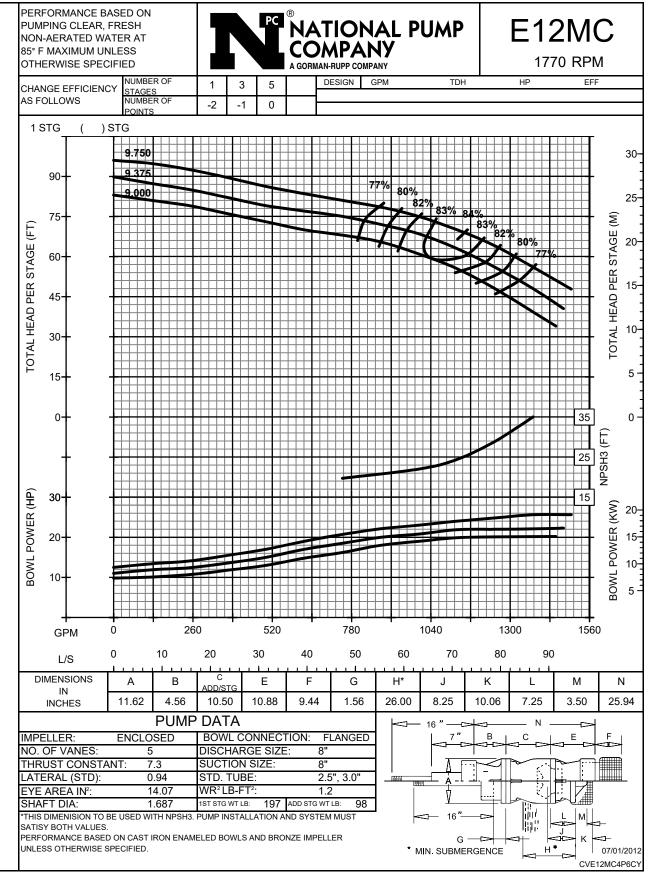


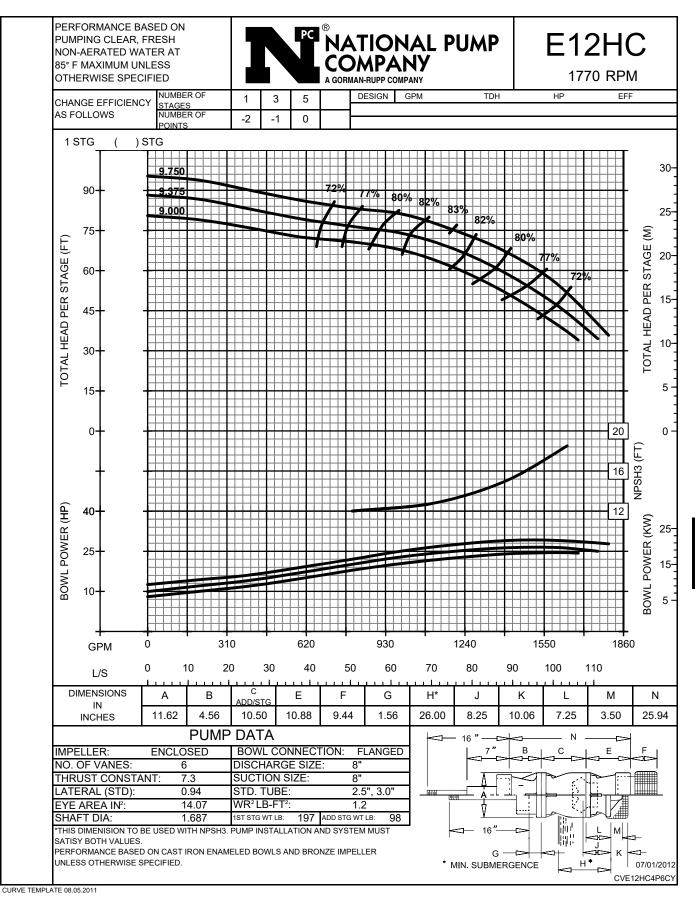


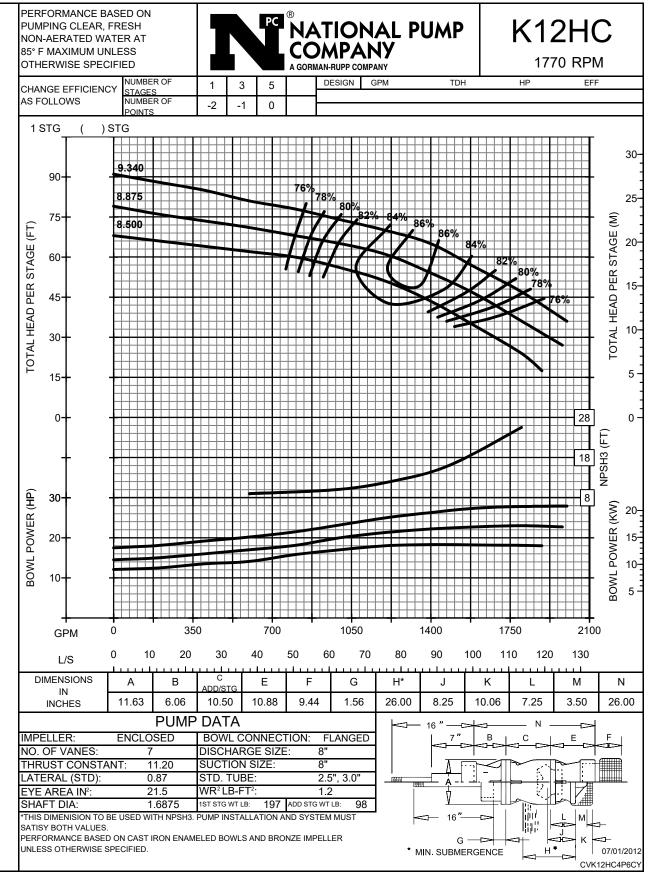




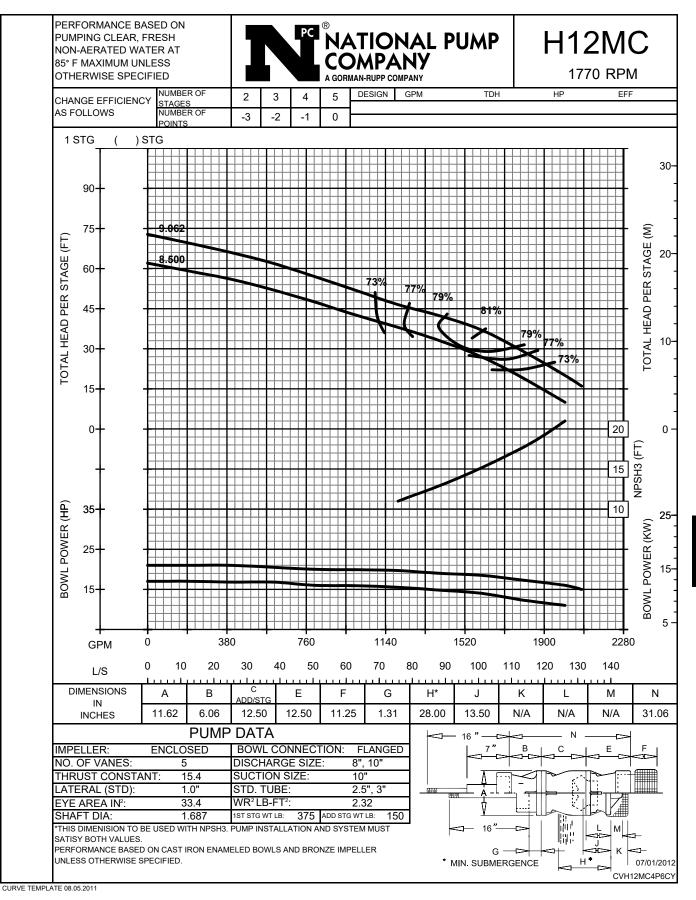


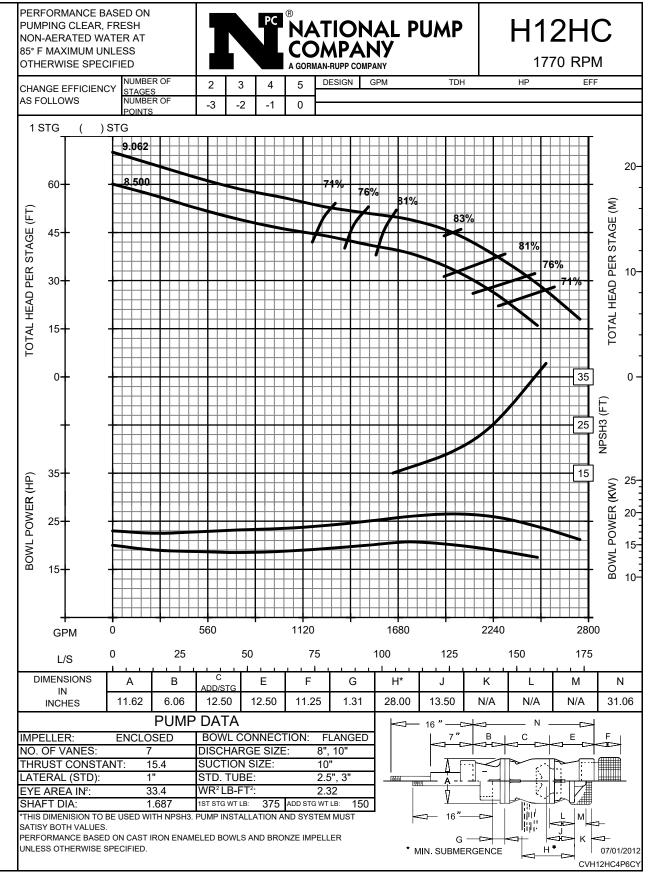


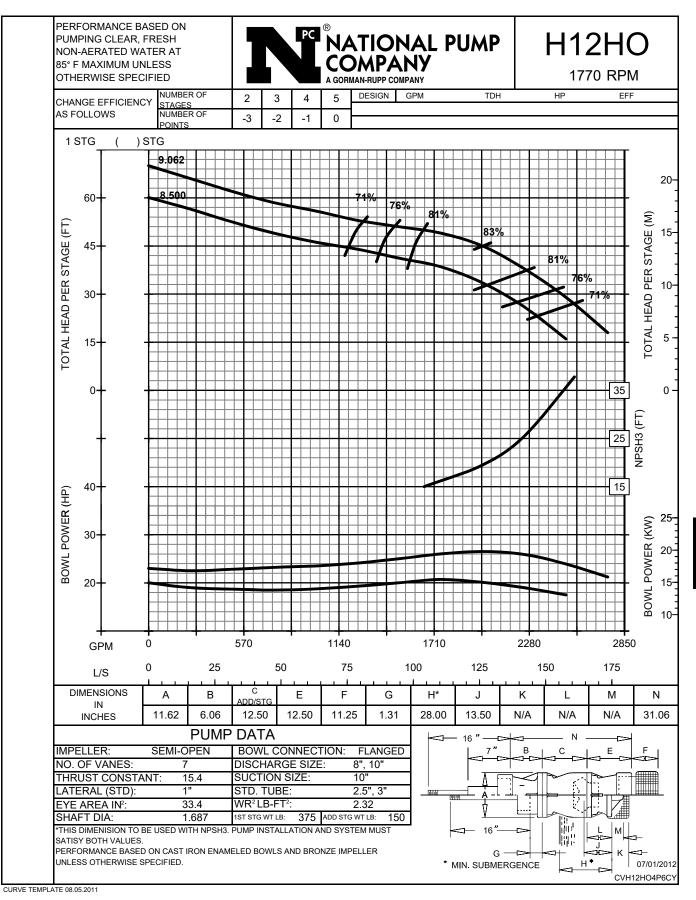


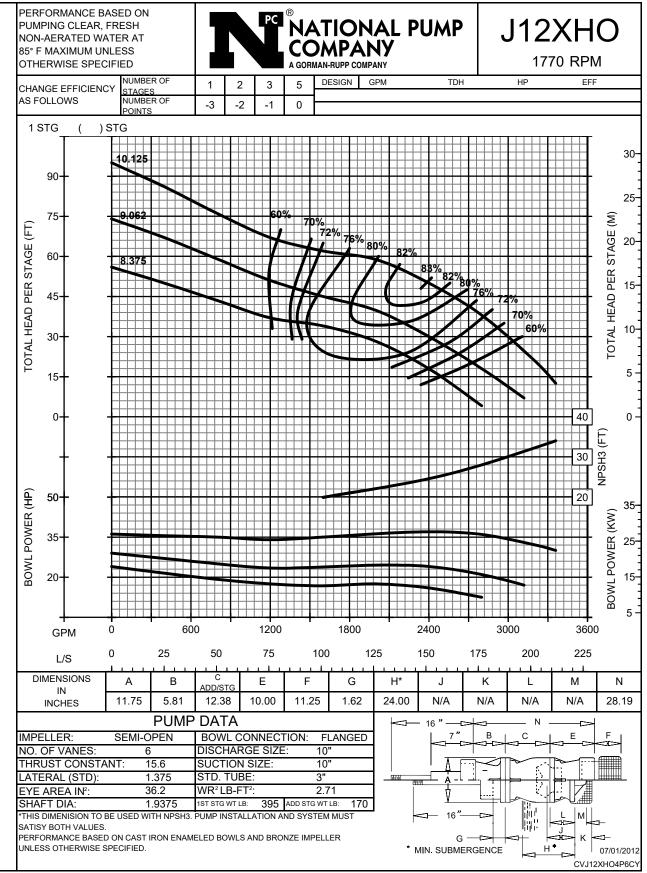


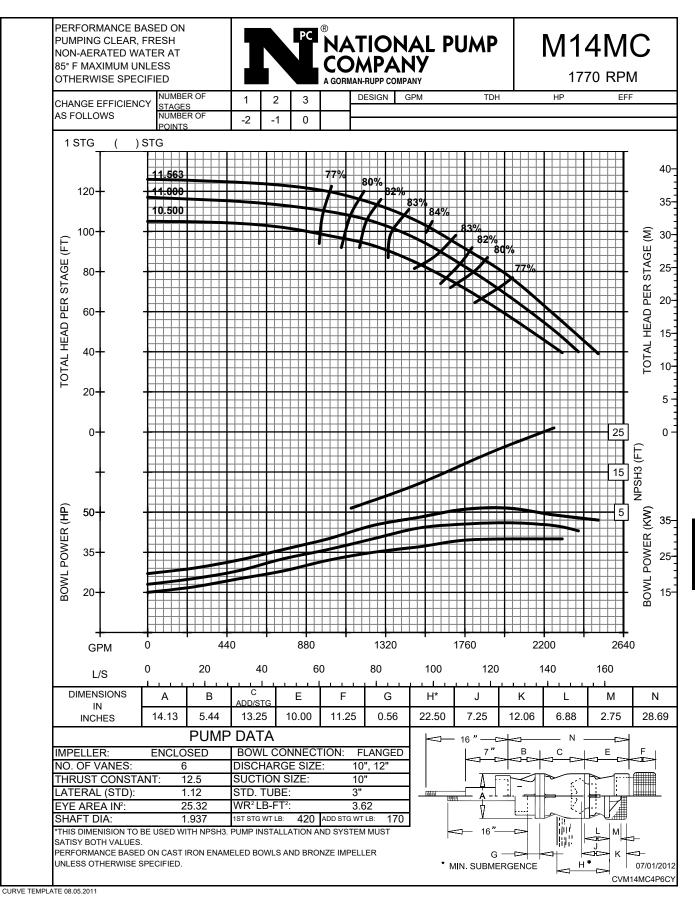


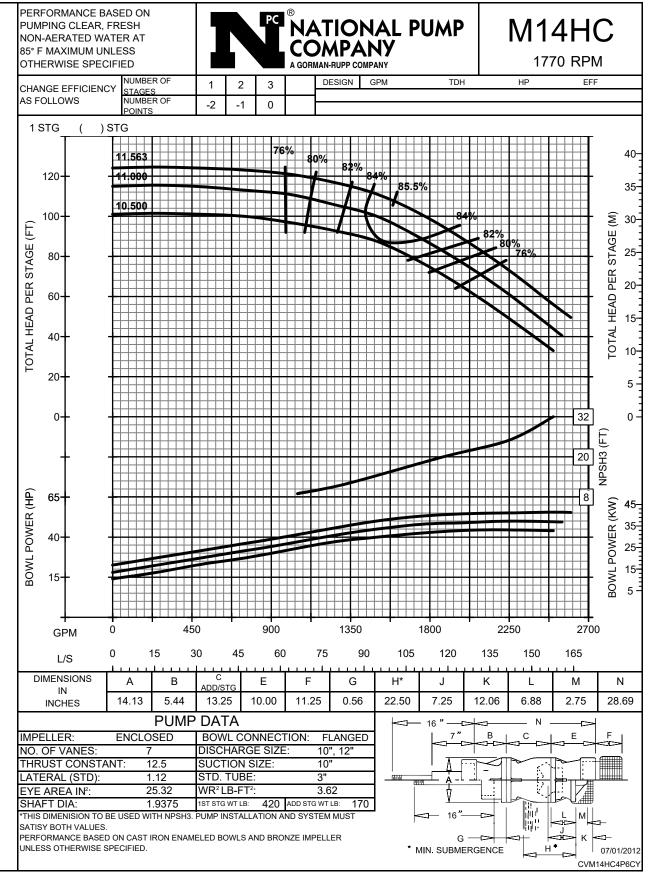


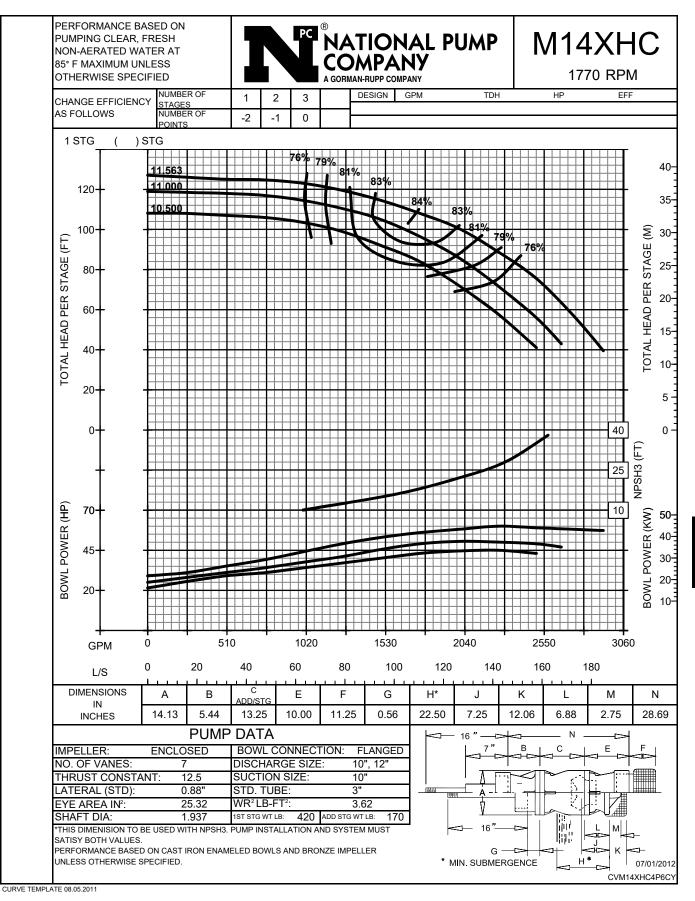


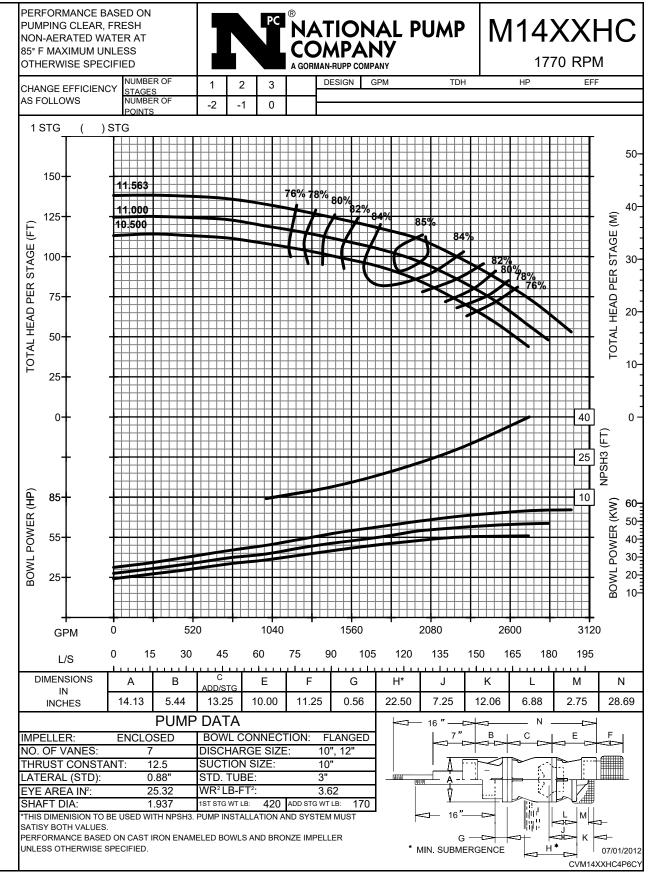


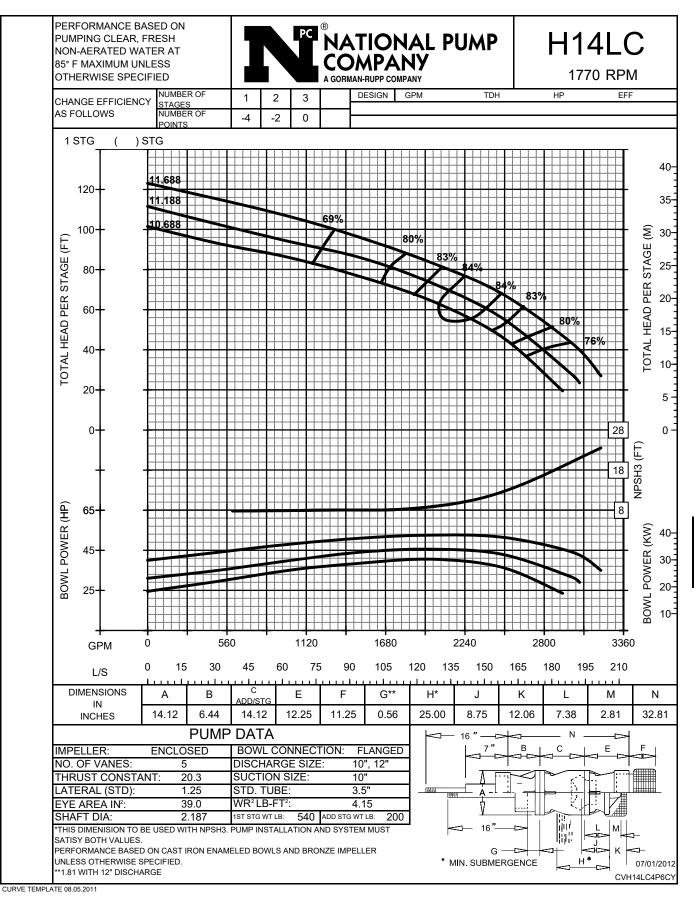


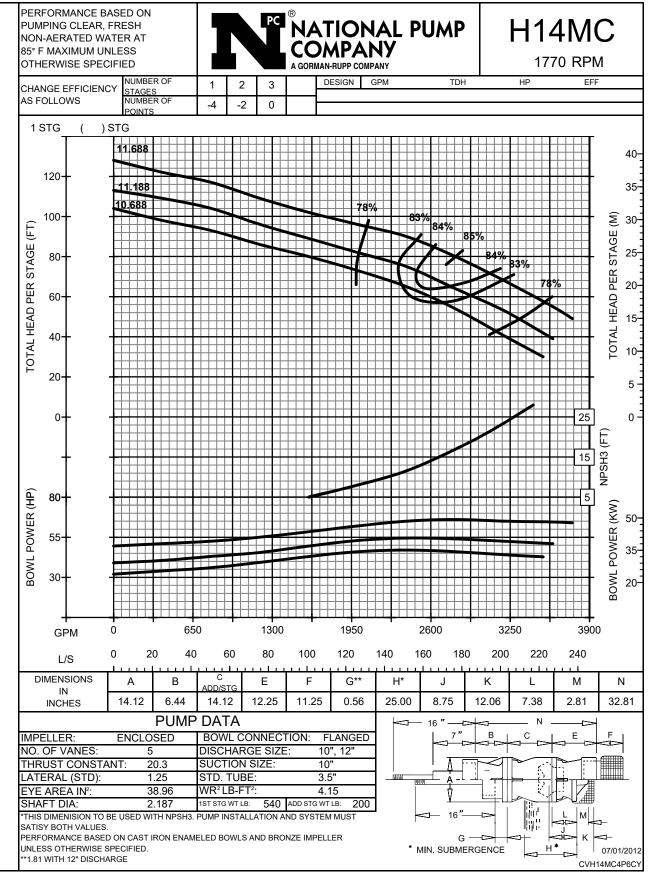


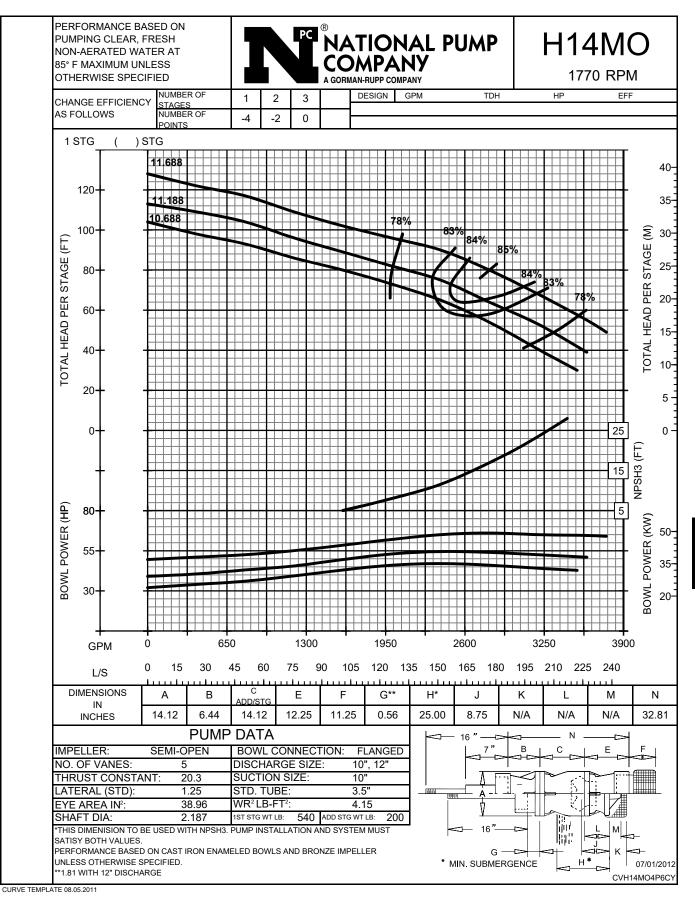




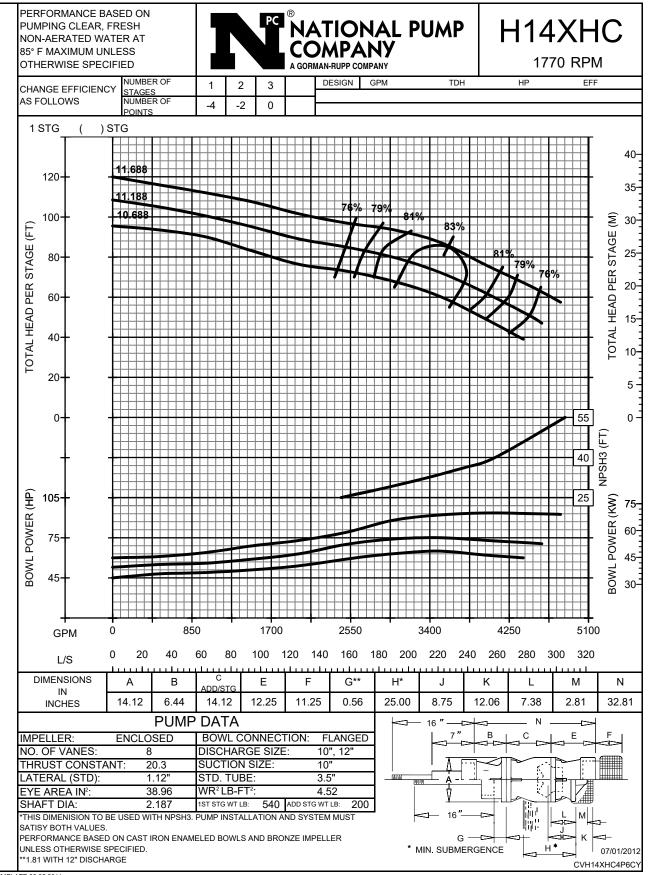




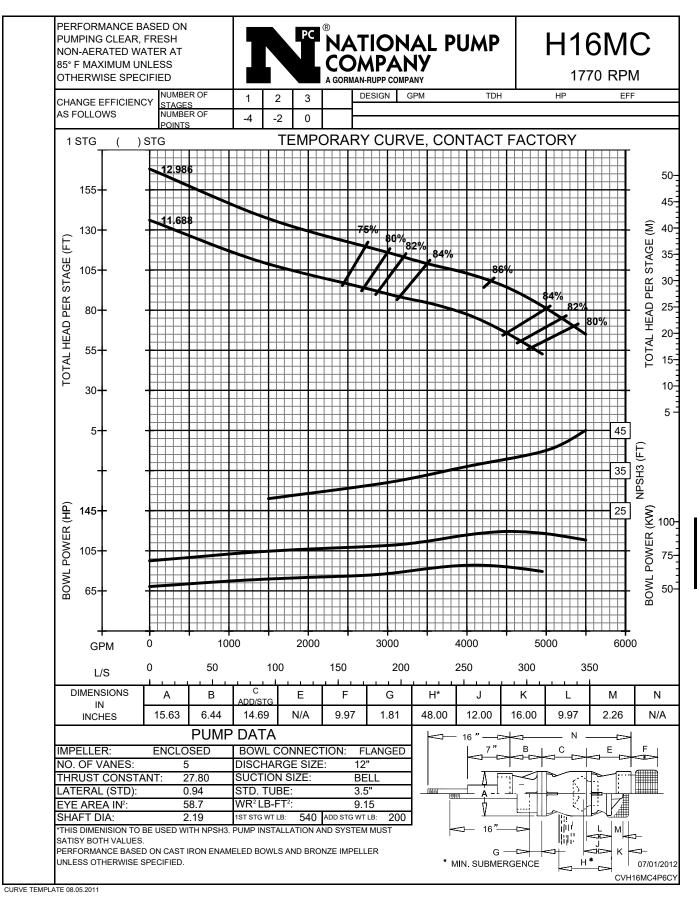




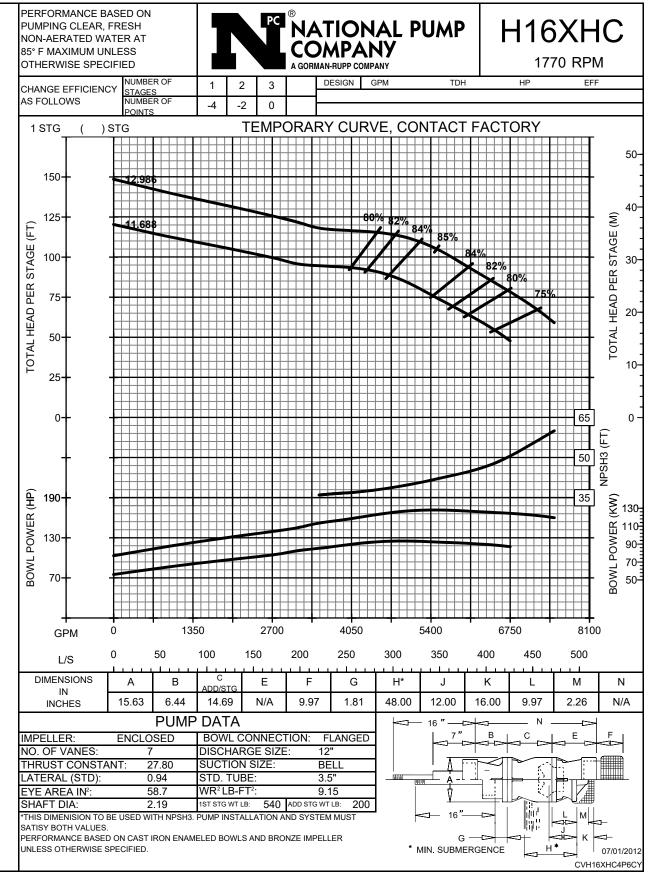


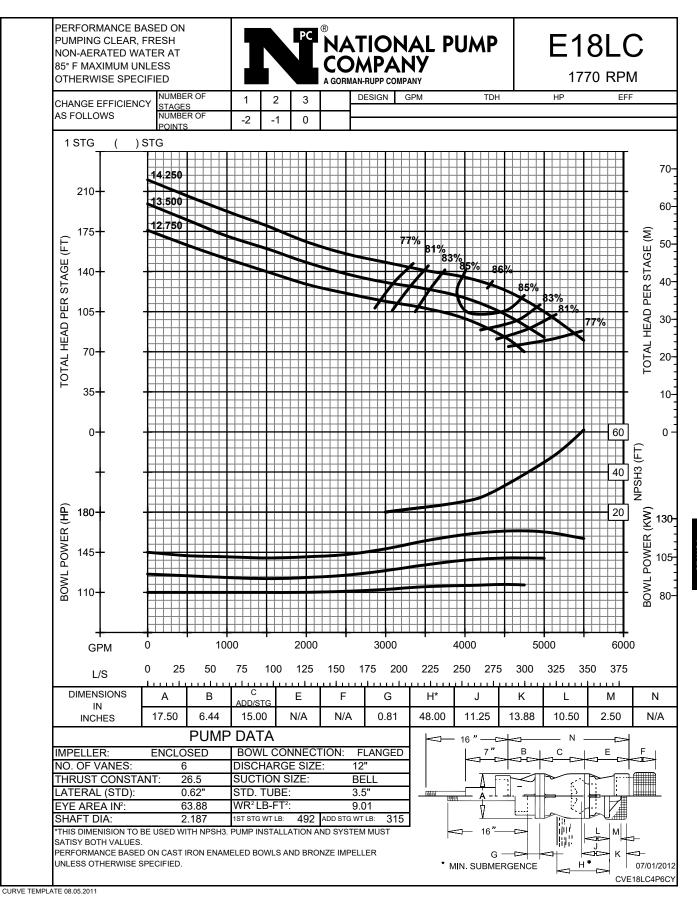


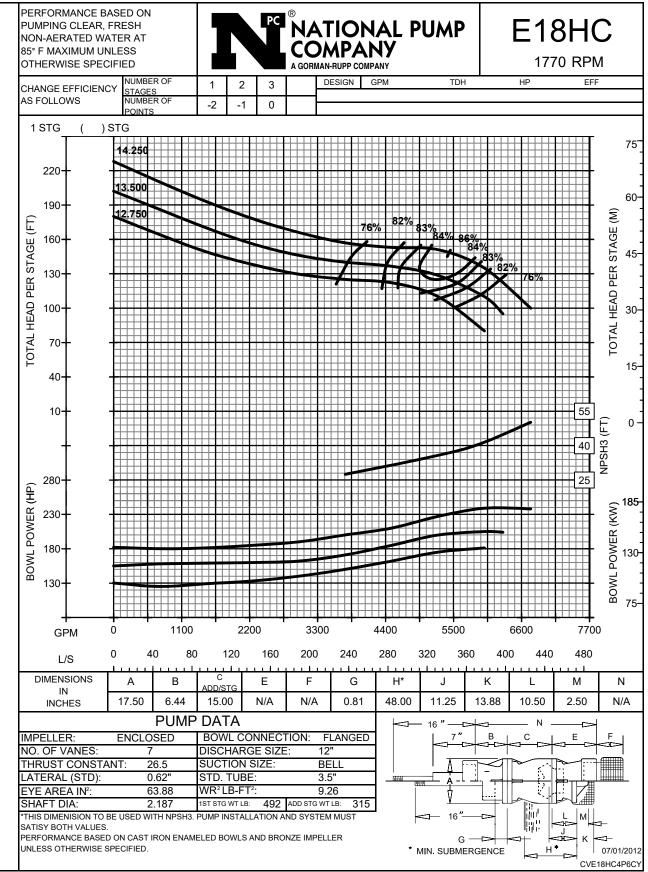
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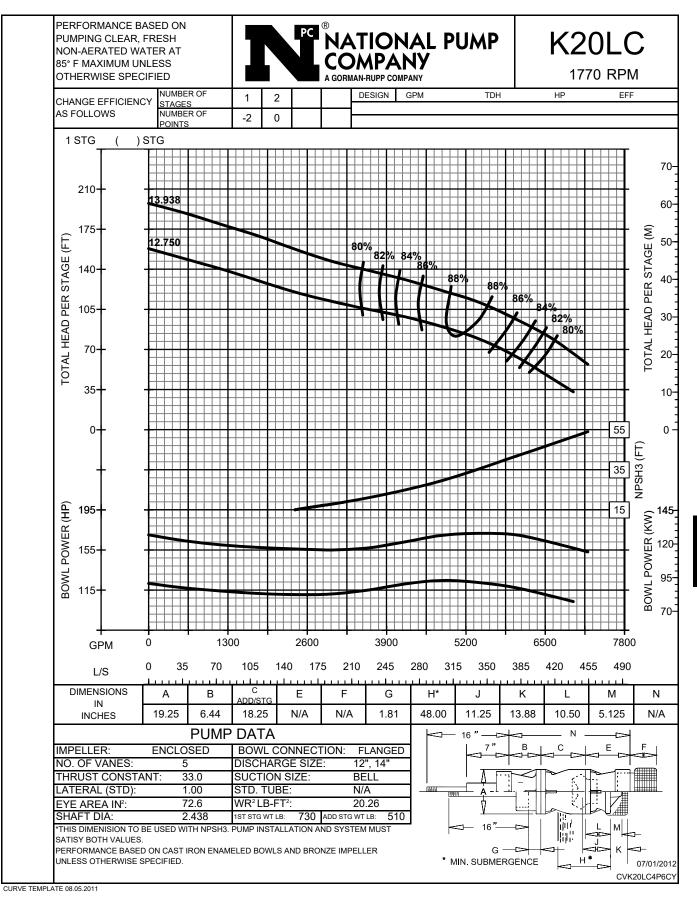




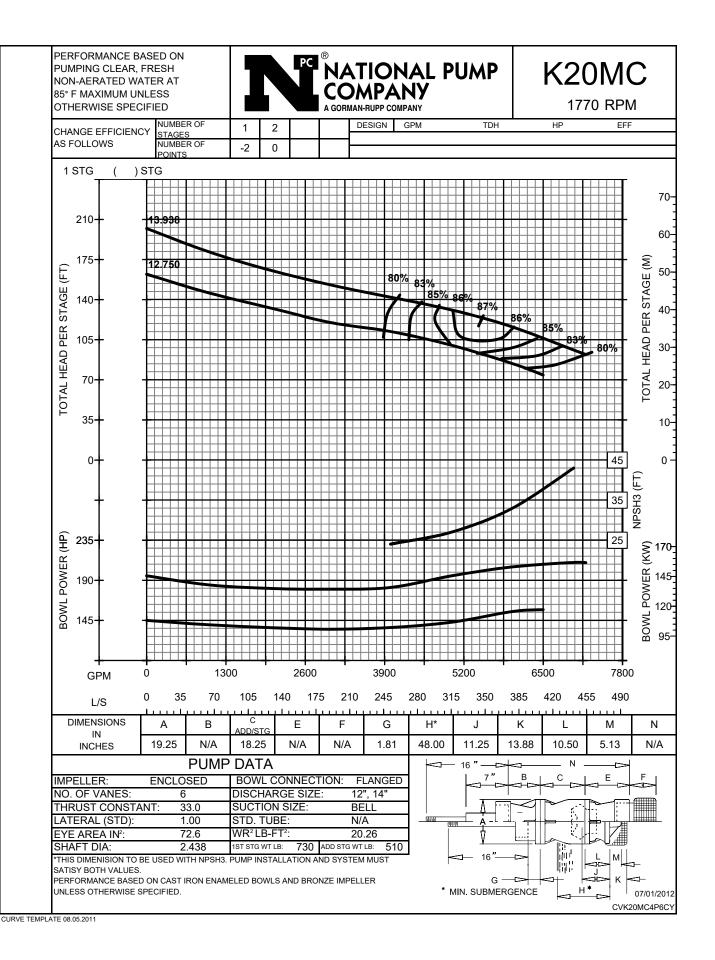


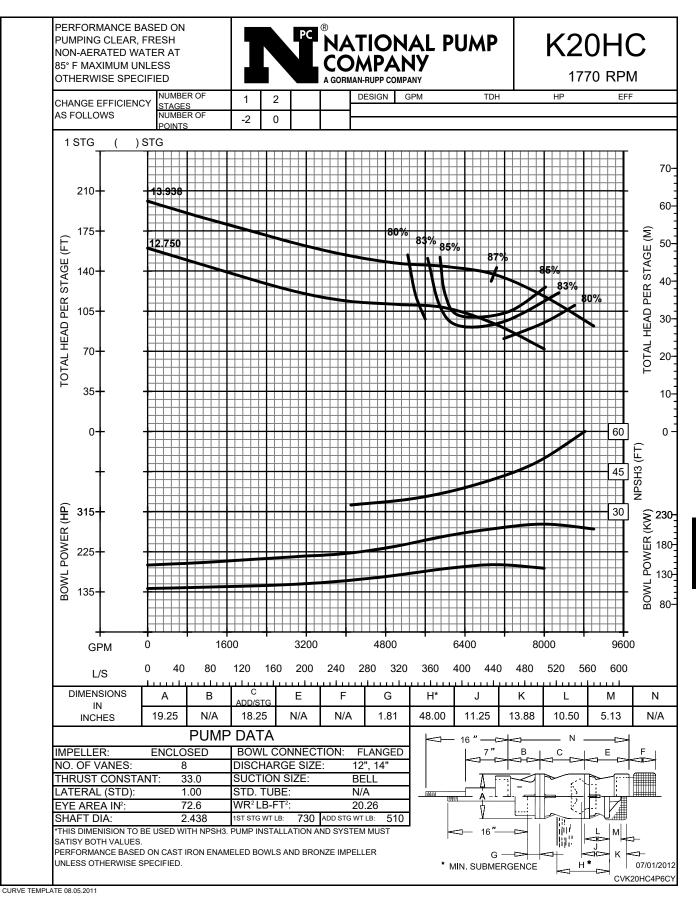


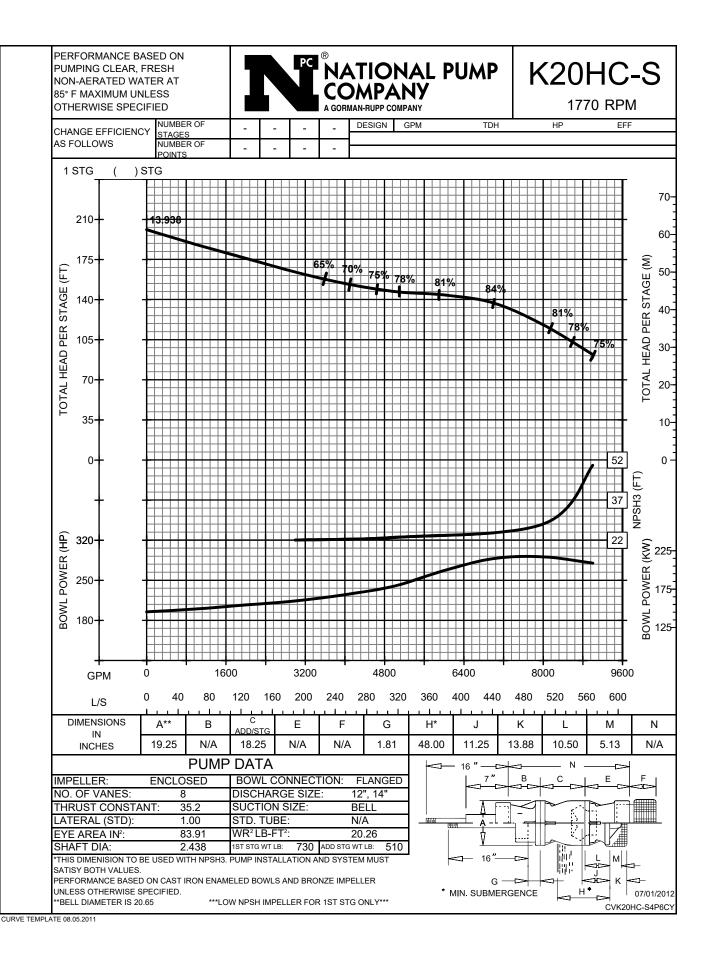


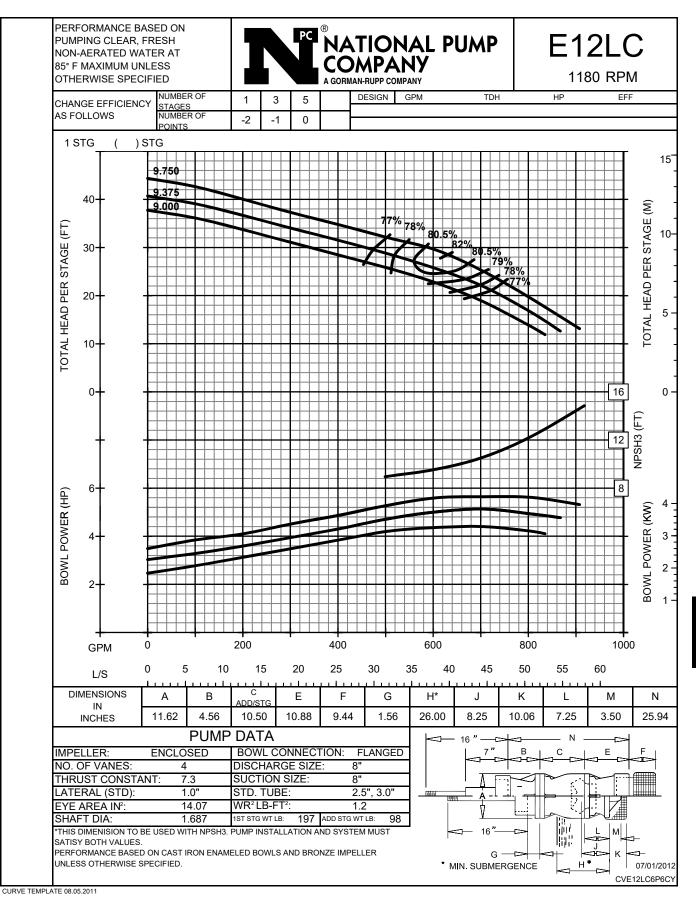


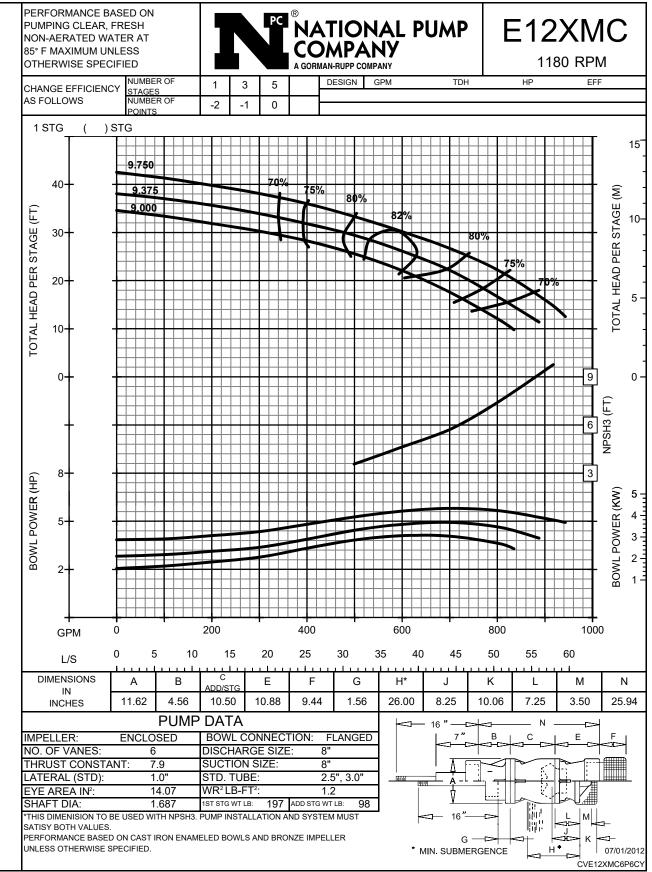


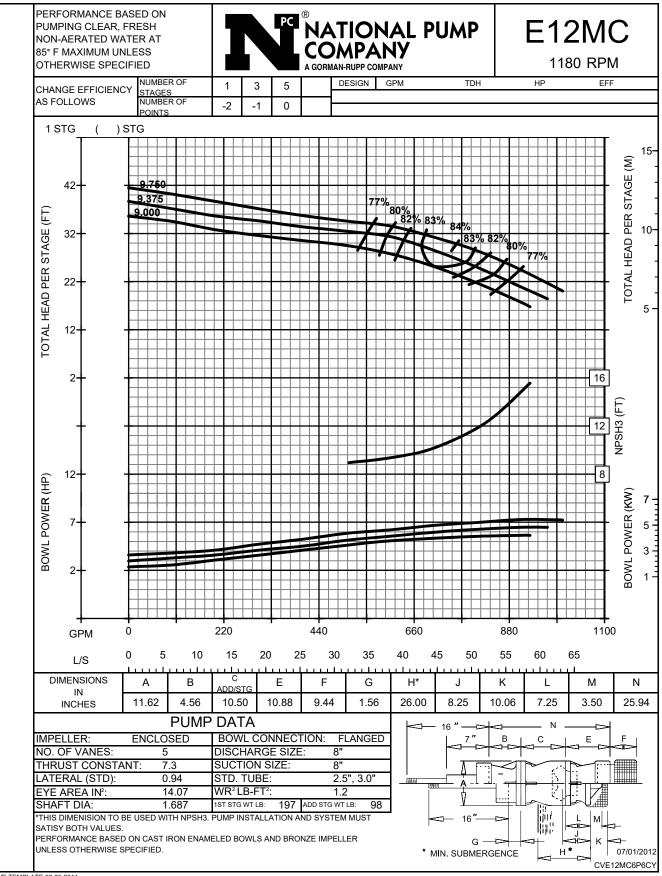




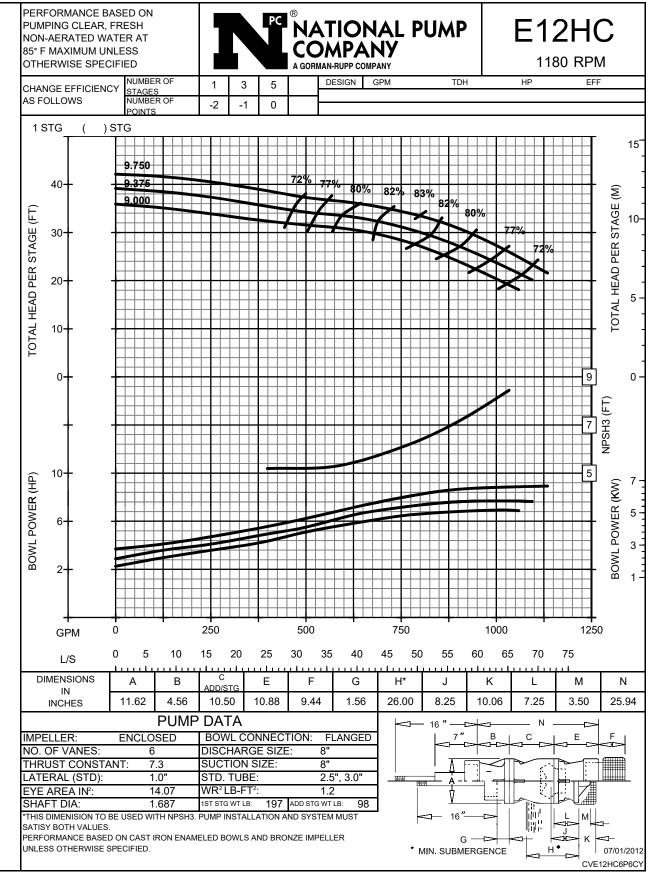


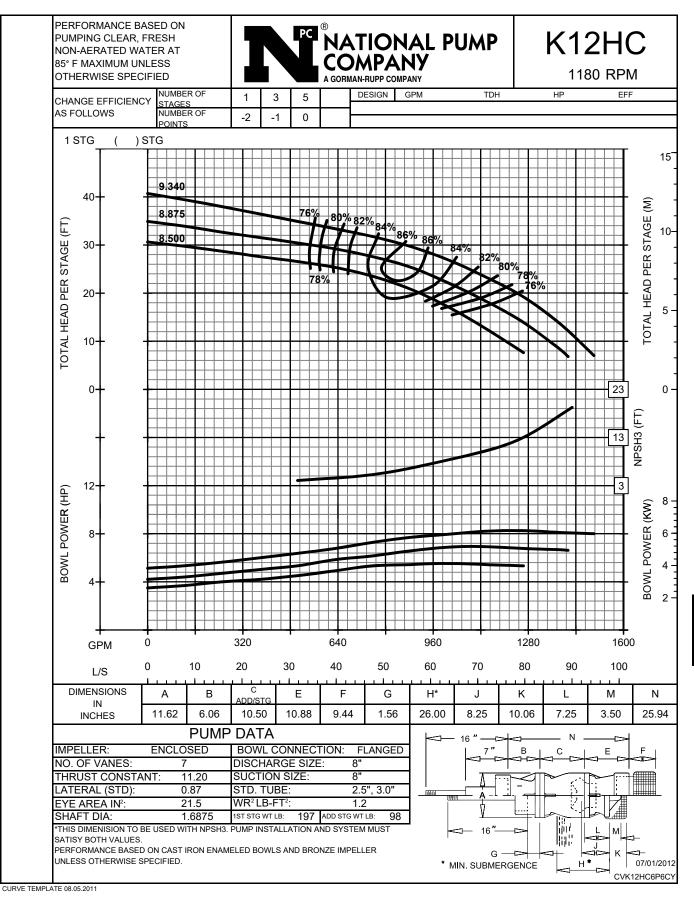


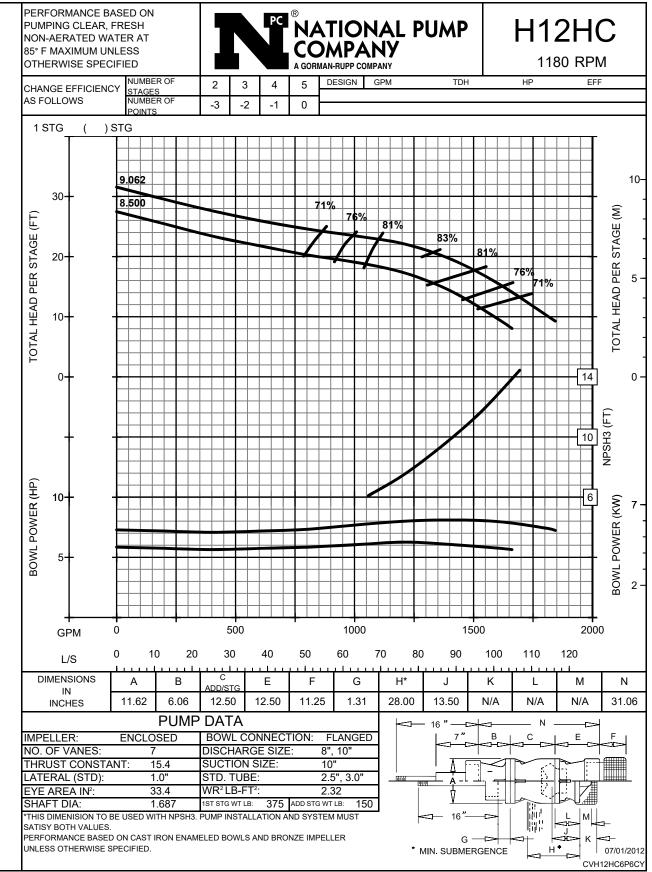


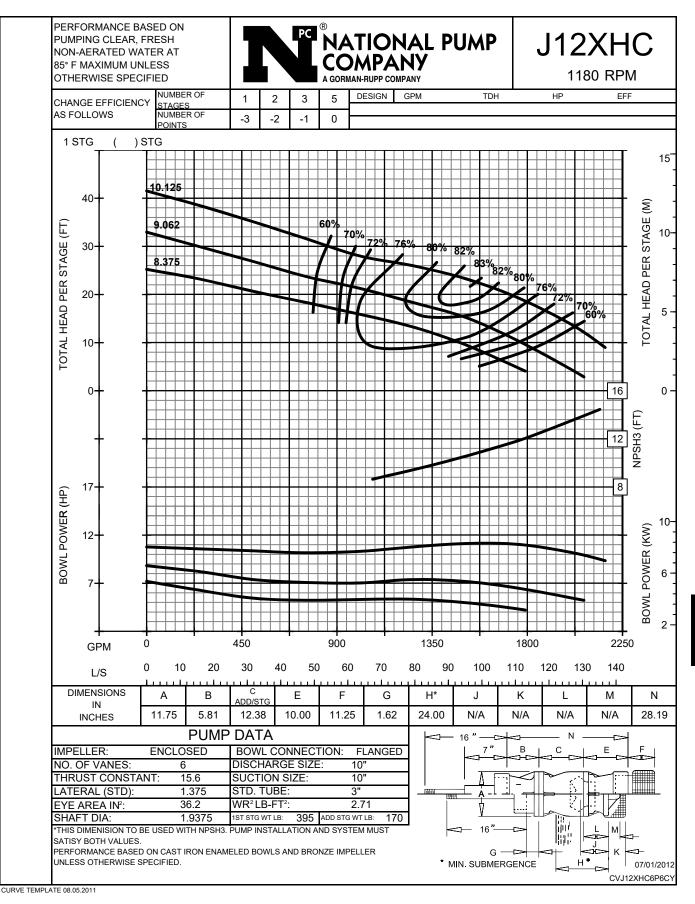


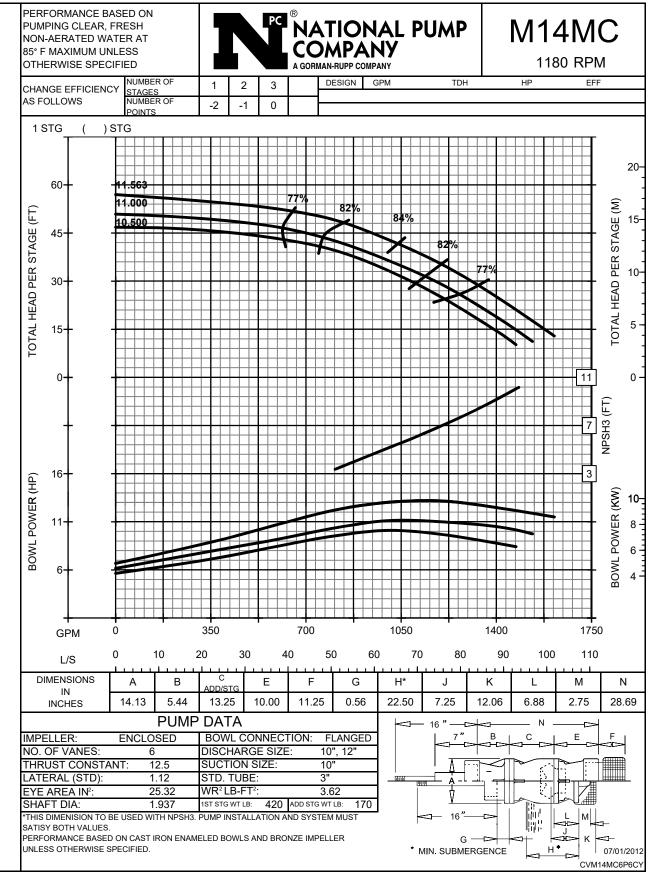
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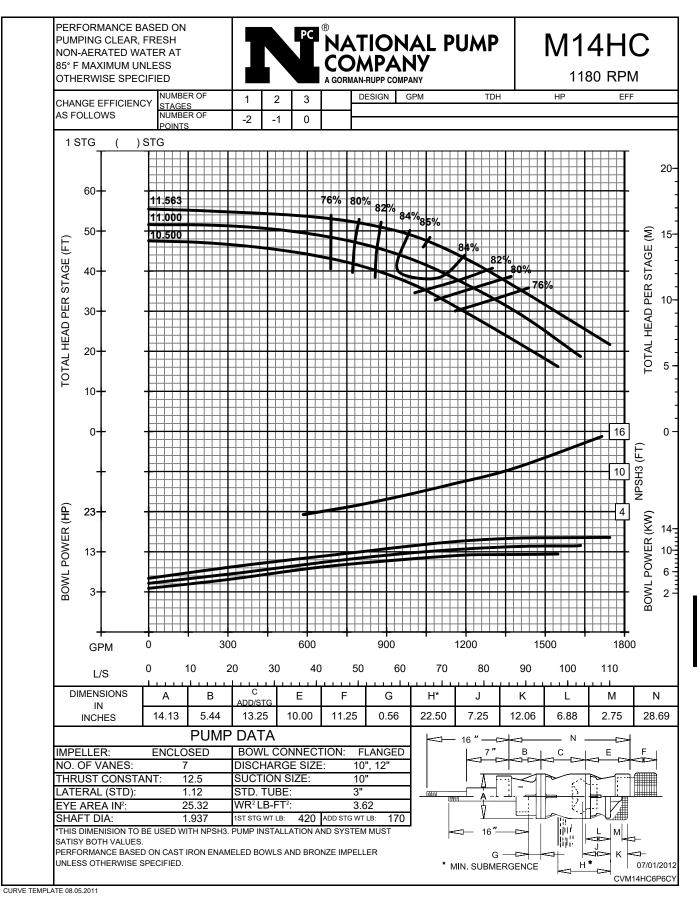


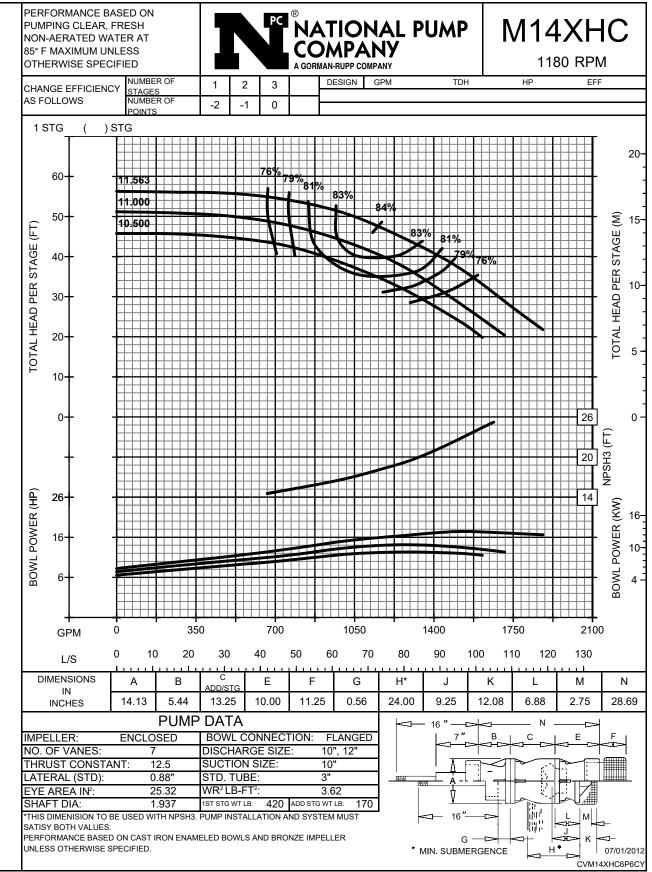


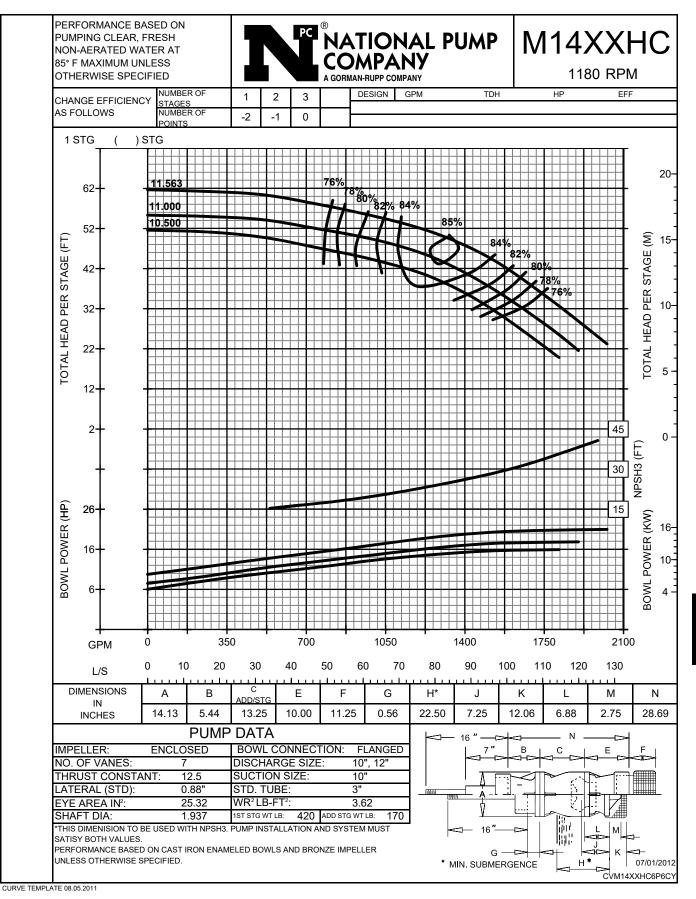


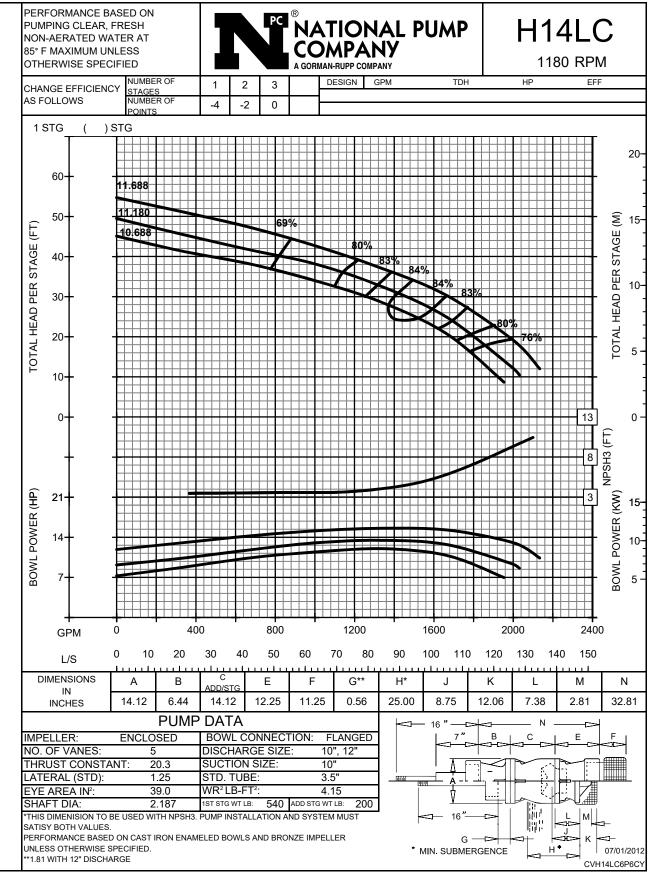


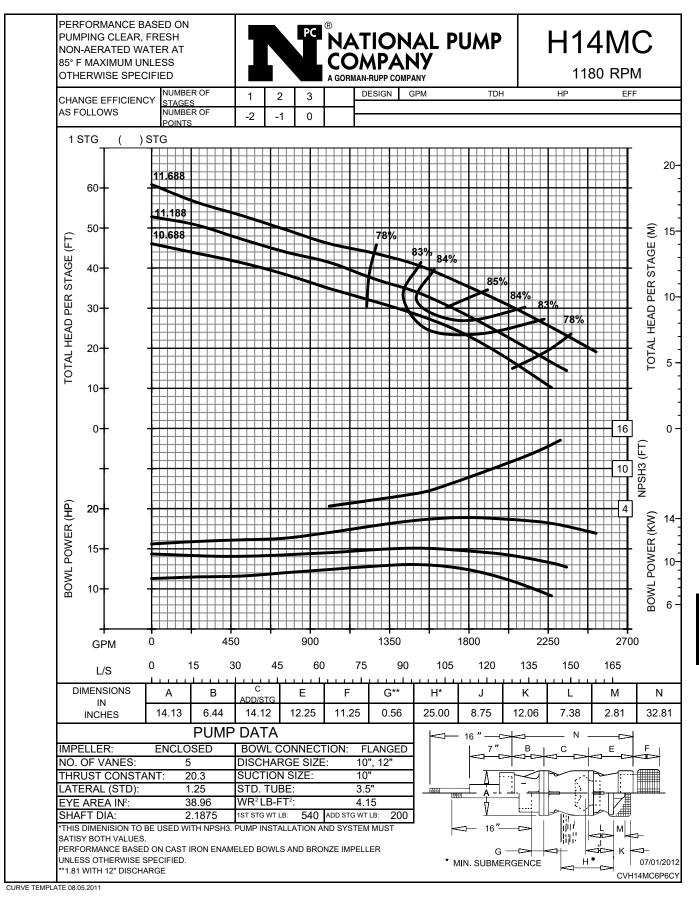


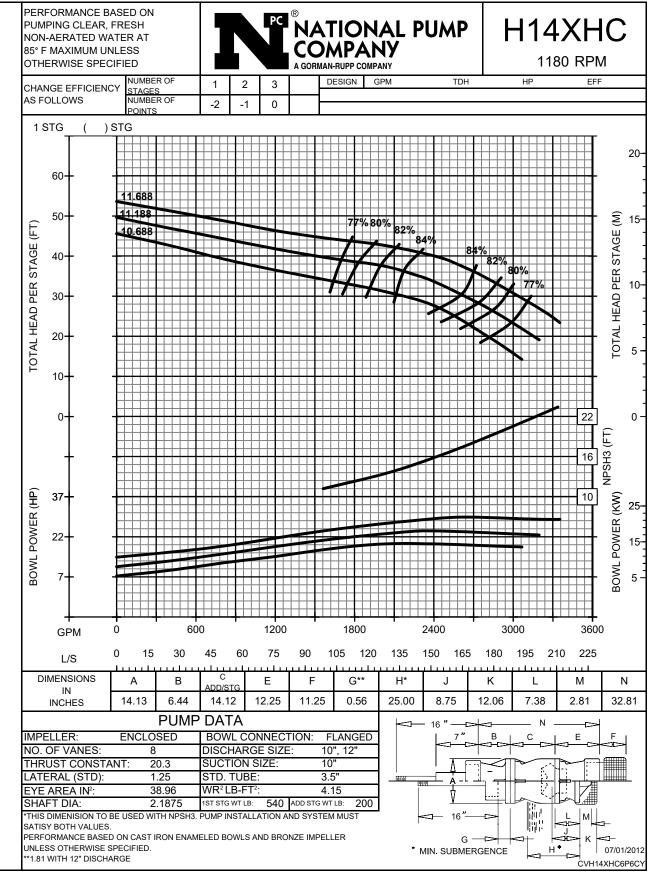


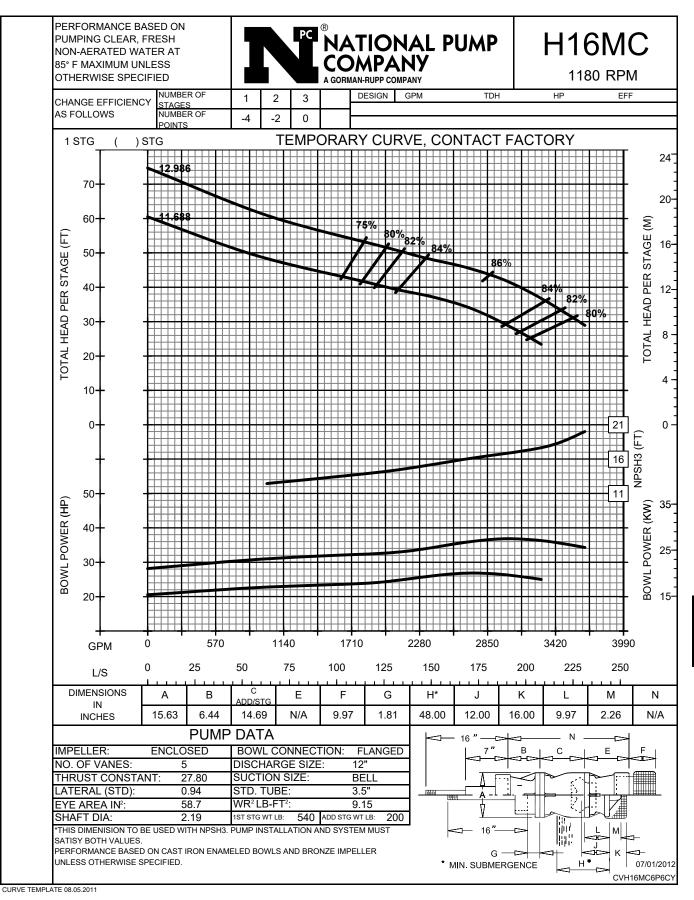


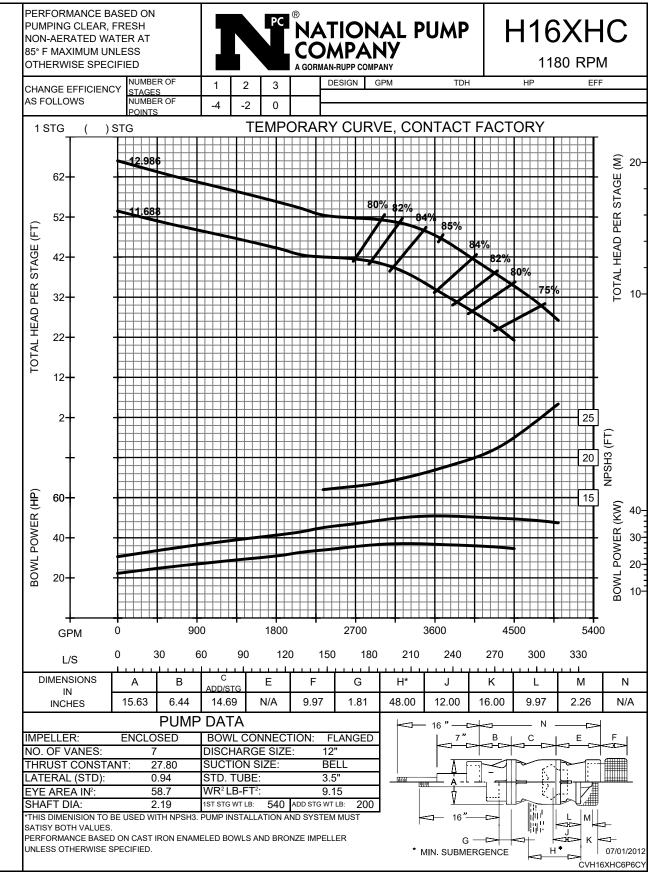


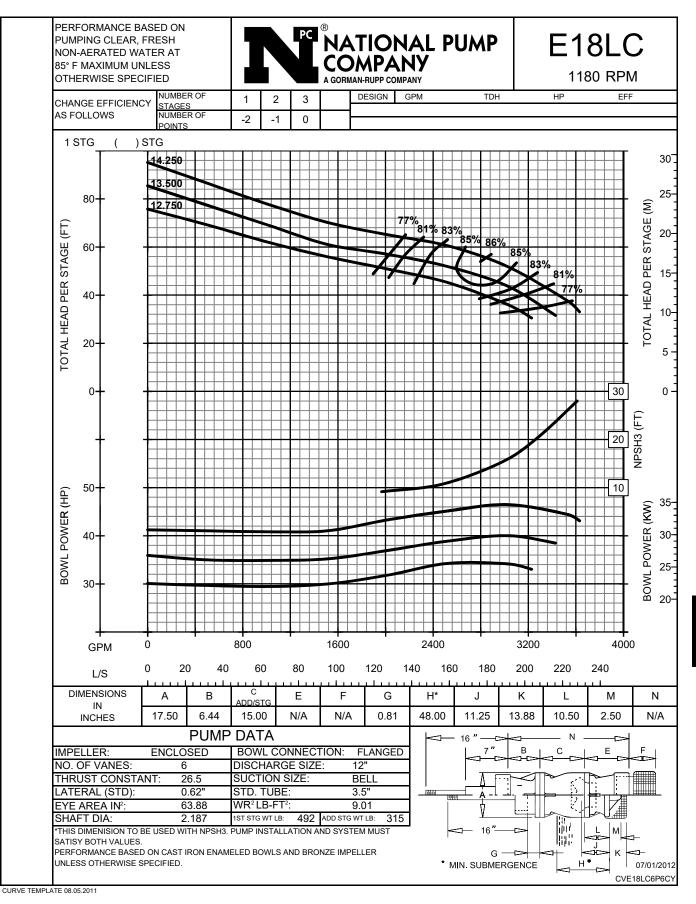


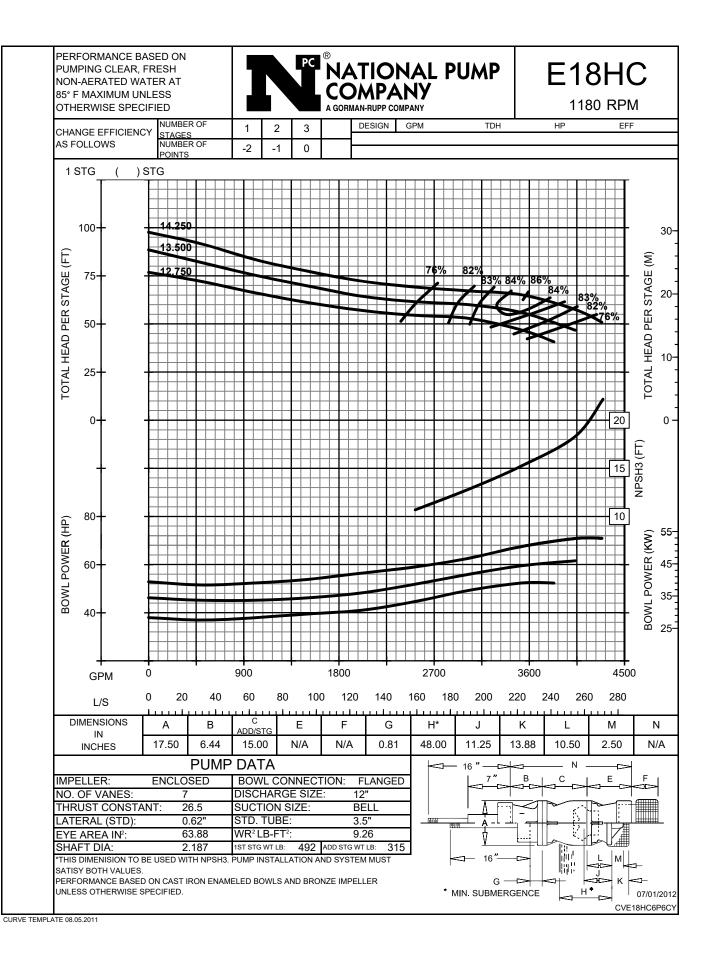


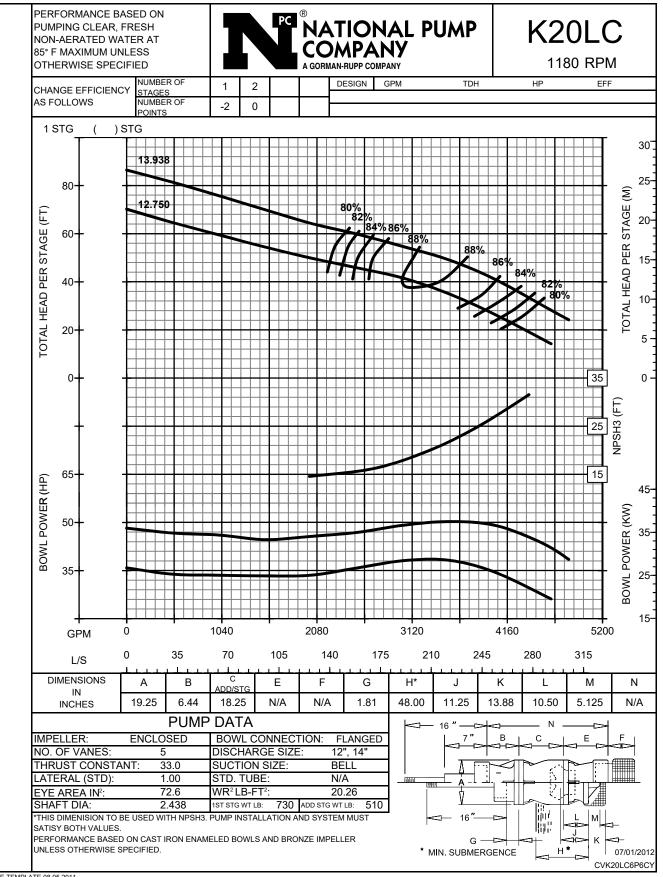




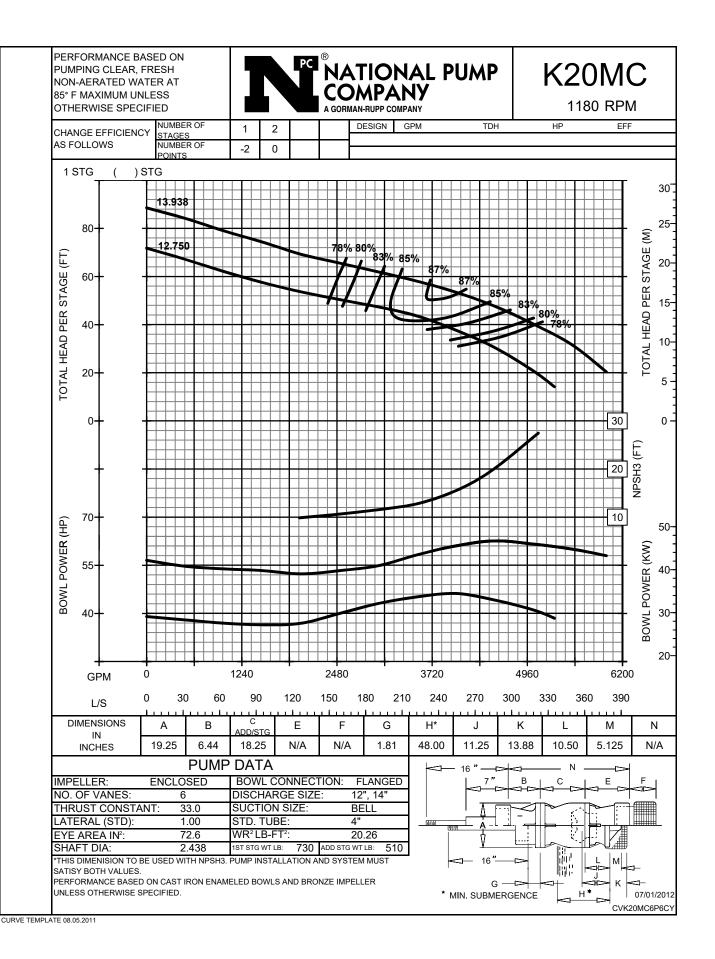


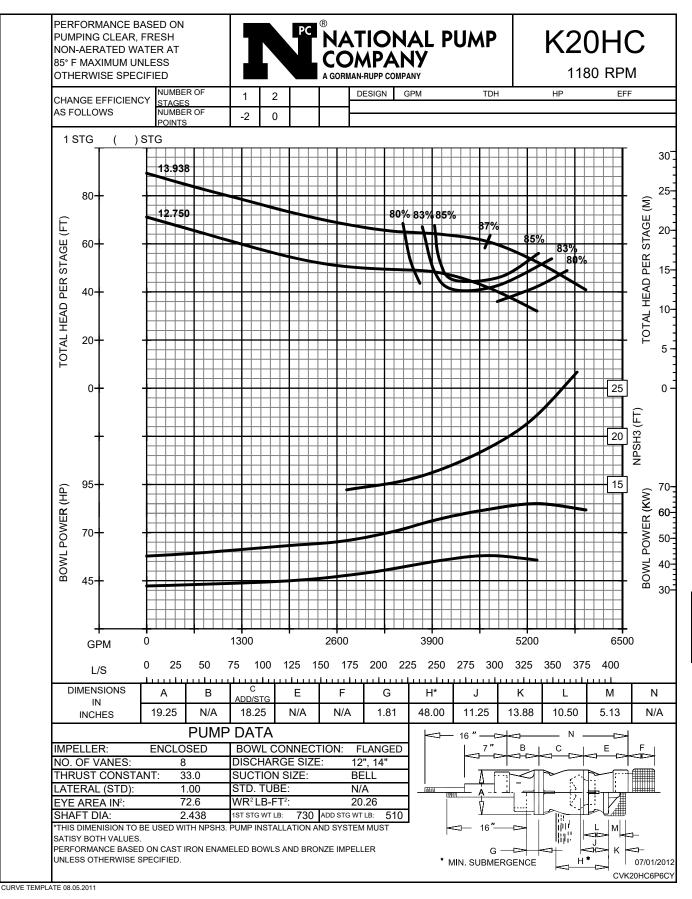


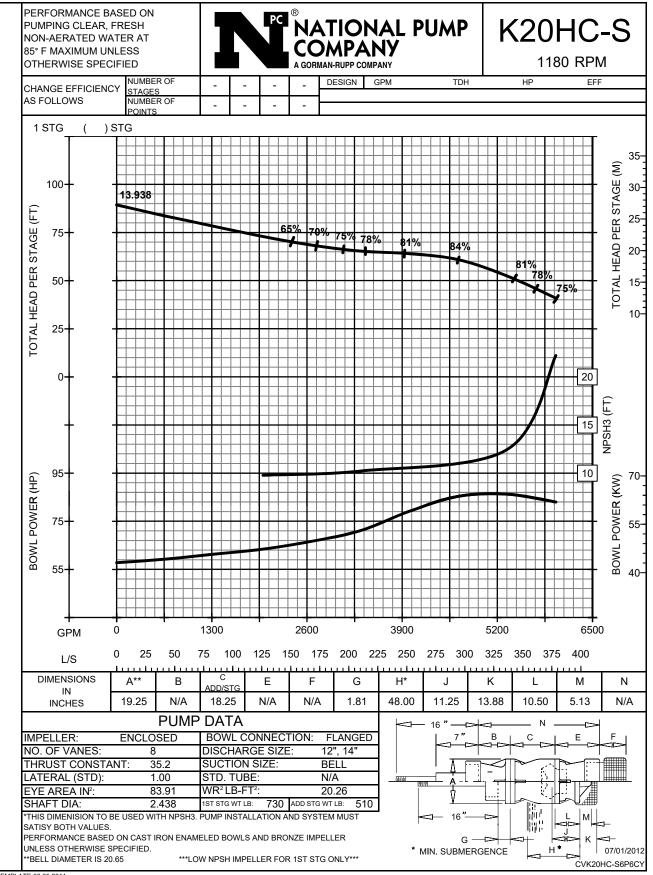


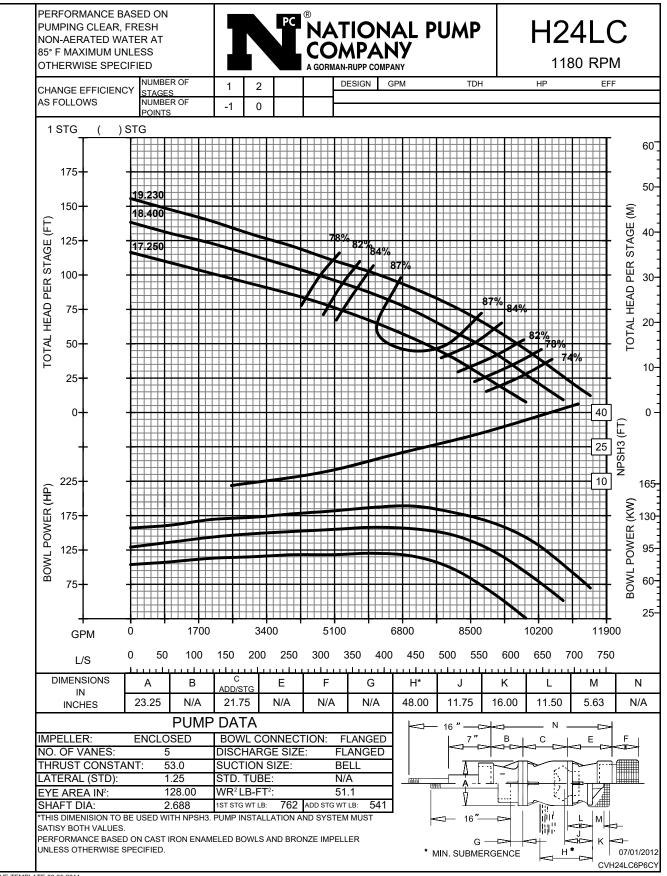


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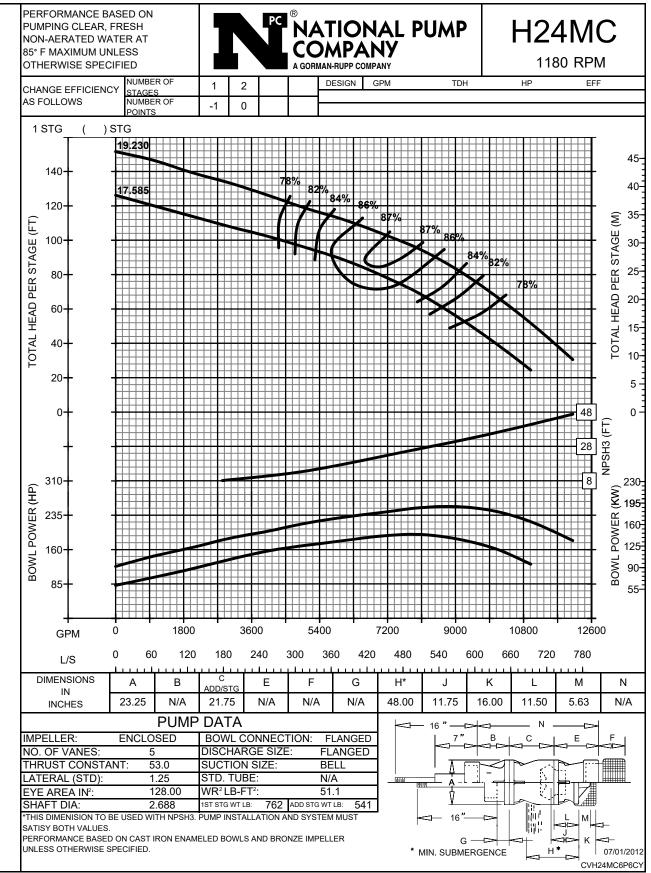


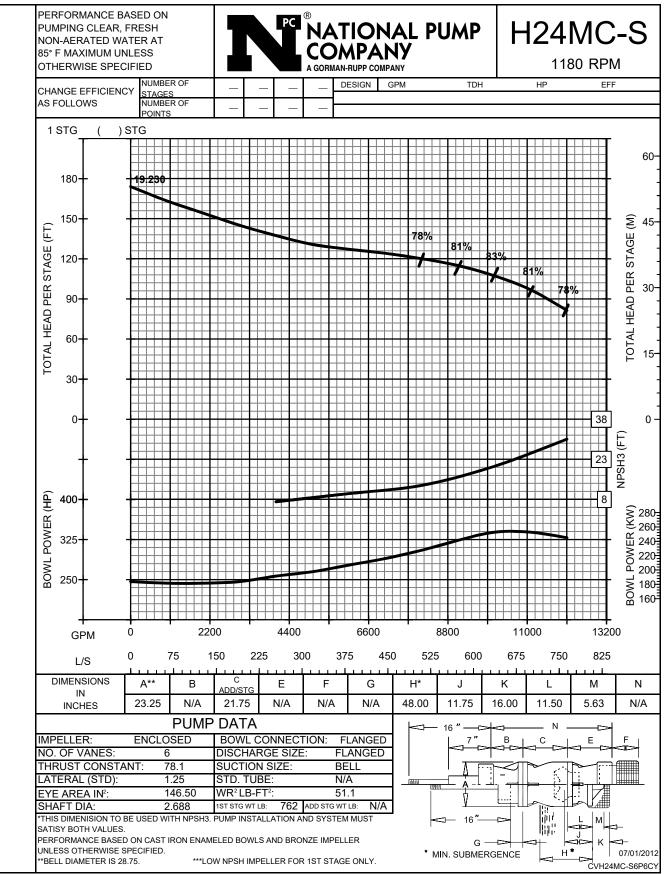




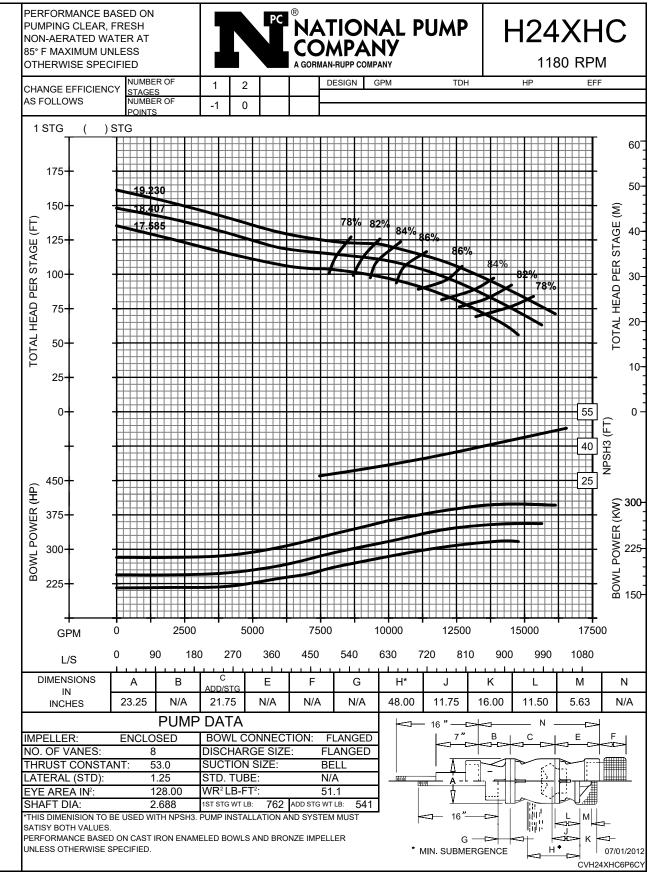


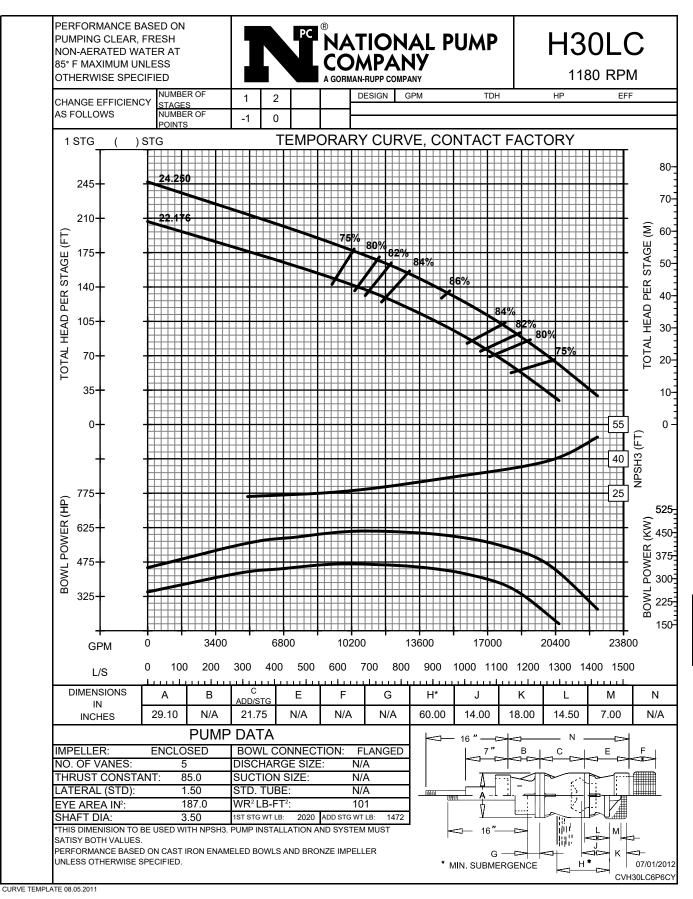
¹¹⁸⁰ CURVES

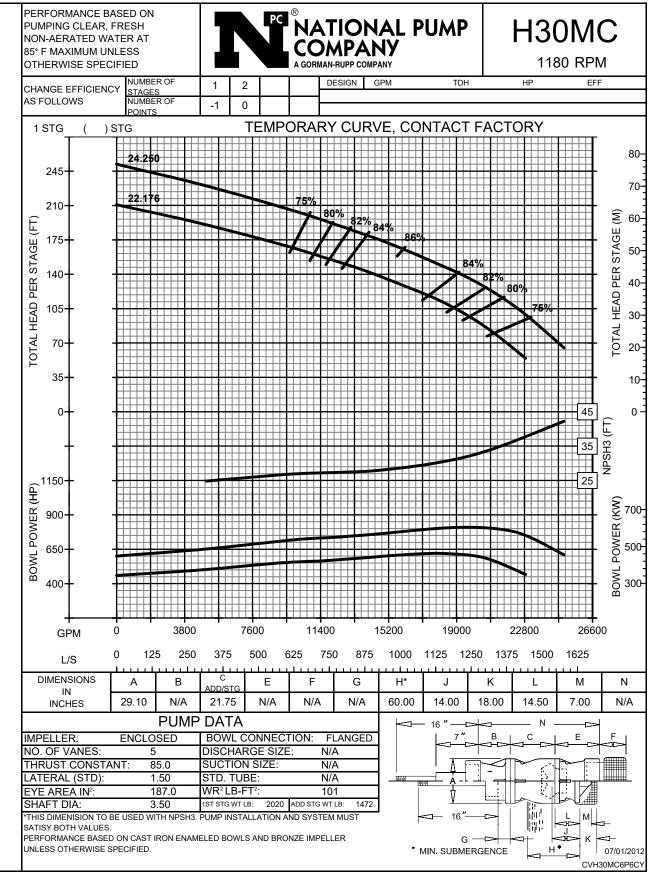




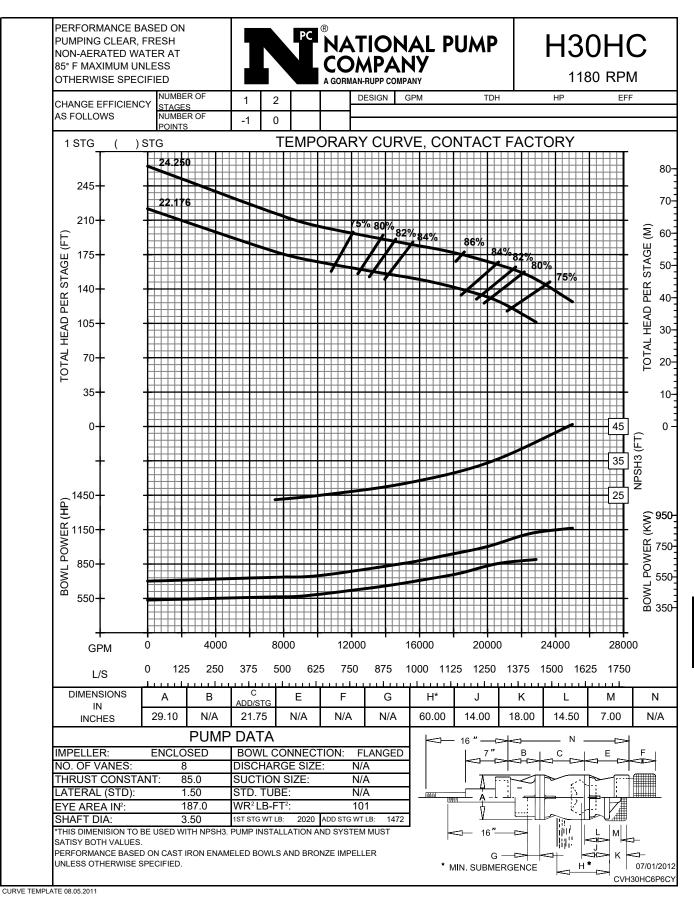
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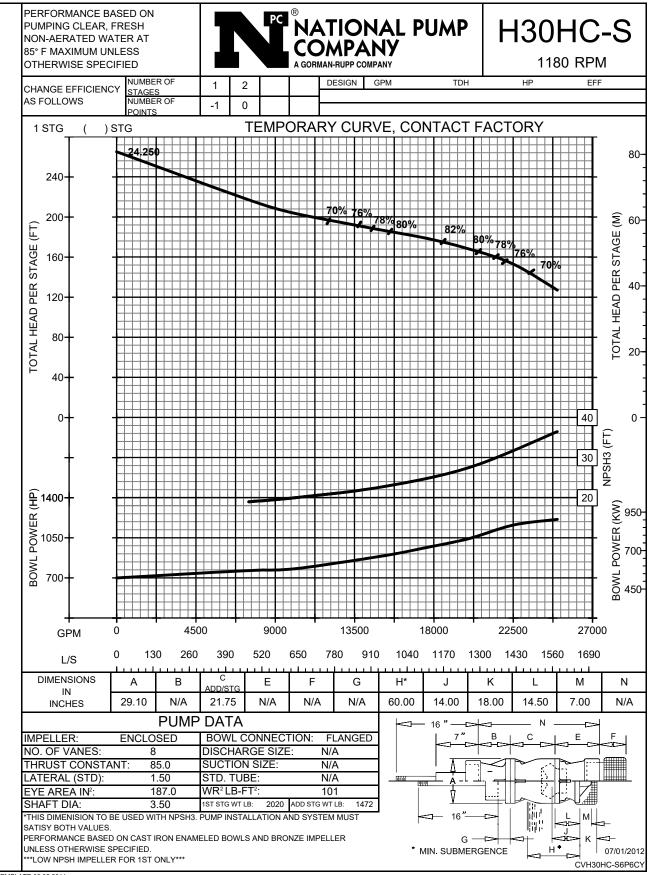


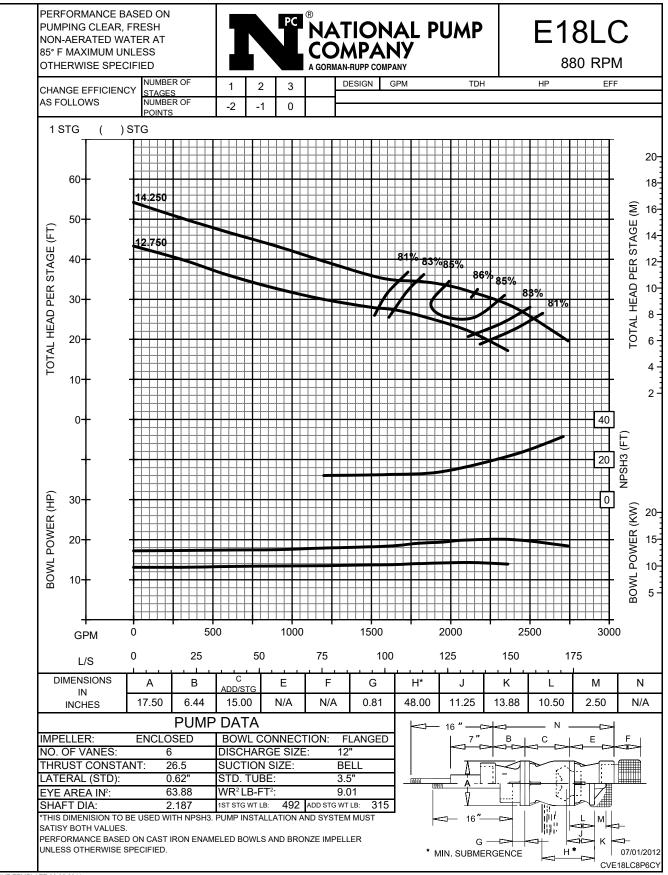




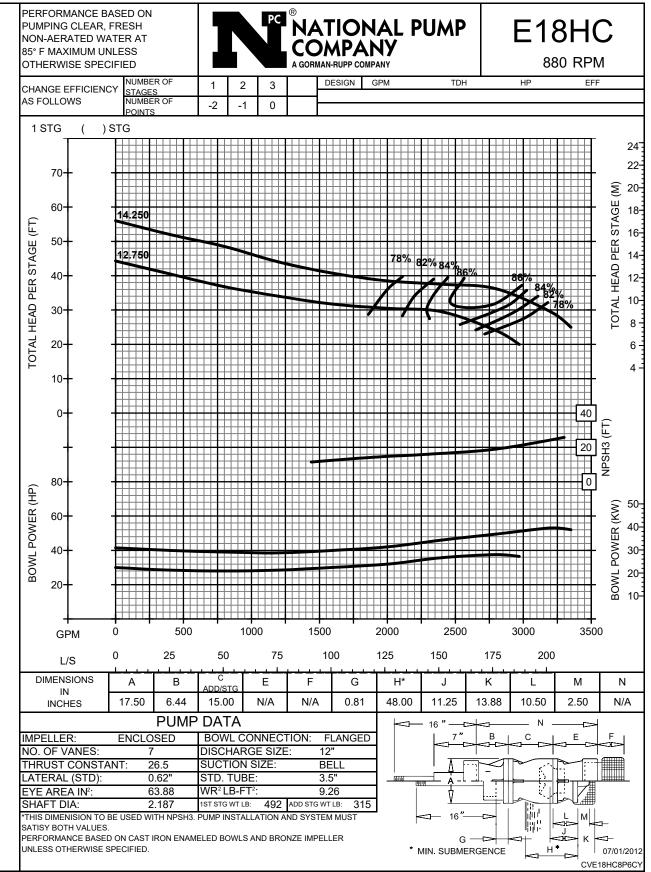


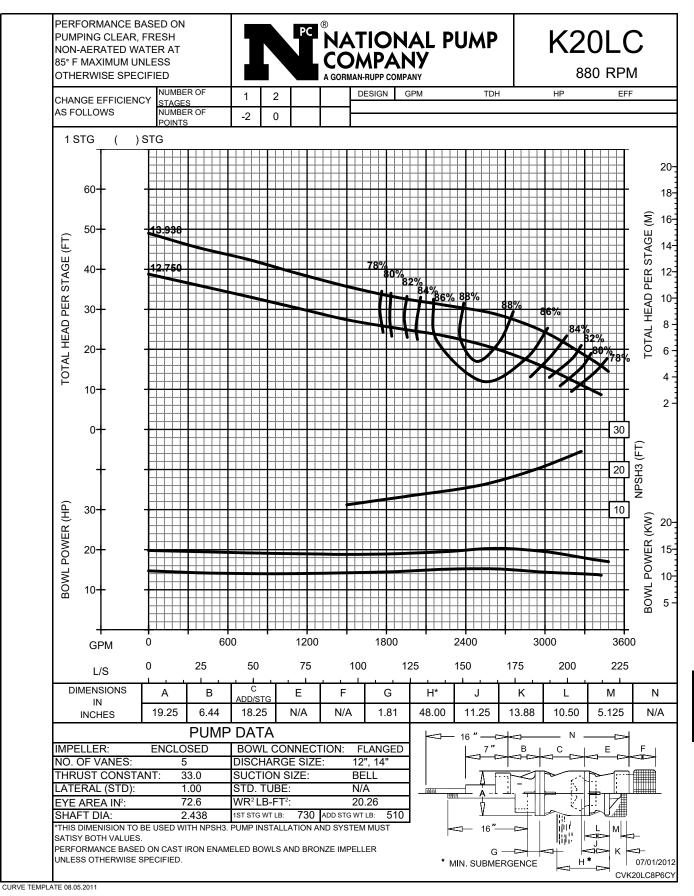


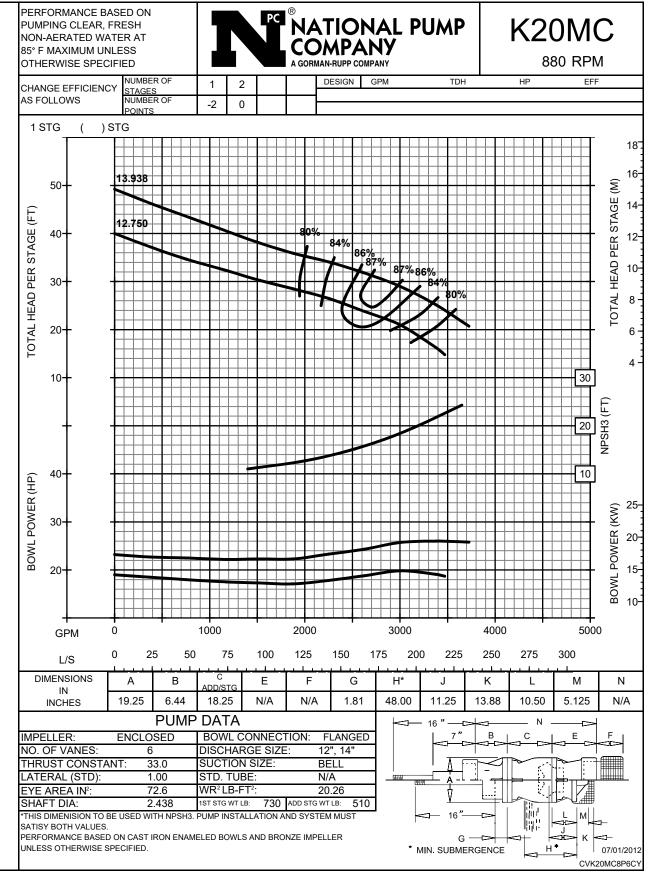


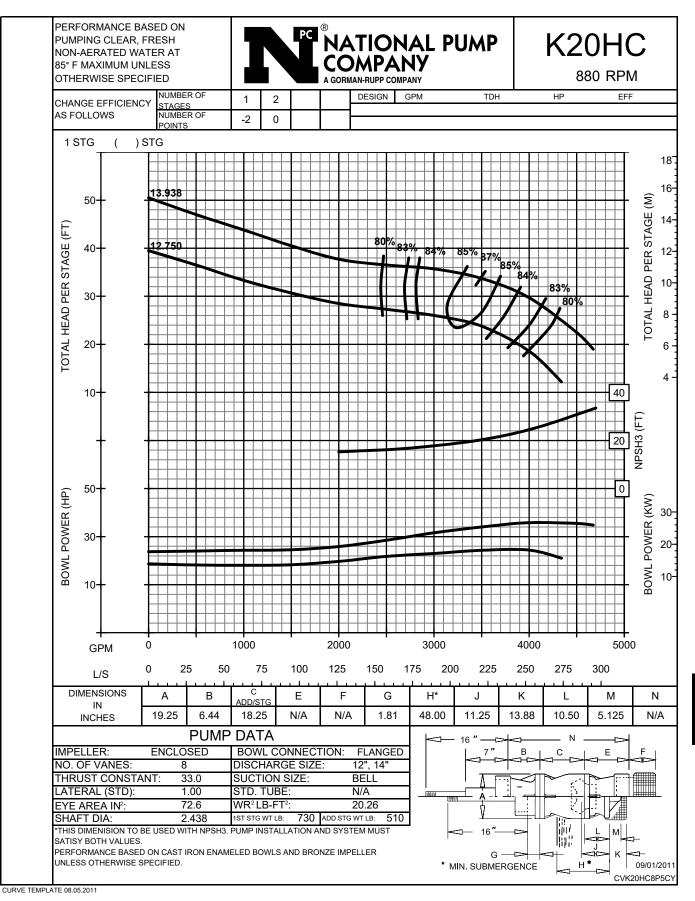


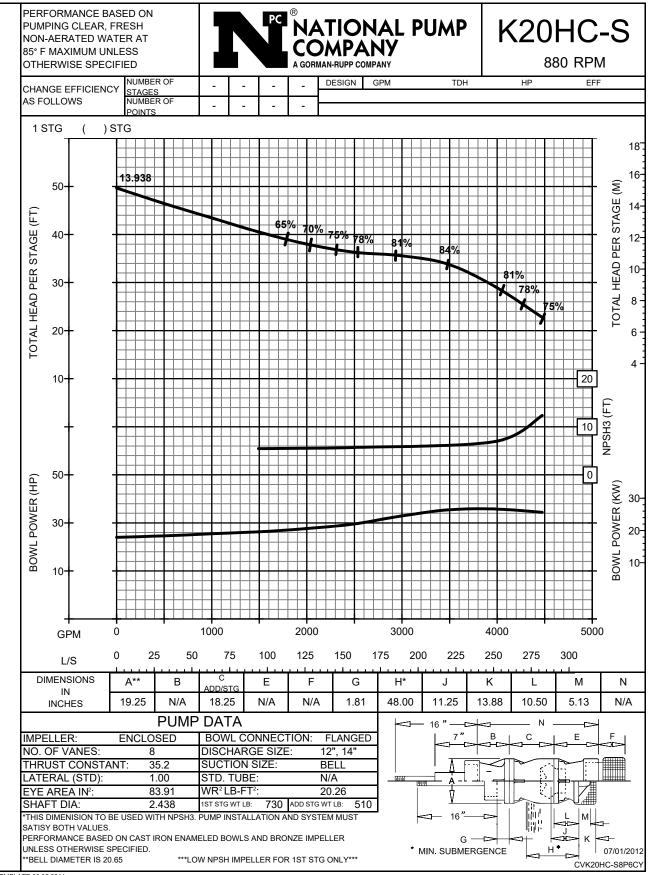


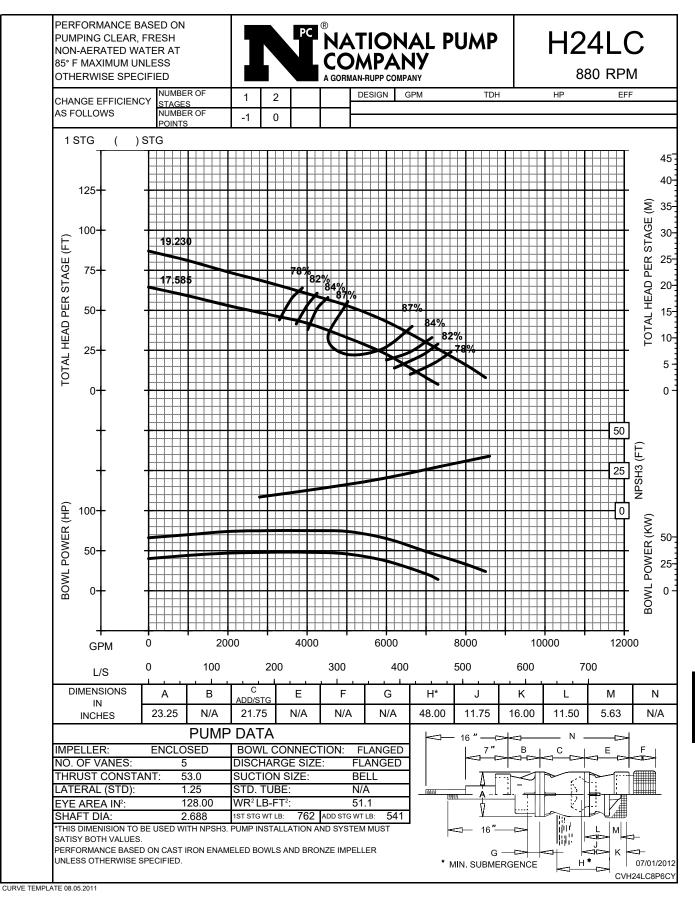




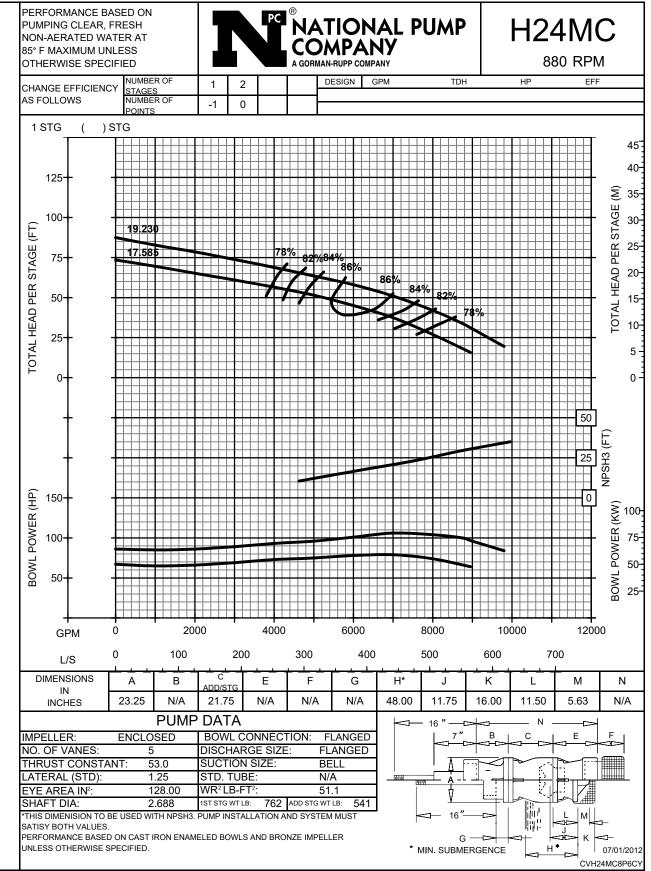


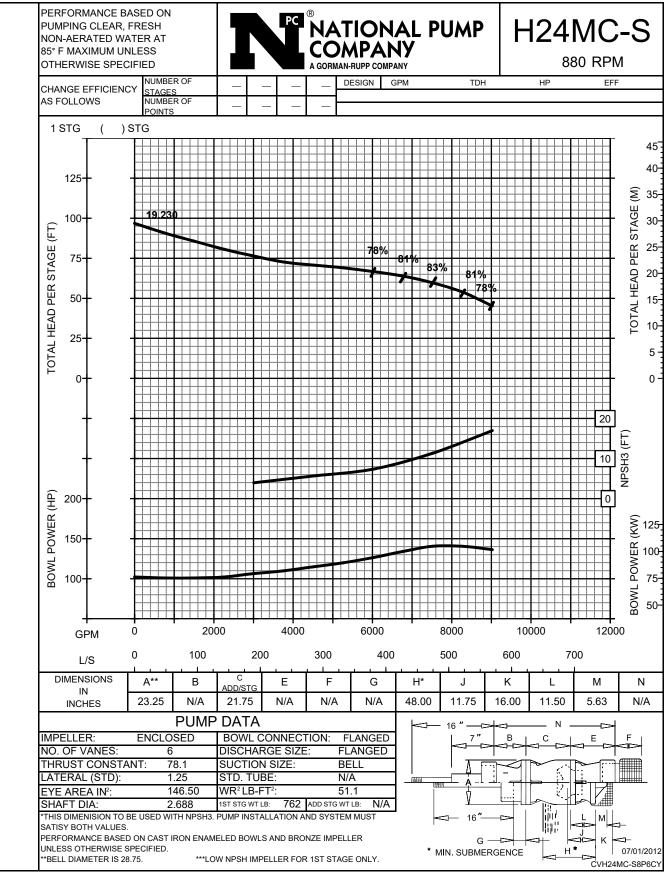




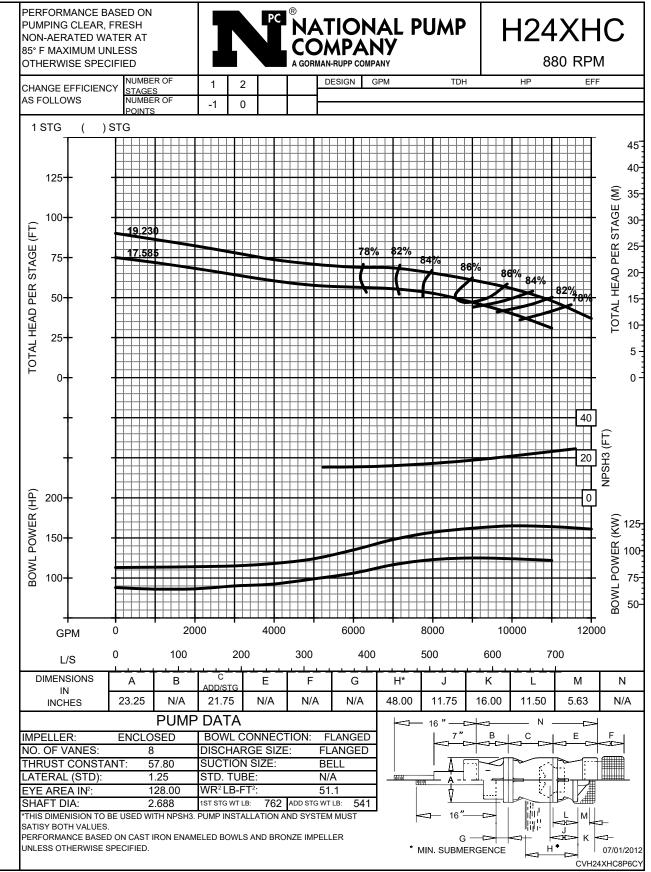


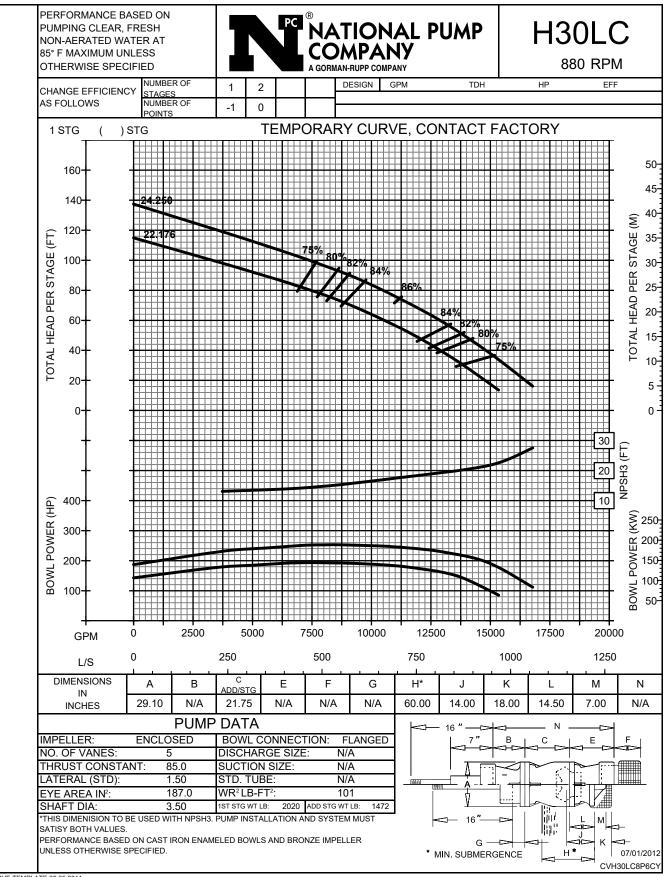


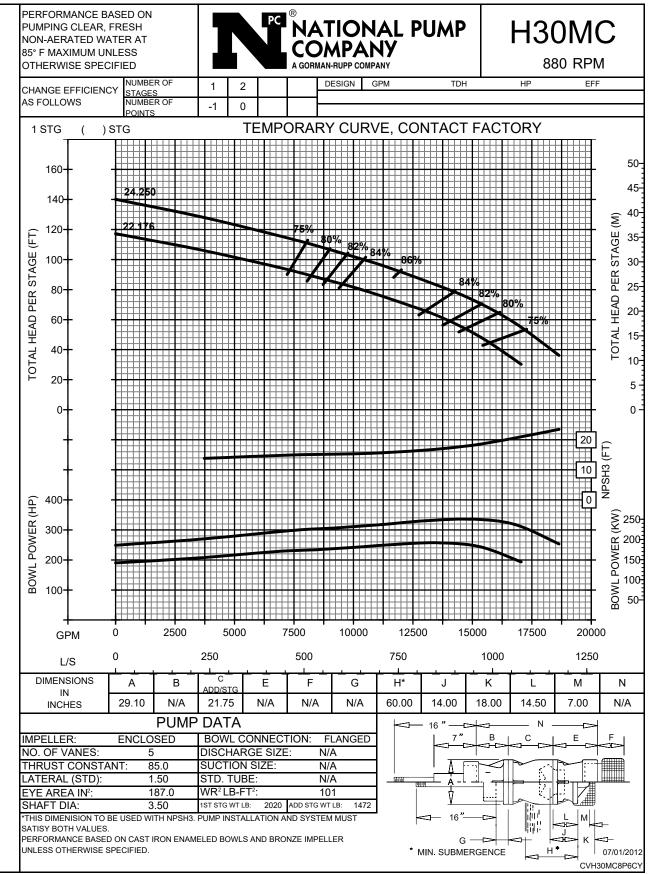


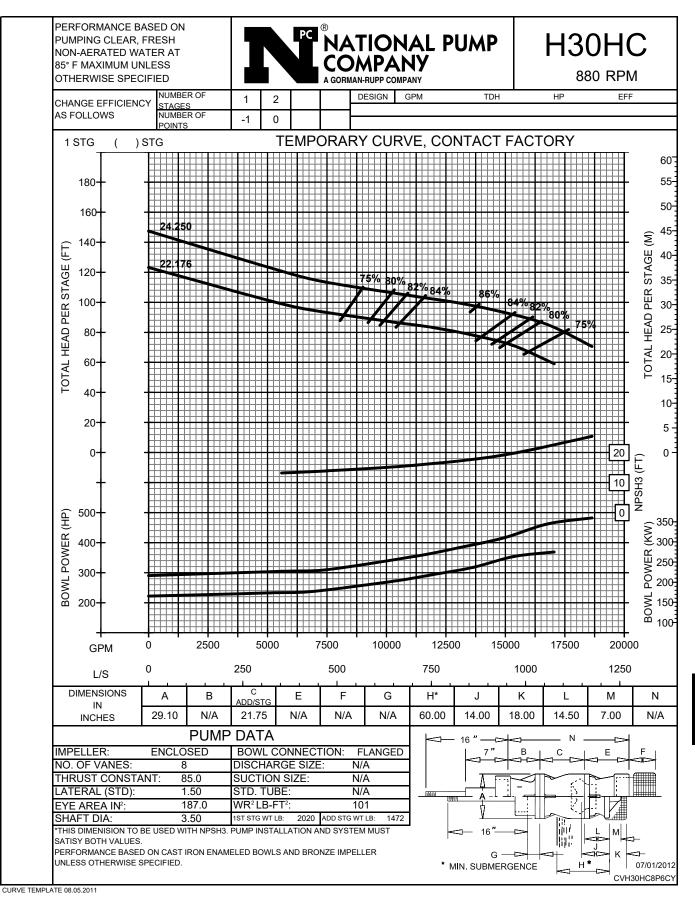


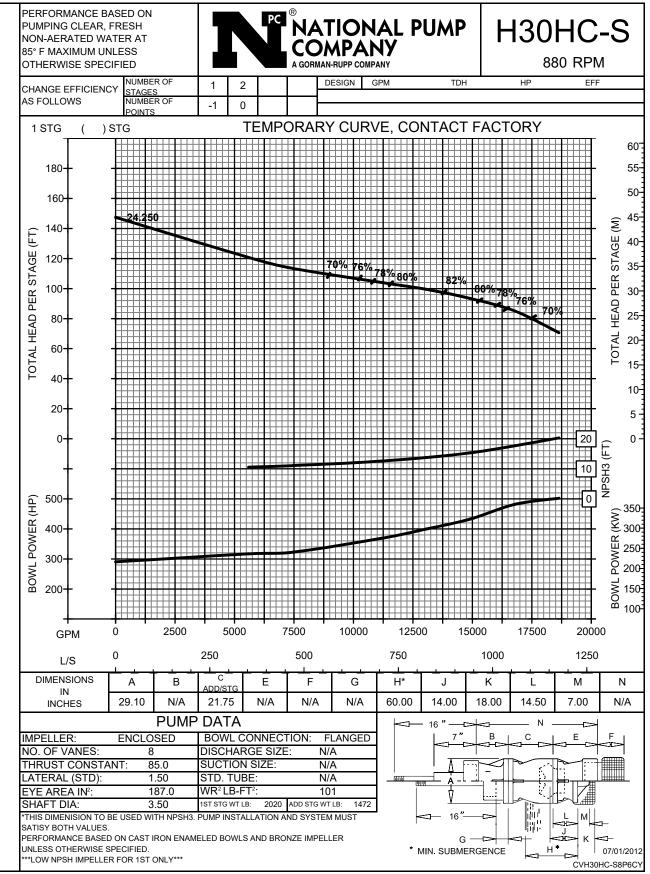
⁸⁸⁰ RVES



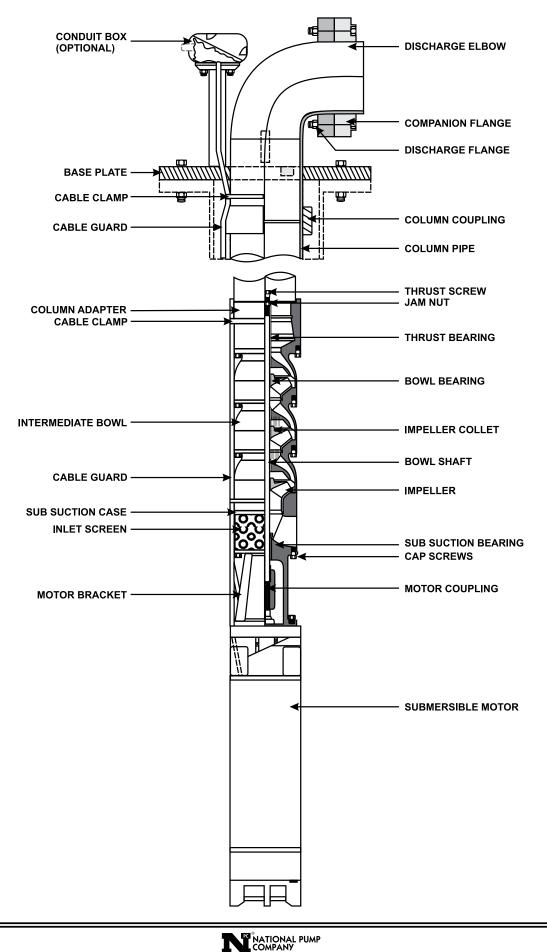








SUBMERSIBLE PUMP



SUB SAMPLE SPECIFICATIONS

GENERAL

The contractor shall furnish, completely installed, including connection to the motor starter, one (1) NATIONAL vertical turbine submersible pump, Model No. ______ and appurtenances to meet the requirements herein or as shown on the drawings or approved equal. Concrete foundations, piping beyond the pump discharge, and wiring beyond the motor starter will be provided by others. The pump is to deliver a capacity of ______ GPM against a total head (not including pump inlet, drop pipe, and discharge elbow losses) of _______ feet. The setting from the bottom of the surface plate to the top of the bowl section shall be not less than ______ feet. Pump RPM shall not exceed ______. The pump will be installed in a ______ " diameter well having a total depth of ______ feet with static water level ______ feet below surface and pumping water level ______ feet below surface when pumping design capacity. Water temperature will not exceed _______ ° F.

INFORMATION REQUIRED IN THE PROPOSAL

- 1. Data Sheet completely filled in.
- 2. Performance curve showing accepted performance at design point. Curve will show head, capacity, efficiency, and horsepower based on bowl performance and shall cover the complete operation range of the pump from zero capacity to the maximum capacity.
- 3. Drawings of the proposed equipment giving general dimensions sufficient to determine how the equipment is to be supported and if it will fit within the space available.
- 4. Any additional information such as descriptive literature, manufacturer's specifications, and other data to demonstrate compliance with these specifications.

DETAILED REQUIREMENTS

PUMP BOWLS

Intermediate bowls and discharge bowls shall be of cast iron enameled, free of foundry imperfection, and other detrimental defects. Bowls may be either flanged or threaded type.

IMPELLERS

The impellers shall be of bronze of the enclosed type and statically balanced. They shall be securely fastened to the impeller shaft with tapered split collets.

IMPELLER SHAFT

Impeller shaft shall be of 416 stainless steel. Shaft shall be of ample size for the horsepower required and shall be supported by bronze bearings on each side of each impeller.

SUCTION CASE

Suction case shall be of cast iron and be provided with a bearing to stabilize shaft, insure accurate alignment between pump shaft and motor shaft and to avoid radial thrust on motor bearing. Suction case shall also incorporate suction screen having minimum open area of 4 times the eye area of the impeller. Flange for connection of the motor must provide accurate rabbet fit to insure positive alignment of pump and motor.

DROP PIPE

Pipe size shall be such that friction loss shall not exceed 5' per 100' of drop pipe and velocity shall not be less than 3.5 ft./sec. based on rated capacity of the pump. The pipe may be furnished in random lengths of approximately 20' per length. Pipe shall be coupled with threaded sleeve type couplings. Pipe and couplings must be 3/4 NPT type threads.

SURFACE PLATE

The surface discharge assembly shall be of fabricated steel. It shall be of ample strength to support the motor, bowl assembly, drop pipe, cable, and column of water. The surface discharge plate shall incorporate suitable watertight openings to accommodate the cable, well vent connection, and water level measuring device. Cable entry shall terminate in watertight conduit box located approximately 12" above the top of the surface plate. Discharge shall be provided with a (flanged elbow) (female thread elbow).

SUB SAMPLE SPECIFICATIONS (CONT.)

CABLE

The cable shall consist of three or more separate conductors (or) a single jacketed three conductor cable assembly. Each conductor shall be insulated with synthetic rubber or plastic suitable for continuous immersion in the liquid being pumped. The cable must be protected by a suitable shield or guard when it passes the bowl section to prevent damage in installation or operation. Cable size shall be such that voltage drop will not exceed 5% under rated operating conditions.

CHECK VALVE

When total head exceeds 200', a drop pipe check valve is to be used and installed approximately 20' above bowl section. For settings over 600', two drop pipe check valves are to be used and the first valve installed approximately 100' above bowl section and the second valve installed approximately 60% of the distance between the first valve and the surface plate. Valves are to act as surge valves and permit the water in the drop pipe to drain slowly.

MOTOR

The motor shall be designed for operation, completely submerged. The motor shall not be loaded in excess of 115% of name plate rating under any operating condition.

Motor will operate on 3-phase, 60-cycle, _____-volt electric current and shall be suitable for operation with this power supply.

Motor thrust bearing rating must be ample to carry the thrust load imposed by the pump when operating under the maximum anticipated pumping head. With the motor in the "shaft up" position, direction of thrust shall be downward. Motor thrust bearing must be capable of operating with rotation in either direction, and thrust capacity, when operated in reverse rotation, shall not be less than 75% of rated thrust capacity.

An expansion chamber diaphragm shall be provided to relieve thermal expansion of internal motor fluid due to temperature variation and shall provide motor internal and external pressure balance under all conditions of temperature and pressure.

Shaft shall be Type 416 stainless steel or equivalent corrosion resistant material. Outer shell shall be of material to resist corrosion.

DATA REQUIRED

The following data must be filled in and included with the proposal:

PUMP DATA

Design Capacity	FT. T.D.H.
Design Head	%
Pump Efficiency - Field	HP
Pump Horsepower - Field	LBS.
Total Pump Downthrust	IN.
Impeller Shaft Diameter	IN.
Drop Pipe Diameter (nominal)	LBS./FT.
Drop Pipe Weight	FT.
Length of Drop Pipe	IN.
Size of Discharge (nominal)	AW/G#
Cable Size	AWG#

MOTOR DATA

Manufacturer	
Motor Rating	HP
Full Load Speed	RPM
Full Load Amperes	AMPS
Thrust Bearing Rating	LBS.
Electric Characteristics	PHASE
	CYCLE
	VOLTS
Weight of Pump and Motor	LBS.



SUBMERSIBLE PUMP APPLICATION

The submersible pump is a type of construction in which the driving motor is coupled directly to the turbine bowl assembly and is designed to be submerged in the fluid pumped. Power is supplied to the motor by means of waterproof electrical cable running from the motor to the power source.

Submersible pumps are suitable for most applications.

Since the complete unit is either enclosed or below the surface of the ground, there are several applications where the submersible pump has many advantages. Some of the more important are: (1) extremely deep wells which may present problems with shafting, especially if the well is crooked, (2) installation subjected to surface flooding which may be damaging to electric motors, (3) applications such as booster pumps that are in locations that require quiet operation, (4) installations where there is little or no floor space to install the unit, such as under a street or sidewalk, (5) horizontal pipe line booster pumps placed directly in the pipe line, and (6) agriculture installations where time consuming maintenance operations offers a great savings and security from ever rising vandalism of irrigation pumping units.

OPERATION

These pumps may be operated and controlled in the same manner as any other type of turbine pump in similar applications. No special consideration peculiar to the submersible is generally necessary, with the exception of the motor starting equipment. This is due to the fact that the motor, being installed in the pumped fluid, may not be subjected to the same ambient temperature as the overload relays in the starter. Overload protection is a must for submersibles. Unless the correct overload protection is used on all three motor legs, the motor warranty is void. Why? For two reasons: (1) for running protection and (2) if the motor stalls, power must be cut within 10 seconds or you may damage the motor windings. In three-phase submersible motors, use ambient compensated, quick trip heaters.

CONSIDERATIONS

Submersible pumps can be built in sizes up to several hundred horsepower for most applications where this type of construction is practical. However, there are some uses that do not lend themselves too well to this pump. Among these are high fluid temperatures, unusually corrosive applications, or a large amount of abrasives.

SUB MOTOR COOLING

It is important that the motor have an adequate flow of water passing it to maintain proper operating temperature and avoid premature failure. If the well casing is "oversize" or the motor is installed in a "pit" or "pond", or the inflow from the well is above the pump, a closed top shroud of the proper size must be installed above the pump suction inlet to force the liquid to pass the motor before entering the pump. Since recommendations vary between motor manufacturers and temperature of liquid and installation configurations, it is important that the application be reviewed with the particular motor manufacturer involved for proper sizing of the motor shroud.

CROOKED WELLS

A submersible pump will give better service in a crooked well than a lineshaft type pump since the length of the rotating parts are much shorter. Where the well is known to be crooked, a gage of the same length and diameter of the motor and bowl section assembly should be lowered into the well on at least 40 feet of pipe of the size to be installed on the unit. If the gage with pipe can be lowered to the depth at which the pump will be set, a submersible pump can be installed. Never install a pump in a well known to be crooked without gaging the well.

BOOSTERS

The submersible pump has been designed for pipe line booster service for industry, municipal water systems, petroleum products pipe lines, and other booster applications. The unique design enables the submersible, ordinarily operated in a vertical setting, to be suspended horizontally within the pipe line, and furnish a powerful booster to the liquid being carried by the line. The many advantages of noiseless operation, close-coupled motor and bowl assembly, totally enclosed motor operating completely immersed in the line liquid, economy of operation, and completely new ease of access to the pump and motor all combine to make this new concept of submersible booster operation the engineered answer to pipe line booster problems. Costly pump houses to maintain and keep clean, additional property to purchase, motor damage from heat, dust and moisture, possibility of vandalism, stuffing boxes and packing gland maintenance are completely eliminated. The submersible installation makes all of these obsolete.

The horizontal application enables the submersible unit to be fitted into a special section of the pipe line. This section is flanged at each end and becomes an integral part of the line. Within this section, the motor is centered and firmly held by special spiders. The line liquid is drawn past the motor and into the bowl assembly which passes it along at a greatly increased pressure. The submersible power cable is clamped firmly to the bowl assembly and leads to a terminal box mounted on the outside of the special section and from there to a control box.

The vertical application enables the submersible unit to be fitted into a canister used as a booster in many places.



SUBMERSIBLE PUMP SELECTION

A submersible pump consists of the following basic elements:

- < Bowl Assembly
- < Motor
- < Cable
- < Drop Pipe
- < Surface Plate (with)(without) discharge elbow

DATA REQUIRED FOR SELECTION

- < Capacity in GPM
- < Static and Pumping Levels in Well
- < Setting Required (drop pipe)
- < Well I.D. Diameter
- < Electric Characteristics

DETERMINATION OF TOTAL HEAD

Total head = H + P + F where:

- H = Distance from surface to water level when pumping
- P = Pressure (head) at pump discharge
- F = Drop pipe friction (+) check valve(s) loss

BOWL ASSEMBLY SELECTION

Select impeller in exactly the same manner as for lineshaft type pump. Note comments under WELL SIZE.

DROP PIPE SELECTION

Size of drop pipe is selected based on the capacity to be pumped. Submersible pumps frequently require smaller drop pipe than do line shaft pumps since the full area of the pipe is used to deliver water to the surface.

Minimum velocity in drop pipe should not be less than 3.5Ft./Sec.

We recommend drop pipe size be selected to limit the maximum friction loss to 5' per 100' of pipe. Selection table is based upon this limitation. Smaller size drop pipe may be used when bowl assembly and motor are adequate for operation with the increased head and horsepower.

Pipe furnished by others must be standard pipe with 3/4 taper NPT threading throughout and to connect to the bowl assembly and surface plate.

CHECK VALVES

Where total head exceeds 200', the use of a drop pipe check valve is recommended. Check valve should be located approximately 20' above the bowl assembly. For settings over 600', the use of two check valves are recommended, with the first valve approximately 100' above bowl unit and the second located approximately 60% of the distance between the first valve and the surface plate.



SUBMERSIBLE PUMP SELECTION (CONT.)

CABLE SELECTION

Select a drop cable designed for use in water. The insulation on the conductors should be RW, RUW, TW, or their equivalent. DO NOT compromise on drop cable quality. Paying a little more will save you money in the long run. Cable selection chart is based on horsepower, voltage, and length of cable required. Cable sizes and lengths are maximum allowable. Higher operating efficiency will be obtained by using the next larger cable size when lengths approach listed limits. All size and cable lengths shown are for copper wire only.

NOTE: Use of smaller cable than recommended will void warranty.

Select cable length equal to length of setting plus an additional 10' or more to connect to starter at the surface, plus 1 additional foot for each 50' of length in the well to compensate for unavoidable slack in the installation.

SURFACE PLATE

Surface place consists of flat steel plate with connection for drop pipe, hole for entrance of cable, vent hole, hole for air line or water level gauge. Surface plate is supplied (with)(without) elbow. If elbow is furnished, it can be flanged or female thread. Surface plate is selected to match drop pipe size.

MOTOR SELECTION

Motor selection is based upon horsepower required, pump RPM, thrust load, well diameter, and power supply. Also, see comments under WELL SIZE and WATER TEMPERATURE.

STARTING EQUIPMENT

Selecting the proper overload protection is one of the most important factors in obtaining a successful submersible installation. Submersible motor starters should provide the following:

- < Positive motor protection against single phasing.
- < Positive motor protection against sustained overload in excess of 115% of motor rating.
- < Motor protection if rotor is stalled.
- < Tripping timers independent of ambient temperature; (Ambient Compensated Quick Trip Heaters).

NOTE: Failure to provide quick trip overload heaters will void warranty.

Also, note that under certain conditions of maximum load on the motor (use of the 1.15 service factor), a starter one size larger may be required.

LIGHTNING PROTECTION

Lightning and power surge damage are major causes of submersible motor failures, so a three-phase lightning arrestor is a must. The arrestor is mounted in the pump panel and grounded to both ground terminals onto pump panel and well head. If you use plastic pipe, the ground wire should also be connected to a stud on the motor to obtain good grounding and maximum benefit from the arrestor.

WARNING: Failure to ground this unit may result in serious electrical shock. A faulty motor or wiring can be a serious electrical shock hazard if it is accessible to human contact. To avoid this danger, connect the motor frame to the power supply grounding terminal with copper conductor no smaller than the circuit conductors. In all installations, connect above ground metal plumbing to the power supply ground per National Article 250-80 to prevent shock hazard.



SELECTION PROCEDURE EXAMPLE

REQUIREMENTS:

Capacity	850 GPM
Head	140 Feet
Pumping Level	200 Feet
Well Diameter	.12" Inside Diameter
Power Supply	3 Ph. / 60 Hertz / 480 Volts
Pumping Liquid	Fresh Water

1. <u>DETERMINE TOTAL DYNAMIC HEAD:</u> (TDH) = pumping level + head required + drop pipe friction loss + check valve(s) friction

TDH =	 a. Pumping level b. Head required c . 8" drop pipe friction head for 850 GPM is 2.2 feet per 100 feet. 200 feet of new 8" drop pipe has a total loss of 2.2 x 2.0 = d. Friction head loss in one 8" check valve = 	140 Feet 4.4 Feet
	TOTAL Dynamic Head (TDH)	. 346.6 Feet

2. IMPELLER SELECTION:

Since no speed was specified, use 3450 RPM. The S9XHC shows 76% efficiency, full diameter.

a. Number of stages required =

No. Stg. = <u>TDH</u> = <u>346.6</u> = 2.78 USE 3 stages, 75.5% Head/Stage 125

- b. Total Pump Thrust = TDH x Impeller Thrust Factor x Sp. Gr. + (Rotor weight per stage x number of stages) (349.55 x 4.9 x 1) + (10.6 x 3) = 1744.6
- c. Bowl Horsepower = $\frac{\text{GPM x TDH x Sp. Gr.}}{3960 \text{ x Bowl Eff.}}$ = $\frac{850 \text{ x } 346.6 \text{ x } 1}{3960 \text{ x } 75.5\%}$ = 98.54 BHP
- d. Pump Efficiency = $\frac{\text{GPM x TDH x Sp. Gr.}}{3960 \text{ x Bowl H.P.}}$ = $\frac{850 \text{ x } 346.6 \text{ x } 1}{3960 \text{ x } 98.54}$ = 75.5%



SELECTION PROCEDURE EXAMPLE (CONT.)

	MOTOR SELECTION: a. Bowl Horsepower = 98.54 b. Pump Operating Speed = 3450 RPM c. Total Pump Thrust = 1744.6 d. 3 Phase, 60 Hertz, 460 Volts (nameplate) e. Thrust Bearing Loss = <u>.10 x Total Pump Thrust</u> = <u>.10 x 1744.6</u> = .17 H.P. 1000 1000
ſ	f. Horsepower Loss in Cable: Total Cable Length = 200 feet + 10 + 4 = 214 feet Select #00 cable from Selection Chart 100 H.P. motor current = 130 amps full load Horsepower loss in #00 cable = <u>H.P. loss per 100' x Total Cable Length</u> = <u>.65 x 214 = 1.39HP</u> 100 100
9	g. Total Horsepower: = Bowl horsepower + Thrust HP loss + Cable horsepower loss = 98.54 + 1.39 + .17 = 100.10 H.P. (100 H.P. motor OK to use.)
i	 <u>CABLE SELECTION:</u> a. Determine total cable length. Total Cable Length = Pumping Level + Surface Length + Slack = 200 + 10 + 4 = 214 feet b. Per Cable Selection Chart @ 460 volts horsepower, use #00 cable.
	SURFACE PLATE: Use 8" surface plate.
-	<u>CHECK VALVE:</u> One 8" check valve required.
-	CALCULATION OF FIELD PERFORMANCE: To determine field head and overall pump efficiency: a. Field Head = laboratory head minus total friction loss. (1) Total friction loss = loss in drop pipe + check valve(s) b. Overall Pump Efficiency = <u>Water HP x (motor eff. % - cable loss %)</u> Laboratory H.P.
	c. Water Horsepower = <u>GPM x Head</u> 3960 d. Laboratory Horsepower = <u>GPM x Head x Sp. Gr.</u>
	3960 x Pump Eff.
Ca	lculations for other values of power consumption can be carried out per equations noted below:
	e. Wire to Water Efficiency - same as Overall Efficiency. f. Input Horsepower = <u>Pump Brake Horsepower</u> Motor Efficiency - Cable Loss
	g. Wire to Water Horsepower = Same as Input Horsepower h. Kilowatt Hours per 100 Gallons = <u>Field head x .00314</u> Overall Efficiency
	i Kilowette Input - Input Hereenower v 0.746

- i. Kilowatts Input = Input Horsepower x 0.746
- j. Gallons per Kilowatt Hour = <u>Overall Efficiency x 1000</u>

Field Head x .00314





DETERMINATION OF FIELD PERFORMANCE

GENERAL INSTRUCTIONS

- Select drop pipe size from selection chart. (NOTE: 5' per 100' friction loss is maximum; 3.5'/Sec. velocity is minimum.)
 - a. Calculate drop pipe friction loss

Friction per 100 feet x <u>drop pipe length</u> + check valve friction loss 100

b. Calculate Total Dynamic Head (TDH)

TDH = Pumping level + discharge head required at surface + check valve friction loss + drop pipe friction loss

- 2. Impeller Selection: From performance curves with known capacity and speed, select the bowl assembly that has its peak efficiency as close as possible to desired capacity. Well I.D. must be larger than bowl diameter. If speed is unknown, the speed should be as high as possible for a given capacity.
 - a. Number of stages required = <u>TDH</u> = Number of stages Head/stage
 - b. Total Pump Thrust = (TDH x Impeller Thrust Factor x Sp. Gr.) + (rotor weight per stage x number of stages)
 - c. Bowl Horsepower = $\underline{\text{GPM x TDH x Sp. Gr.}}$ 3960 x Bowl Eff.
 - d. Pump Efficiency = <u>GPM x TDH x Sp. Gr.</u> 3960 x Bowl H.P.



DETERMINATION OF FIELD PERFORMANCE (CONT.)

3. MOTOR SELECTION:

Select the proper electric motor from the following:

- a. Bowl Horsepower
- b. Pump Operating Speed
- c. Total Pump Thrust
- d. Electric Power Supply Available
- e. Thrust Bearing Loss in H.P. Horsepower loss per 1000# thrust (given by manufacturer is approx. .09 per 1000# thrust; use .10 H.P. per 1000#) =

1000#

f. Horsepower loss in cable (from Cable Loss Chart) to determine horsepower loss per 100 feet.

Total horsepower loss in cable = horsepower loss per 100' x <u>Total Cable Length</u> 100

g. Total Horsepower:

Total H.P. = bowl horsepower + thrust horsepower loss + cable horsepower loss

- 4. Cable Selection:
 - a. Determine total cable length.

Total cable length = pumping level + surface distance to starter panel + allowance for slack

- NOTE: (1) Slack cable, allow 2 feet per 100 feet
 - (2) 10 foot minimum for surface cable to starter
- b. From cable selection chart under proper voltage, select cable under motor full load amps for length of cable used.

NOTE: If full load amps fall between amps on chart, go to next larger size.

- 5. <u>SURFACE PLATE:</u> Select the same size as drop pipe diameter.
- 6. CHECK VALVE: Select the same size as drop pipe diameter (if required by Technical Data).

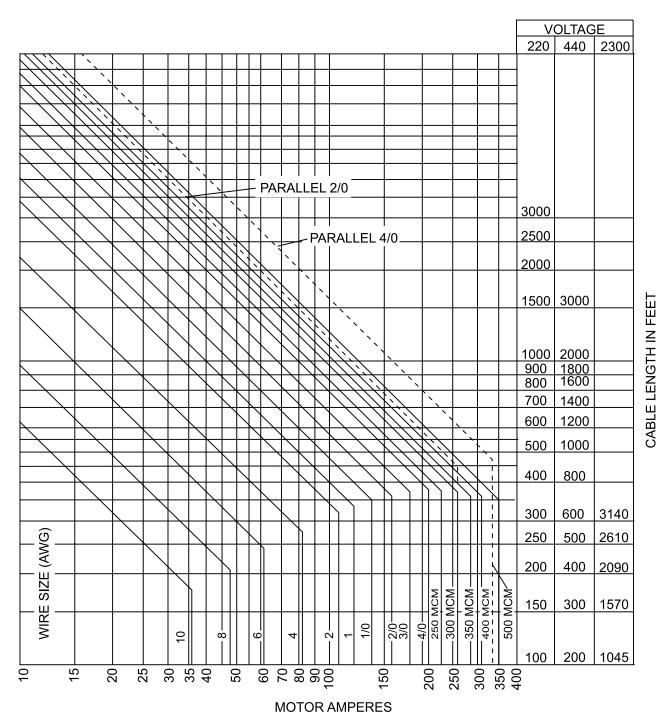
7. ACCESSORIES:

- a. Pump Panel
- b. Air Line and Gauge
- c. Banding Tools
- d. Banding Supplies
- e. Cable



SUBMERSIBLE CABLE SELECTION CHART

CABLE LENGTH VERSUS MOTOR AMPERES



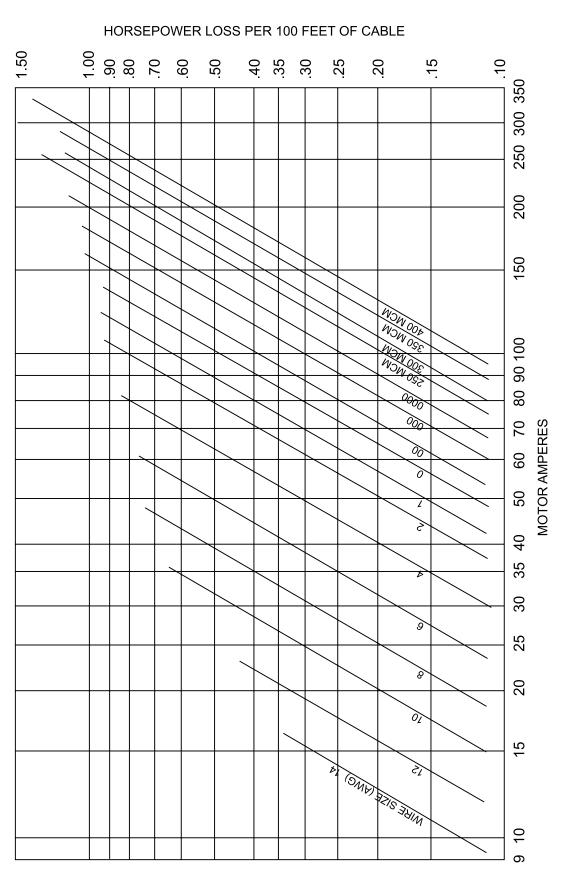
Based on 5% voltage drop - 60° C. copper temperature and 30° C. ambient temperature. Maximum ampere value for each cable size must be reduced if ambient temperature exceeds 30° C.



SUBMERSIB

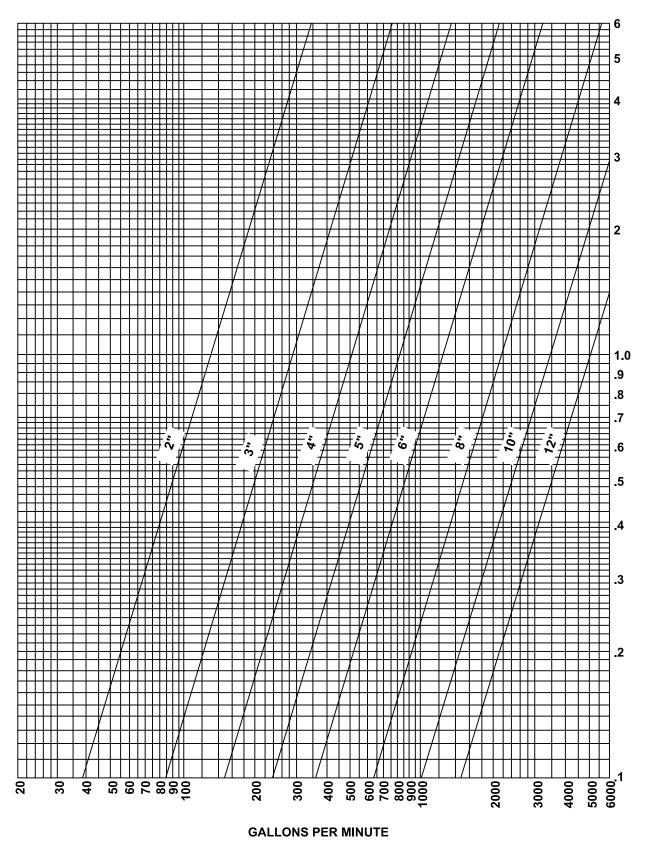
SUBMERSIBLE CABLE LOSS CHART

operating at full lad will draw 200 amperes; checking selection chart we find that 0000 is the minimum recommended cable size for any setting up to 800 To use selection chart find intersection of motor amperes and cable length - use any cable to RIGHT of this point. Example: 150 HP, 440 volt G.E. motor feet. For deeper settings, larger cable must be used. A 900 foot setting on the above motor would require a minimum cable size of 300 MCM



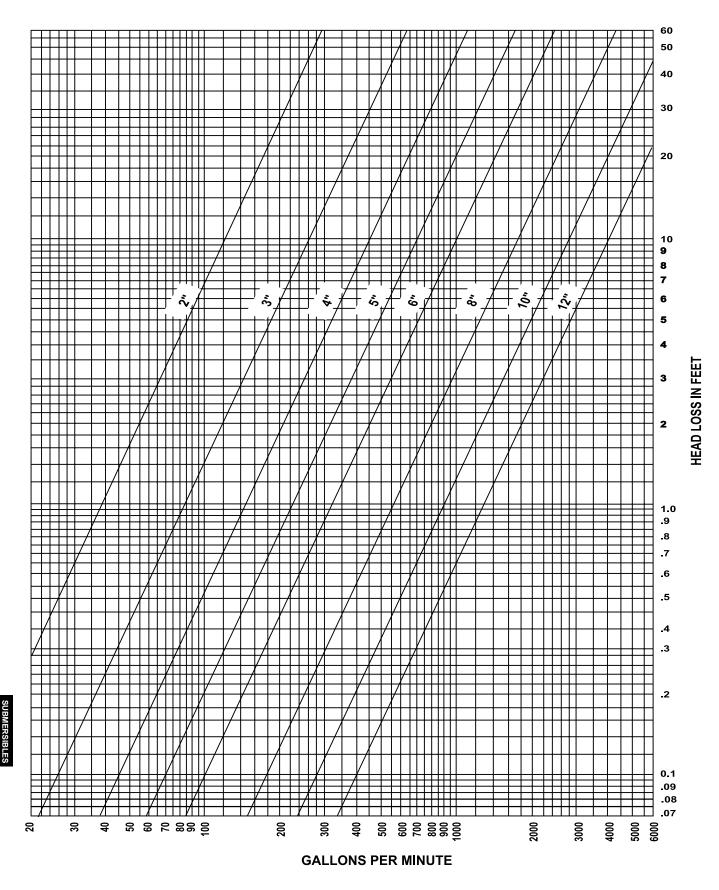
NATIONAL PUMP COMPANY The above chart indicates the power loss (in horsepower) for each 100 feet of submersible cable. This loss must be considered in overall plant efficiency calculations. Long range cost evaluation may dictate the use of a larger than normal size cable.

FRICTION LOSS CHART FOR SUBMERSIBLE SURFACE PLATE ELBOWS



HEAD LOSS IN FEET

FRICTION LOSS CHART FOR SUBMERSIBLE DROP PIPE CHECK VALVES





WEIGHT OF WATER IN FOOT LENGTHS OF PIPE OF DIFFERENT INSIDE DIAMETERS

DIAMETER INCHES	WATER POUNDS	DIAMETER INCHES	WATER POUNDS	DIAMETER INCHES	WATER POUNDS	DIAMETER INCHES	WATER POUNDS
1/8 1/4	0.0053 0.0213	3 3-1/8	3.0643 3.3250	7-3/4 8	20.450 21.790	17 17-1/2	98.897 104.27
3/8	0.0210	3-1/4	3.5963	8-1/4	23.174	18	110.31
1/2	0.0851	3-3/8	3.8782	8-1/2	24.599	18-1/2	116.53
5/8	0.1330	3-1/2	4.1708	8-3/4	26.068	19	122.91
3/4	0.1915	3-5/8	4.4741	9	27.579	19-1/2	129.47
7/8	0.2607	3-3/4	4.7879	9-1/4	29.132	20	136.19
1	0.3405	3-7/8	5.1125	9-1/2	30.728	21	150.15
1-1/8	0.4309	4	5.4476	9-3/4	32.366	22	164.79
1-1/4	0.5320	4-1/4	6.1498	10	34.048	23	180.11
1-3/8	0.6437	4-1/2	6.8946	10-1/2	37.537	24	196.11
1-1/2	0.7661	4-3/4	7.6820	11	41.198	25	212.80
1-5/8	0.8991	5	8.5119	11-1/2	45.028	26	230.16
1-3/4	1.0427	5-1/4	9.3844	12	49.028	27	248.21
1-7/8	1.1970	5-1/2	10.299	12-1/2	53.199	28	266.93
2	1.3619	5-3/4	11.257	13	57.540	29	286.34
2-1/8	1.5375	6	12.257	13-1/2	62.052	30	306.43
2-1/4	1.7237	6-1/4	13.300	14	66.733	31	327.20
2-3/8	1.9205	6-1/2	14.385	14-1/2	71.585	32	348.65
2-1/2	2.1280	6-3/4	15.513	15	76.607	33	370.78
2-5/8	2.3461	7	16.683	15-1/2	81.799	34	393.59
2-3/4	2.5748	7-1/4	17.896	16	87.162	35	417.08
2-7/8	2.8142	7-1/2	19.152	16-1/2	92.694	36	441.26

(62.35 POUNDS PER CUBIC FOOT)

Weights of water in cylinders of the same length are proportional to the squares of the diameters. Therefore, to get weight of cylinder of water one foot long and 60 inches diameter, take from above table weight of water of 30 inch pipe and multiply it by the square of 60 - 30, or the square of two; thus, $306.43 \times 4 = 1226.72 =$ the weight of water in one foot length of a 60 inch pipe.



POWER CONSUMPTION

VARIOUS EFFICIENCIES PUMPING 1000 GALLONS OF CLEAR WATER AT ONE FOOT TOTAL HEAD

OVERALL EFFICIENCY PUMP UNIT	KWH PER 1000 GALLONS AT ONE FOOT TOTAL HEAD	OVERALL EFFICIENCY PUMP UNIT	KWH PER 1000 GALLONS AT ONE FOOT TOTAL HEAD	OVERALL EFFICIENCY PUMP UNIT	KWH PER 1000 GALLONS AT ONE FOOT TOTAL HEAD
32	.00980	51.5	.00609	71	.00442
32.5	.00958	52	.00603	71.5	.00439
33	.00951	52.5	.00597	72	.00435
33.5	.00937	53	.00592	72.5	.00432
34	.00922	53.5	.00586	73	.00430
24.5	00000	F 4	00504	70 5	00407
34.5	.00909	54	.00581	73.5	.00427
35	.00896	54.5	.00575	74	.00424
35.5	.00884	55	.00570	74.5	.00421
36	.00871	55.5	.00565	75	.00418
36.5	.00860	56	.00560	75.5	.00415
37	.00848	56.5	.00555	76	.00413
37.5	<u>.</u> 00837	57	.00550	76.5	.00410
38	.00826	57.5	.00545	77	.00407
38.5	.00815	58	.00541	77.5	.00405
39	.00804	58.5	.00536	78	.00402
39.5	.00794	59	.00532	78.5	.00399
40	.00784	59.5	.00527	79	.00397
40.5	.00775	60	.00523	79.5	.00394
41	.00765	60.5	.00518	80	.00392
41.5	.00756	61	.00514	80.5	.00389
42	.00747	61.5	.00510	81	.00387
42.5	.00738	62	.00506	81.5	.00385
43	.00730	62.5	.00502	82	.00382
43.5	.00721	63	.00498	82.5	.00380
44	.00713	63.5	.00494	83	.00378
	00705		00,400	00 F	00075
44.5	.00705	64	.00490	83.5	.00375
45	.00697	64.5	.00486	84	.00373
45.5	.00689	65	.00482	84.5	.00371
46	.00682	65.5	.00479	85	.00369
46.5	.00675	66	.00475	85.5	.00367
47	.00667	66.5	.00472	86	.00365
47.5	.00660	67	.00468	86.5	.00362
48	.00653	67.5	.00465	87	.00360
48.5	.00647	68	.00461	87.5	.00358
49	.00640	68.5	.00458	88	.00356
49.5	.00634	69	.00454	88.5	.00354
50	.00627	69.5	.00451	89	.00352
50.5	.00621	70	.00431	89.5	.00350
51	.00615	70.5	.00445	90	.00348
		70.0	.00++0		.000+0

KWH/100 GAL. = K*H

K = KWH/1000 GAL. AT ONE FT. HEAD H = TOTAL HEAD



SUBMERSIBLE PUMPS

GENERAL INFORMATION

The application of a submersible pump requires attention to certain conditions which do not exist with a lineshaft pump.

- 1. If there is inadequate or restricted circulation of water past the motor, the motor may overheat and burn out. Each motor manufacturer has different recommendations; but, in general, if water is continually flowing into the pump chamber and flow past the motor is unrestricted, the motor will operate satisfactorily. Consult the factory in doubtful cases. Use of a liquid level control or flow switch to prevent pump from breaking suction is recommended.
- 2. If the temperature of the water exceeds 86° F. (30° C), motor failure may result. Consult factory if water temperature exceeds this limitation.
- 3. The use of semi-open impellers with submersible motors may effect pump performance as the motor shaft expands when the motor is in operation and lifts the impellers away from the bowl seats, thus reducing head by 5 percent and efficiency by 3 percent.
- 4. Length of drop pipe must be sufficient to keep the bowl assembly and motor leads completely submerged at all times.
- 5. Motor controls should be equipped with quick-trip overload protection on all three legs. This is available at very little added cost when the starter or panel is furnished. This protection is required because submersible motors heat up much faster than a conventional motor due to their compact design.
- 6. When pricing cable, allow one extra foot for every 50 feet of drop pipe, plus 10 feet more to connect to surface wiring. If a conduit box is used at the well head (this is highly recommended), three feet extra will usually be adequate.
- 7. Voltage at the motor leads must be within plus or minus 10% of the nameplate voltage. If there is 5% voltage drop in the submersible pump cable, voltage at the surface must not be less than 95% of rated voltage.
- 8. Drop pipe should have 3/4" NPT taper threads with matching heavy duty couplings. 3", 4", and 5" are normally 21 foot random lengths; larger sizes are 20 foot. If butt thread drop pipe is used, it must be pinned at each joint to prevent unscrewing, as the motor torque tends to loosen butt threads.



SUB ASSEMBLY INSTRUCTIONS

MOTOR TO PUMP END

<u>Step 1</u>

Remove the motor and pump end from containers. At this time, check to make sure pump model horsepower matches motor horsepower rating. Also, check motor phase and voltage to make sure it matches power source.

Raise motor to vertical position, making sure motor is adequately supported. Pump and motor should never be assembled in horizontal position as damage to the pump shaft could occur.

<u>Step 2</u>

Raise pump to vertical position over motor, inspect flanges of pump and motor making sure all dust, paint, grease, and rust are removed from flange faces. Make sure no obstruction is in motor coupling.

Step 3

Lower pump slowly onto motor. Guide pump into proper alignment (never rest pump on motor shaft). Align cable recess on pump making sure you do not pinch motor leads. Coupling should slip freely into place to join pump and motor. Pump should be lowered to meet motor flange flush. Bolt pump end and motor together with stainless fasteners provided. NOTE: Should pump end not meet motor flange flush, see Step 4.

<u>Step 4</u>

The thrust assembly is pre-set at factory but could need final adjustment when pump and motor are coupled. The thrust assembly consists of either thrust bolt and jam nut or thrust plug. First, the thrust bolt should be screwed all the way down against the pump shaft. When the bolt bottoms, the bolt may be backed off two (2) turns. With a wrench as a backup, now screw the jam nut against the pump casting and jam lock nut and bolt.

With the thrust plug, screw all the way down against the pump shaft, then back off one and a half (1-1/2) turns. This will allow for ample momentary upthrust.

The thrust assembly, if set too closely, could prevent you from bolting pump and motor or even locking shaft rotation. Make sure you have ample clearance for pump to fit flush with motor.

Consult factory or local sales office should questions arise.



CABLE SPLICING INSTRUCTIONS

There are several good methods of attaching the drop cable to the motor leads. Any method used must have high insulation value, be corrosion resistant, and most of all, must be waterproof under pressure.

As every 2.31 feet of water represents one pound of pressure, the total pressure at the splice depends on the submergence. This is why testing a finished splice in a bucket of water, as is sometimes done, is not an accurate test.

As pressure testing is not a practical operation, in most cases it becomes evident that great care should be used in the splicing operation. Generally, splicing is not a complicated job and if the necessary care and time is taken, there is no reason why the splice should not be successful.

TAPE SPLICING

A good waterproof electrical tape must be used. Never use ordinary friction tape. The tape recommended is the "Scotch" brand due to our personal experience with the product; however, any other brand of good waterproof electrical tape would serve the purpose.

The three types of "Scotch" tape used are as follows:

No. 23 - This is used for the first layer as it affords excellent insulation and, most importantly, it is of a thick pliable texture which is

be noted at this point that on some of the larger sizes of cable splices, it may be necessary to use several wraps of No. 23 to fill the gaps at the connection and smooth out the joint.

No. 33 - This is the tape generally used in tape splicing and is an excellent waterproofing electrical tape which is used for the final 4

tape at close to room temperatures or in some way keep it warm when using.

No. 88 - This tape, although a little more expensive than No. 33, has superior adhesive qualities in cold weather and is highly

firmly but not over-stretched as this tends to "thin the tape out."

TAPE SPLICE INSTRUCTIONS

Cut the cable so that connections will be staggered about 3" apart. (See Figure 1.) Taking care not to nick or cut the copper conductor, strip enough insulation from wire to fit well into connector. Shape the end of the insulation in the manner of sharpening a pencil. This makes it easy to fill the void between the insulation and connector. Carefully scrape or sand the copper wire clean. This step is very important if finished splice is to be a trouble free connection.

Following the cable color code, crimp the wires in the connectors. It is important that the proper crimping tool is used rather than ordinary pliers. If a crimping tool is not available, it is recommended that a good solder connection is made between the wire and the connector. Never use an acid core solder on electrical connections.

As most outer cable insulation has a wax type finish which makes a poor surface for the tape, use sandpaper or steel wool and clean the surface from 3" to 6" on each side of the connector, depending on the size splice to be made. (See Figure 2.)

Fill in around the connector and 1-1/2" to 2-1/2" along the cable with the No. 23 or No. 33 tape. Then, using No. 33 or No. 88 tape, wrap firmly and smoothly (without wrinkles) using an overlap of about half the width of the tape. Complete the splice with 4 of these finishing laps, taking each layer beyond the end of the layer underneath to make a tapered finish. (See Figure 3.) When finished, cut; do not tear the tape. To help insure good sealing, finish off with a coat of "Scotchkote" which is a fairly fast drying sealant and bonding agent. Some pump men prefer to use this sealant between each layer of tape, which is, of course, an added safety feature, but not absolutely necessary if the rest of the splice has been made with care.

A very good splice can also be made using heat shrink tubing in combination with the aforementioned tapes. The shrink tubing contains a sealant which melts when treated, thus making a better seal between cable and tubing.

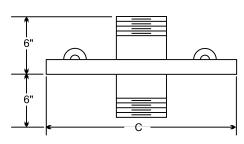
To use shrink tubing, prepare cables in the same way; slide tubing on cables and make connections. Fill in the gaps with No. 23 or No. 33 tape. Centralize tubing on connector; then, using a small heating torch, heat the tubing, working out from the center until the sealant flows from the ends of the tubing. CAUTION: Do not allow naked flame to contact the tubing or the cables.

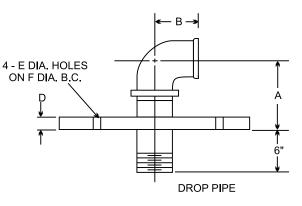
Cover the tubing with 2 or 3 lap layers of No. 33 or No. 88 tape and coat with Scotchkote.



"LDS" SUBMERSIBLE PUMP SURFACE PLATE

DIMENSIONS





DROP PIPE SIZE	А	В	WELL I.D. (NOM.)	С	D	E	F
3	8-3/16	3-1/8	6	11	1	7/8	9-1/2
4	8-11.16	3-3/4	8	13-1/2	1	7/8	11-3/4
5	9-5/16	4-1/2	10	16	1-1/4	1	14-1/4
6	9-7/8	5-1/8	12	19	1-1/4	1	17
			14	21	1-1/4	1-1/8	18-3/4
			16	23-1/2	1-1/2	1-1/8	21-1/4
			18	25	1-1/2	1-1/4	22-3/4
			20	27-1/2	1-1/2	1-1/4	25

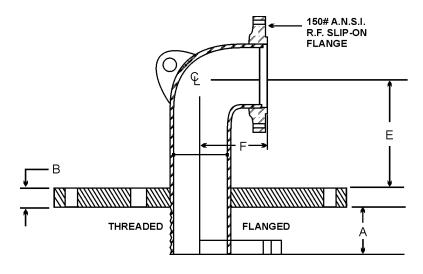
ALL DIMENSIONS ARE IN INCHES

- 1. Standard construction includes steel base plate (not machined) with threaded both ends pipe welded through the center; four foundation bolt holes; two lifting eyes, holes for cable, airline and vent; maximum setting is 600-feet. Contact factory for deeper setting.
- 2. Specify for machined bottom of baseplate and drilling additional holes to match 150# F.F. flange.
- 3. Specify for weather tight junction box, maximum 460 volts.



"HDS" SUBMERSIBLE DISCHARGE HEAD

DIMENSIONS



4 - "C" HOLES ON A "D" DIAMETER B.C. FOUNDATION BOLT HOLES

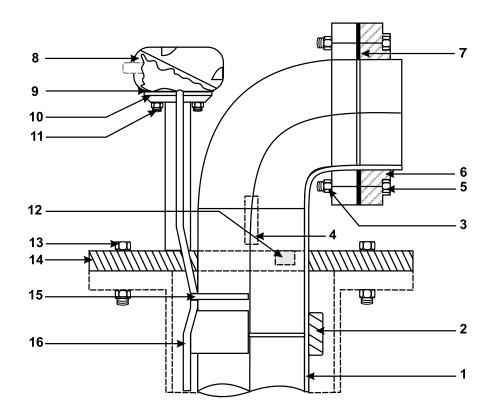
- ALL DIMENSIONS ARE IN INCHES -

DISCHARGE SIZE	CASING SIZE	O.D.	А	В	С	D	E	F	APPROX. WEIGHT
	6	11	6	1	7/8	9-1/2	8	5	50
3"	8	13-1/2	6	1	7/8	11-3/4	8	5	67
	10	16	6	1	1	14-1/4	8	5	90
	6	11	6	1	7/8	9-1/2	8	6-1/2	60
4"	8	13-1/2	6	1	7/8	11-3/4	8	6-1/2	77
-	10	16	6	1	1	14-1/4	8	6-1/2	100
	12	19	6	1-1/8	1	17	8	6-1/2	122
	8	13-1/2	6	1	7/8	11-3/4	9	8-1/2	86
5"	10	16	6	1	1	14-1/4	9	8	106
5	12	19	6	1-1/8	1	17	9	8	142
	14	21	6	1-1/4	1-1/8	18-3/4	9	8	178
	10	16	6	1	1	14-1/4	9	9-1/2	106
	12	19	6	1-1/8	1	17	9	9-1/2	154
6"	14	21	6	1-1/4	1-1/8	18-3/4	9	9-1/2	191
	16	23-1/2	6	1-1/4	1-1/8	21-1/4	9	9-1/2	202
	18	25	6	1-1/4	1-1/4	22-3/4	9	9-1/2	242
	12	19	6	1-1/8	1	17	12	12-1/2	190
8"	14	21	6	1-1/4	1-1/8	18-3/4	12	12-1/2	228
ŏ	16	23-1/2	6	1-1/4	1-1/8	21-1/4	12	12-1/2	238
	18	25	6	1-1/4	1-1/4	22-3/4	12	12-1/2	278
	14	21	6	1-1/4	1-1/8	18-3/4	15	15-1/2	269
	16	23-1/2	6	1-1/4	1-1/8	21-1/4	15	15-1/2	260
10"	18	25	6	1-1/4	1-1/4	22-3/4	15	15-1/2	320
	20	27-1/2	6	1-3/8	1-1/4	25	15	15-1/2	380
	24	32	6	1-1/2	1-3/8	29-1/2	15	15-1/2	490
	16	23-1/2	6	1-1/4	1-1/8	21-1/4	18	18-1/2	342
12"	18	25	6	1-1/4	1-1/4	22-3/4	18	18-1/2	382
12	20	27-1/2	6	1-3/8	1-1/4	25	18	18-1/2	442
	24	32	6	1-1/2	1-3/8	29-1/2	18	18-1/2	552

Surface plates listed consist of a round steel plate machined one side with a flanged or threaded pipe welded through the center. Four foundation bolt holes, lifting lugs, and holes for cable, airline, and well vent are incorporated in the construction of the head. The discharge flange will be a 150 lb. raised face. (Companion flange, bolts, nuts, junction box, and gaskets are not supplied.) A square surface plate instead of a round surface plate is optional at no additional cost.



"HDS" SUBMERSIBLE PUMP SURFACE PLATE



ITEM NO.	DESCRIPTION	ITEM NO.	DESCRIPTION
1	DROP PIPE	9	STOVE BOLT, RND. HEAD (4)
2	PIPE COUPLING	10	CONDUIT BOX - GASKET
3	HEX NUT COMPANION FLANGE	11	SQUARE NUT
4	LIFTING LUGS	12	PIPE PLUG
5	HEX BOLT COMPANION FLANGE	13	CASING BOLTS
6	COMPANION FLANGE	14	SURFACE PLATE
7	GASKET, COMPANION FLANGE	15	CABLE CLAMP
8	CONDUIT BOX (OPTION)	16	POWER CABLE

Standard construction includes steel baseplate (not machined) with threaded one end pipe welded through the center and 90 degree elbow with 150# R.F. flanged discharge; four foundation bolt holes; threaded cable/conduit box connection; holes for airline and vent. All other item are optional features.



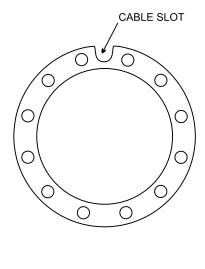
"HDS" SUBMERSIBLE PUMP SURFACE PLATE

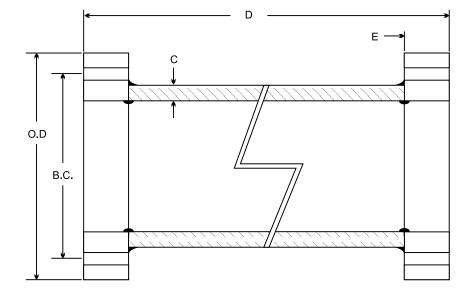
AIR VENT TAP 4DIS. HO NPTI /DIA.	
WELL SOUNDING TAP NPT	<pre># R.F. DISCHARGE FLANGE JUNCTION BOX</pre>
REMARKS	CTION FURNISHED BY



SUBMERSIBLE FLANGED COLUMN PIPE

DIMENSIONS





COLUMN PIPE SIZE	O.D.	B.C.	NO. OF HOLES	SIZE OF HOLES	с	D	E	SIZE & LENGTH OF BOLTS REQUIRED
3	6-1/2"	5.50	4	3/4"	.216	A.R.	3/4"	5/8" x 2-1/2"
4	7-1/2"	6.25	8	3/4"	.237	A.R.	3/4"	5/8" x 2-1/2"
5	10	8.62	8	7/8"	.258	A.R.	1"	3/4" x 3"
6	10	8.62	8	7/8"	.280	A.R.	1"	3/4" x 3"
8	12	10.62	8	7/8"	.322	A.R.	1"	3/4" x 3"
10	14-5/8"	13.00	12	1"	.365	A.R.	1-1/8"	7/8" x 3-1/2"
12	16-5/8"	15.00	12	1"	.375	A.R.	1-1/4"	7/8" x 3-1/2"
14	18-1/2"	16.75	12	1"	.375	A.R.	1-3/8"	7/8" x 4"
16	21-1/2"	18.75	12	1-1/8"	.375	A.R.	1-3/8"	1" x 4"
18	23"	21.00	12	1-1/4"	.375	A.R.	1-5/8"	1-1/8" x 4-1/2"
20	25"	23.00	16	1-1/4"	.375	A.R.	1-5/8"	1-1/8" x 4-1/2"
OTE: A R	= As Real	uired	<u> </u>	1	<u> </u>		I	1

OTE: A.R. = As Required.

CUSTOMER'S SPECIFICATIONS										
PIPE SIZE	O.D.	B.C.	NO. OF	SIZE OF	С	D	Е			



SUBMERSIB

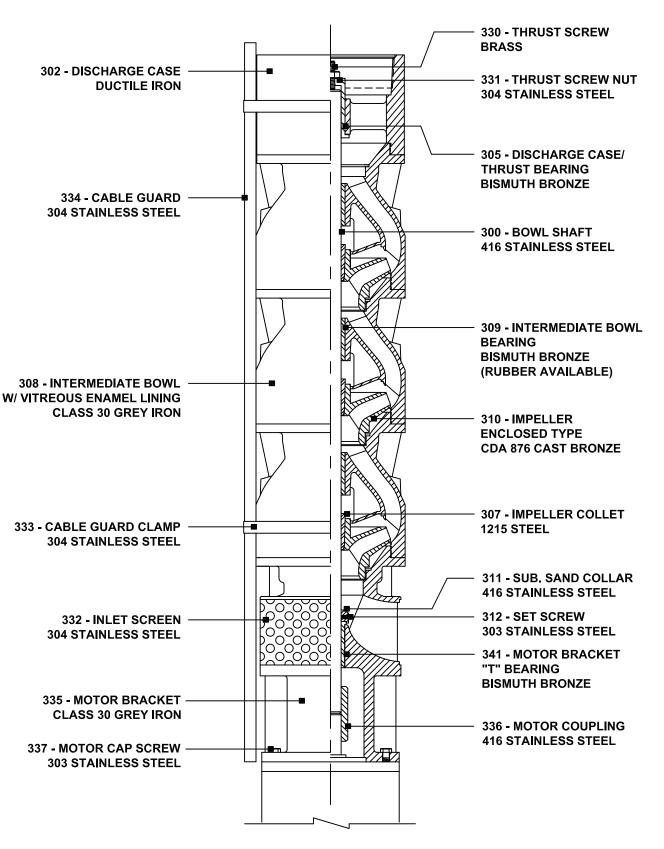
SUBMERSIBLE PUMP AND MOTOR

		MOTOR	2				
	H.P PHASE						
	R.P.MMFG						
			_				
		CABLE	Ξ				
	SIZE LEN	IGTH	TYPE				
	DROP PIPE						
	SIZE LENGTH SECTIONS						
			□ THREADED				
	PUMP						
			074 050				
		<u>م</u>	STAGES				
	US GPM @ AIR LINE □ YES	 □ NO	LENGTH				
	DEPTH GAUGE YES						
	CONTROL PANEL						
	PANEL MANUFACTURE SHORT CIRCUIT DEVIC						
				ING			
			NGTYPE				
			NDARD DEI				
	STARTER MANUFACTU						
	STARTER MANOFACTO						
	TYPE OF STARTER						
			TOTRANSFORM	1FR			
	HEATERS MANUFACTU						
	NUMBER						
	SUBTROL-PLUS:						
	IF YES OVERLOAD SE						
	UNDERLOAD SET?] YES SET AT _	AMPS			
	MATERIALS						
	DROP PIPE	IN	NTAKE SCREEN	I			
	BOWLS						
	IMPELLERS						
	BOWL SHAFT						
	BOWL BRGS						
MARKS:		CUSTO	MER				
	NOT FOR CONSTRUCTION						
	UNLESS CERTIFIED	FURNIS	HED BY				
		P.O. NO)				
	MFG. BY NATIONAL PUMP						
	COMPANY GLENDALE, AZ	PUMP SERIAL NO.					
	5.475						
	DATE:		DRAW	ING NO.			



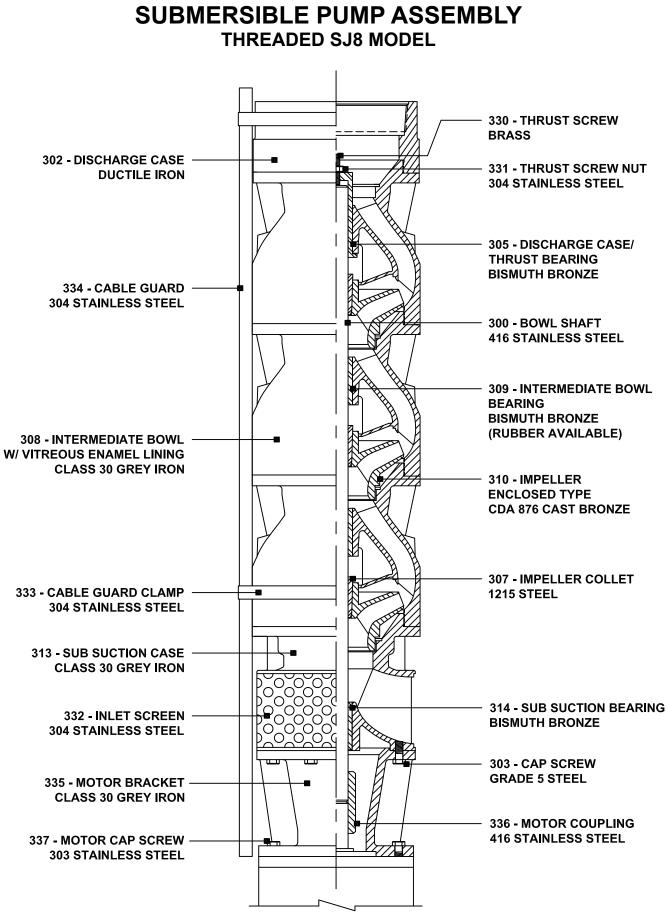


SUBMERSIBLE PUMP ASSEMBLY THREADED S6 - SE6 MODELS



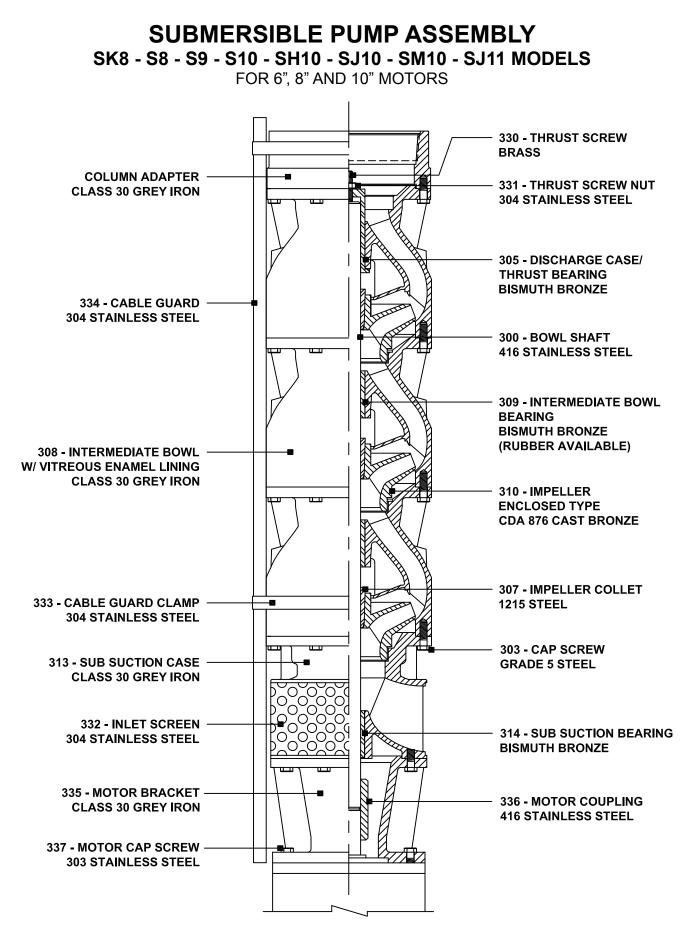
ALTERNATE MATERIAL AVAILABLE UPON REQUEST



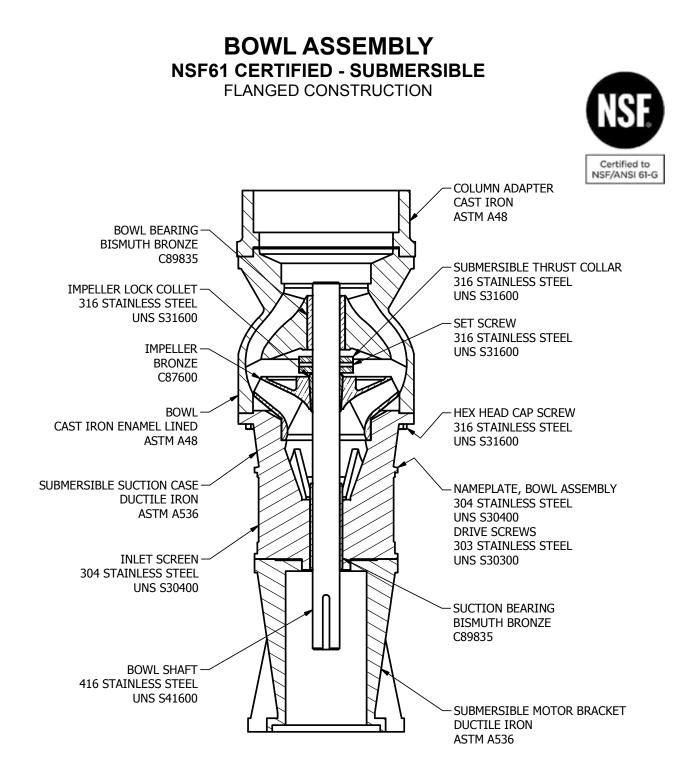


ALTERNATE MATERIAL AVAILABLE UPON REQUEST









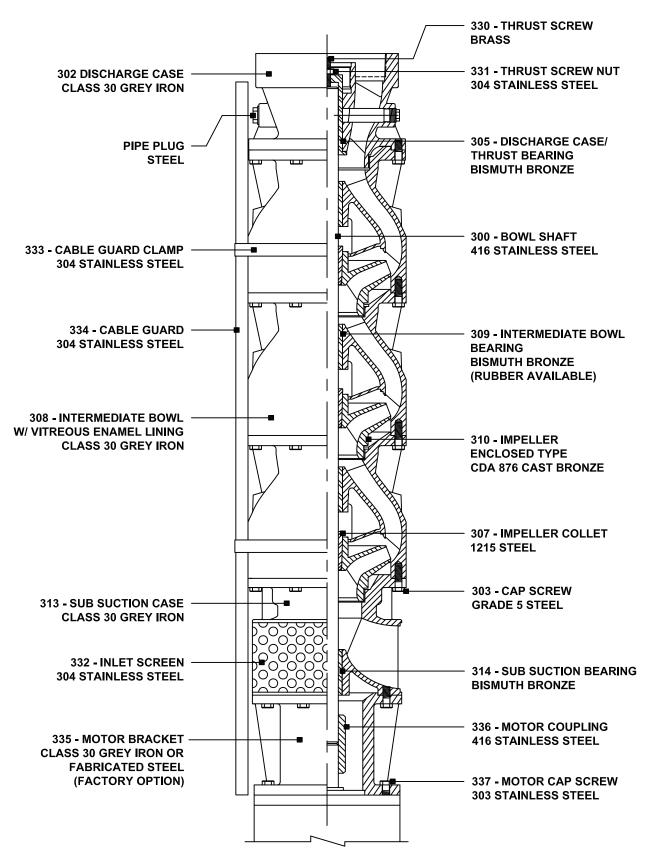
NSF 61 LISTING INFORMAITON: PRODUCT TYPE: SUBMERSIBLE PUMP - PUMP ENDS TRADE DESIGNATION: SUBMERSIBLE BOWL ASSEMBLY (W)(XX)(Y)(Z) W: HYDRAULIC DESIGN (M, K, J, E, H) XX: SIZE, IN INCHES (6, 8, 9, 10, 11, 12, 14, 16, 18, 20, 24, 30) Y: DROP-IN BEARING RETAINERS & BEARINGS (4, 6, 8, 10, 12) - COLUMN SIZE Z: COATING OPTIONS (C, U)

BowlAssy,NSF61,Submersible (2013.04.22)

ALTERNATE MATERIALS NOT AVAILABLE



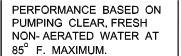
SUBMERSIBLE PUMP ASSEMBLY LARGE MODELS



ALTERNATE MATERIAL AVAILABLE UPON REQUEST

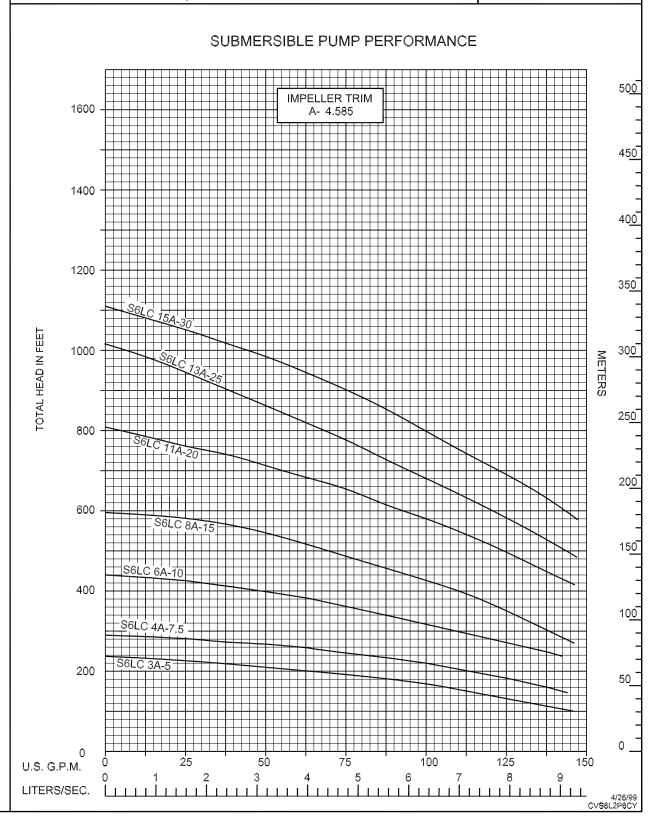


NOTES

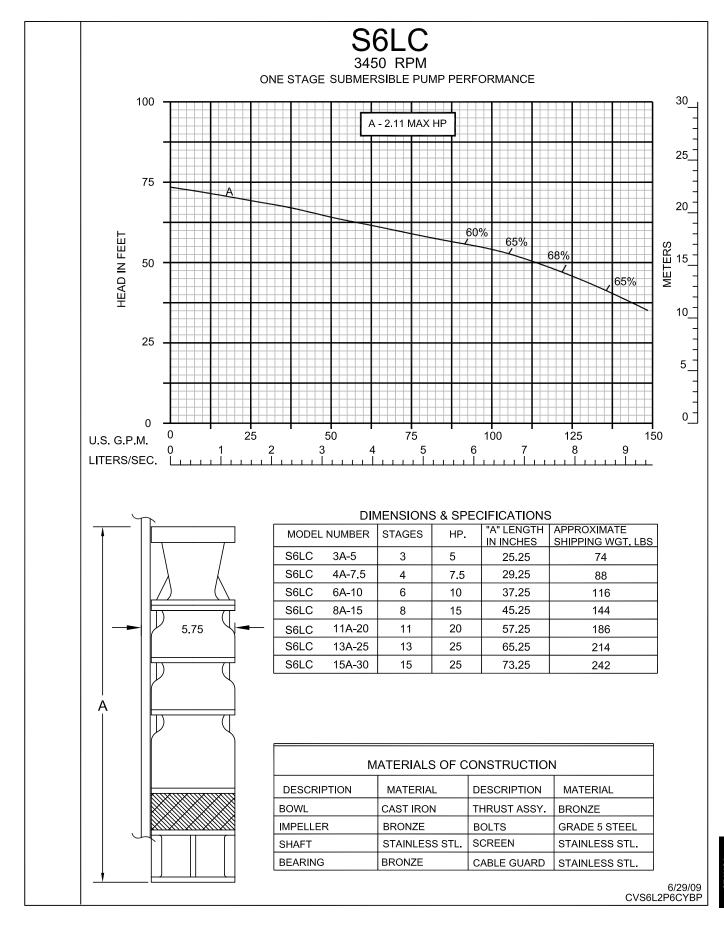




S6LC 3450 RPM



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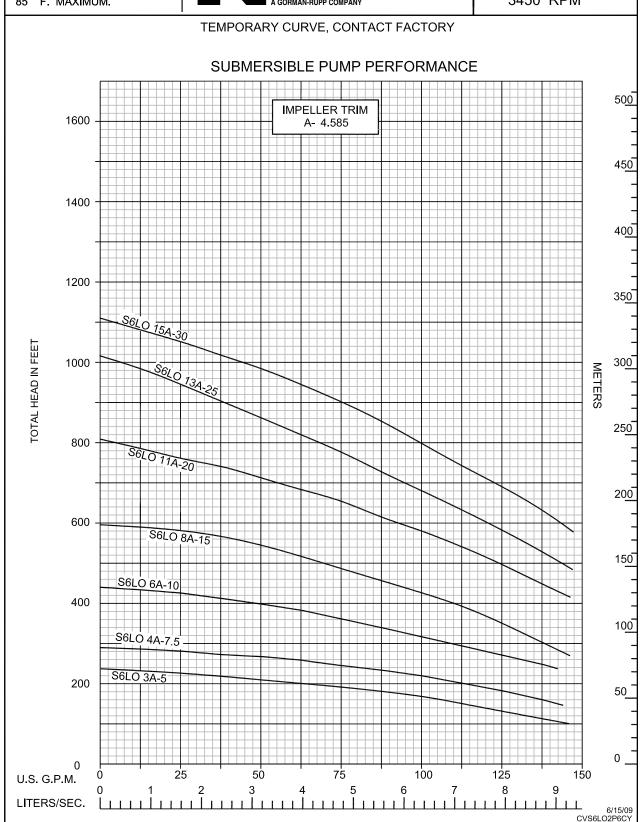




PERFORMANCE BASED ON PUMPING CLEAR, FRESH NON- AERATED WATER AT 85° F. MAXIMUM.

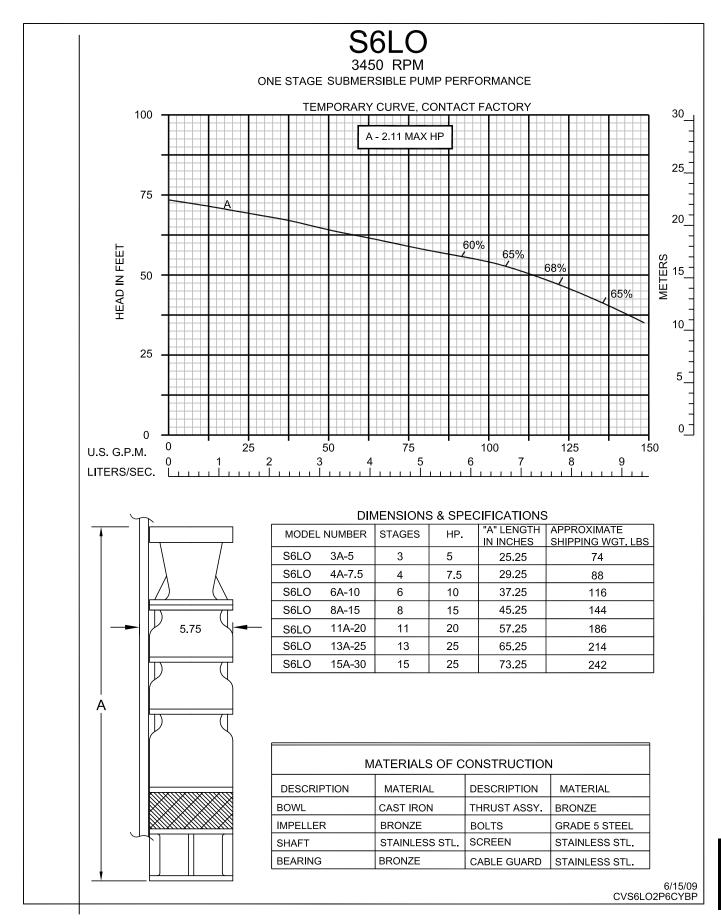


S6LO 3450 RPM



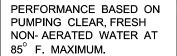
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CURVES



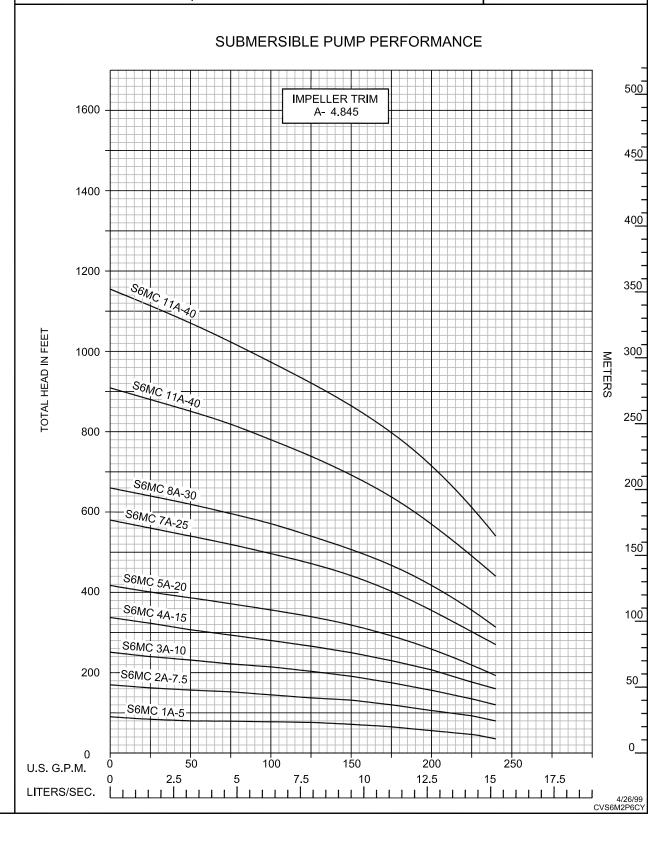
MERSIBLE



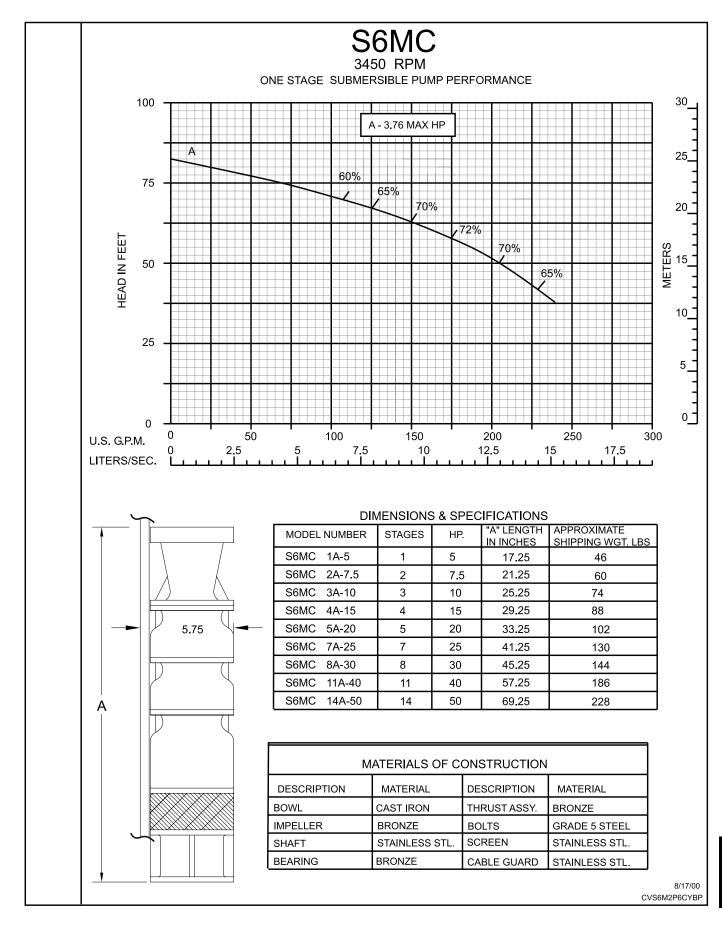








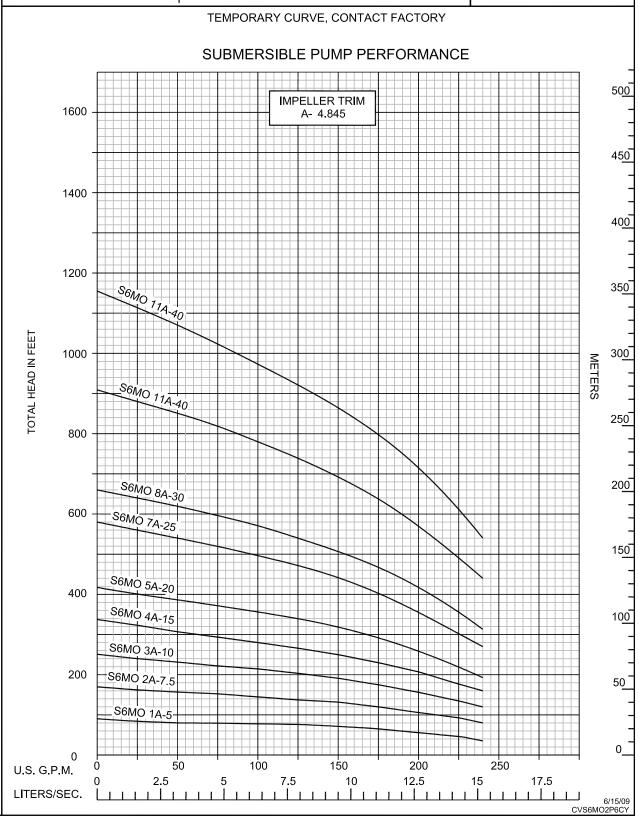
CURVES



UBMERSIBLE CURVES PERFORMANCE BASED ON PUMPING CLEAR, FRESH NON- AERATED WATER AT 85° F. MAXIMUM.

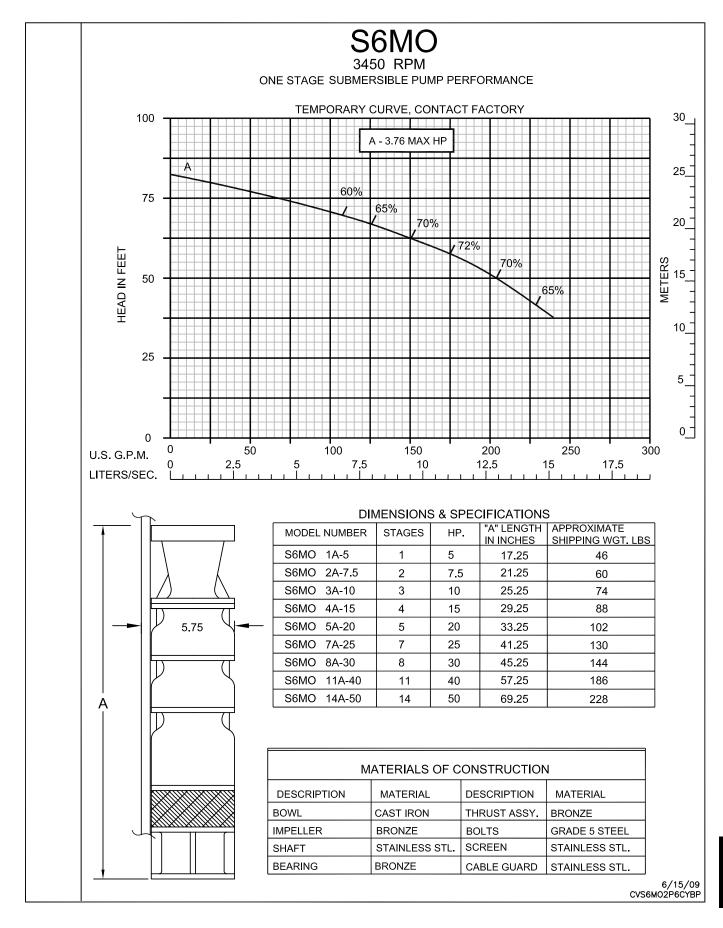


S6MO 3450 RPM

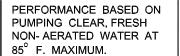


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CURVES

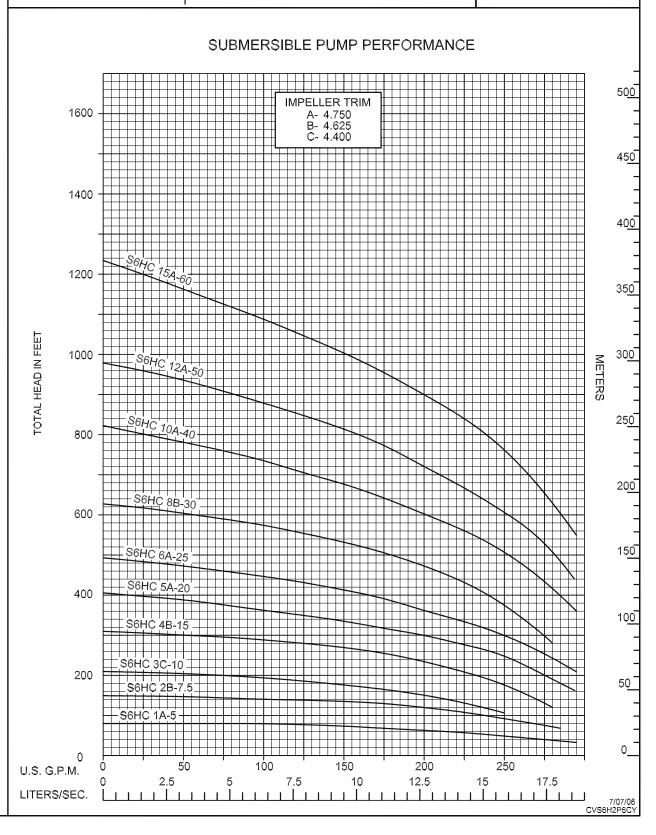




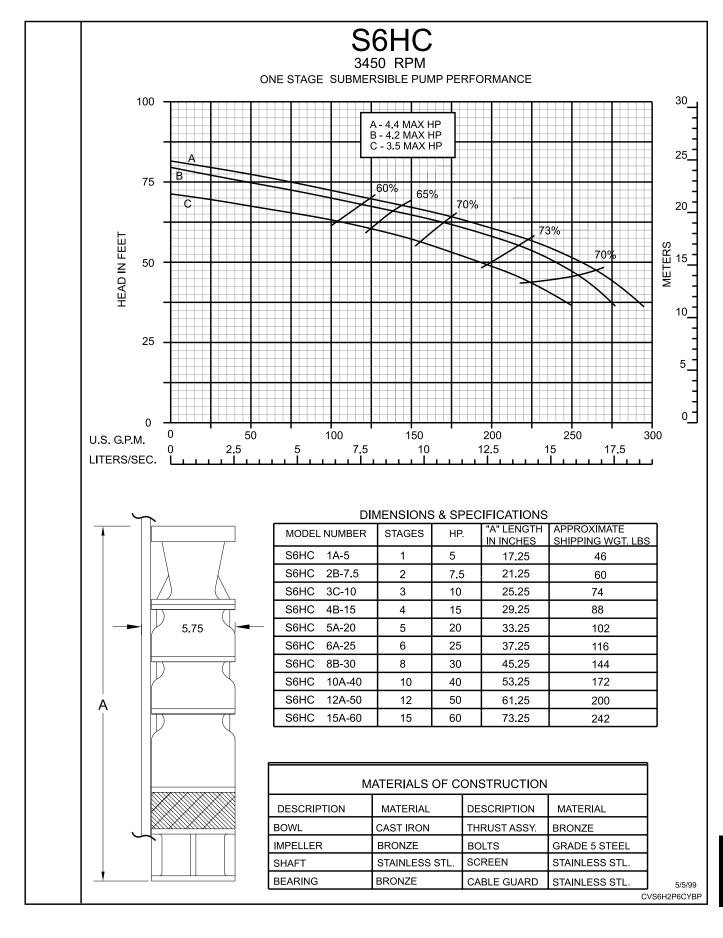


BATIONAL PUMP
 A GORMAN-RUPP COMPANY

S6HC 3450 RPM



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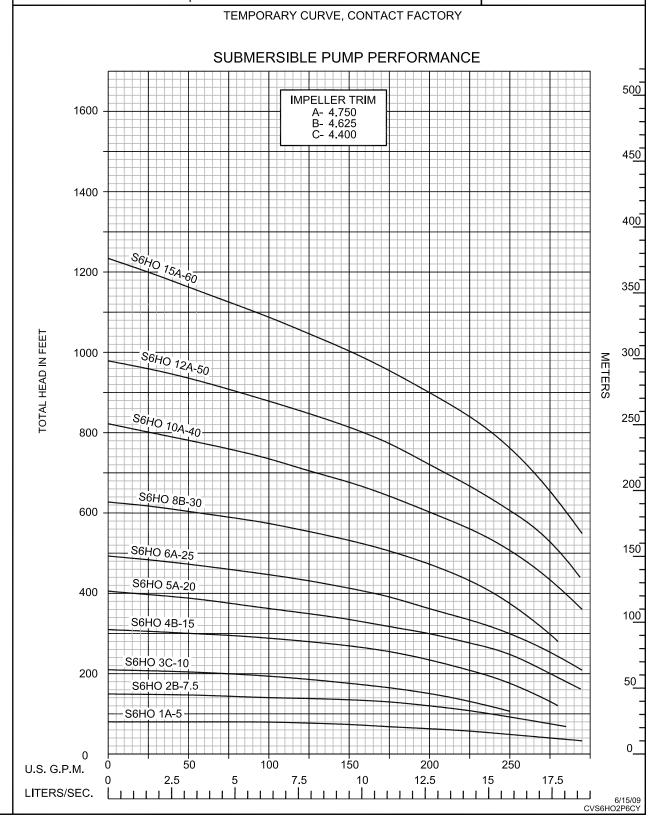


JBMERSIBLE

PERFORMANCE BASED ON PUMPING CLEAR, FRESH NON- AERATED WATER AT 85° F. MAXIMUM.

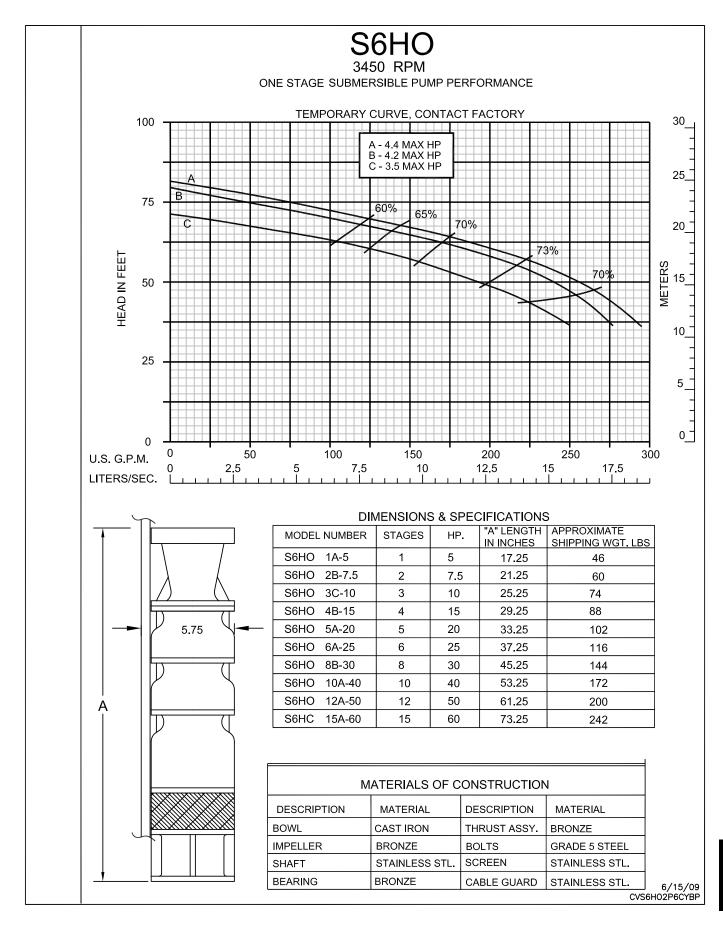


S6HO 3450 RPM



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CURVES



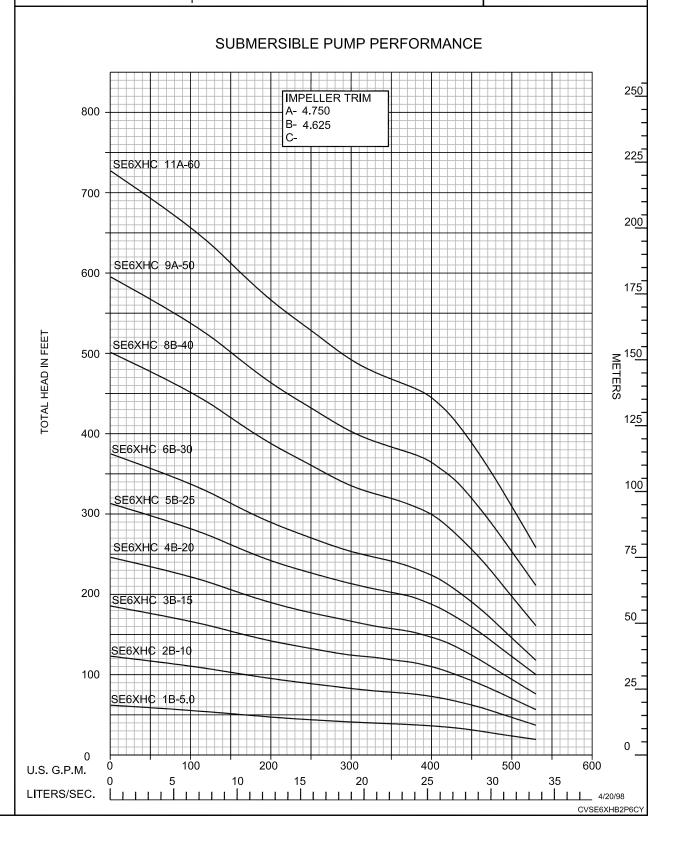
JBMERSIBLE

PERFORMANCE BASED ON PUMPING CLEAR, FRESH NON- AERATED WATER AT 85° F. MAXIMUM.



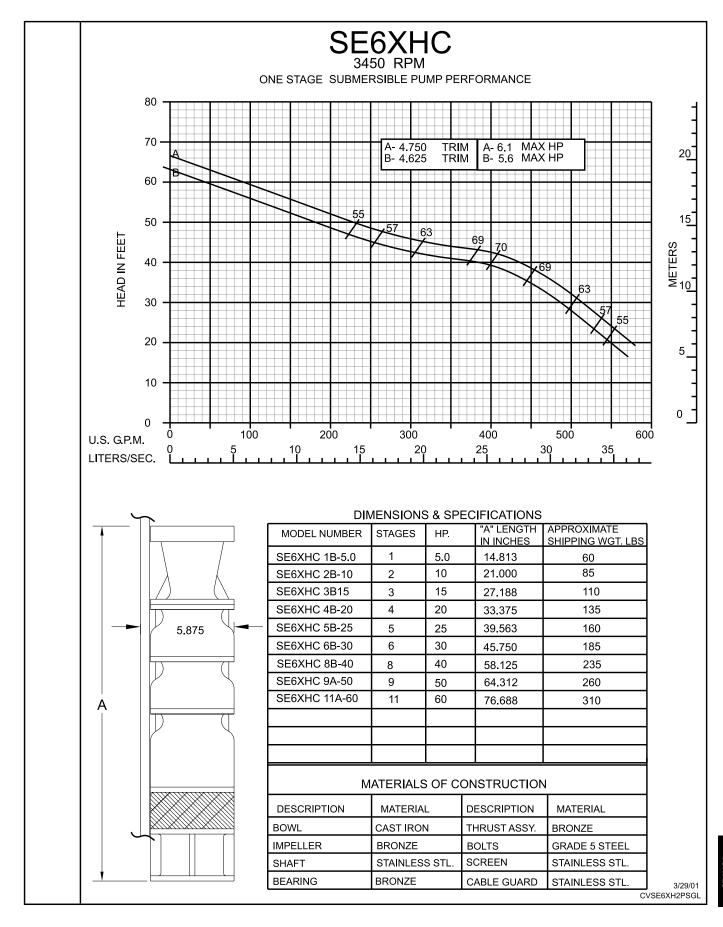
SE6XHC

3450 RPM



N

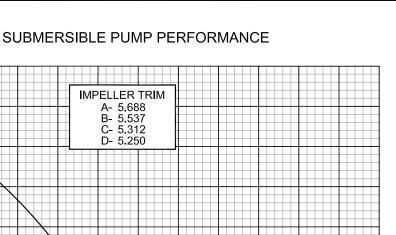
CURVES

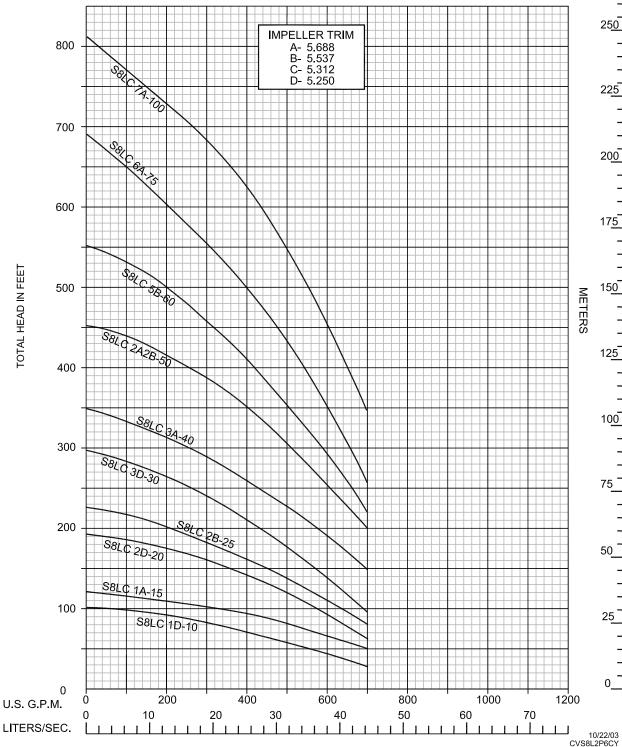


BMERSIBLE CURVES PERFORMANCE BASED ON PUMPING CLEAR, FRESH NON-AERATED WATER AT 85° F. MAXIMUM.



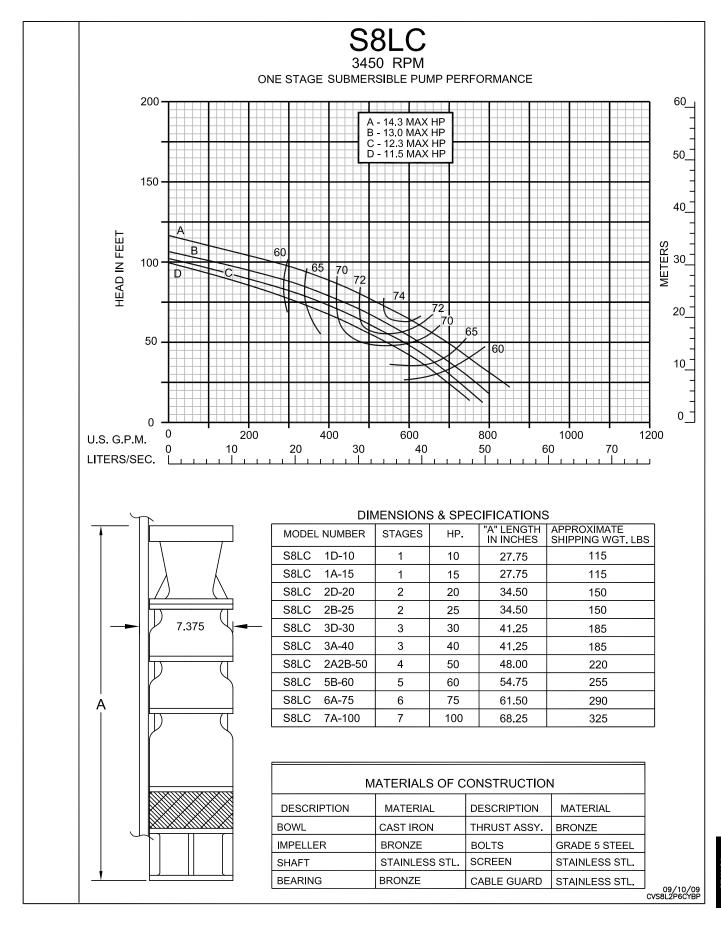
S8LC 3450 RPM





N

SUBMERSIBI CURVES



JBMERSIBLE

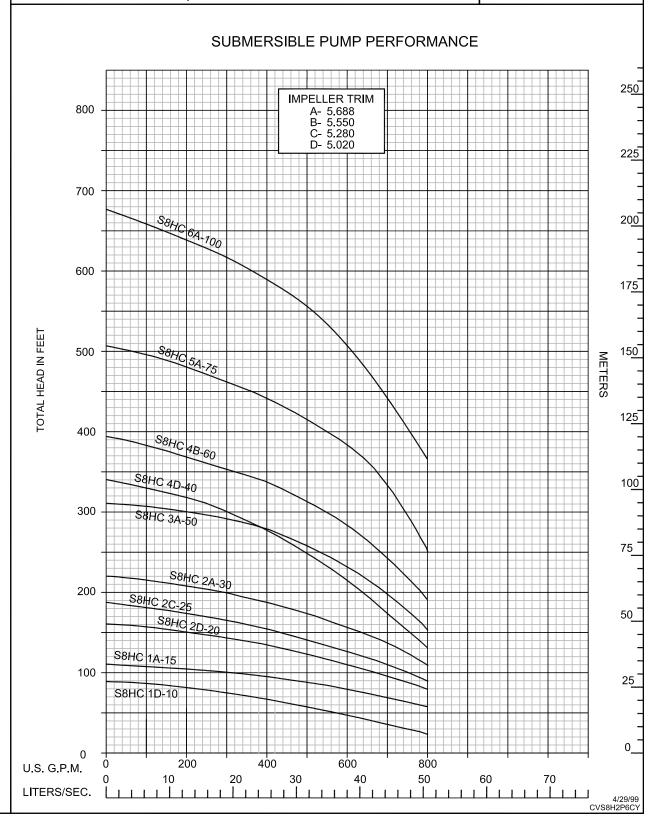
293

PERFORMANCE BASED ON PUMPING CLEAR, FRESH NON- AERATED WATER AT 85° F. MAXIMUM.

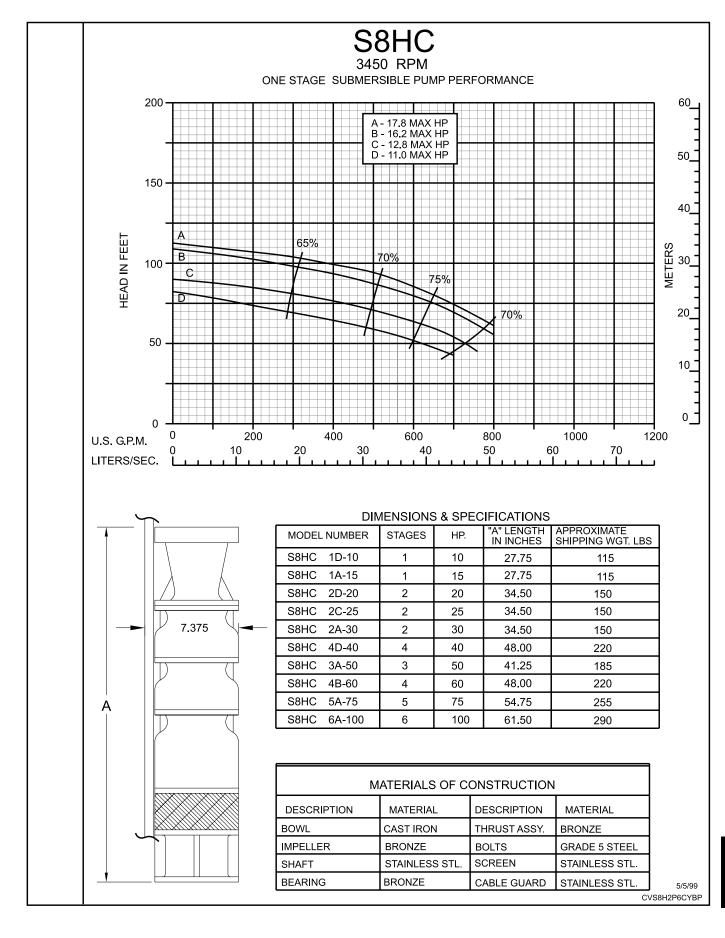


S8HC

3450 RPM



SUBMERSIBI CURVES



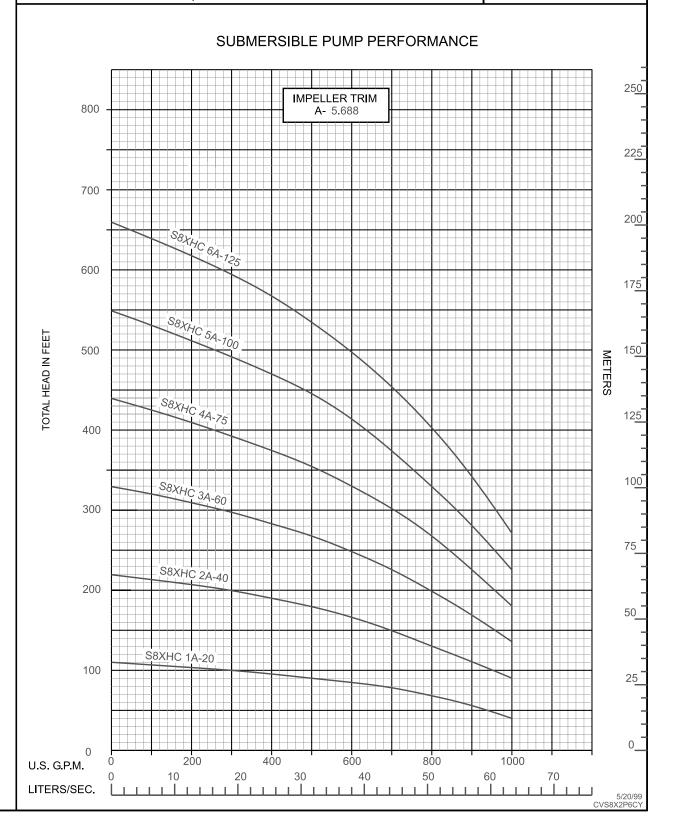


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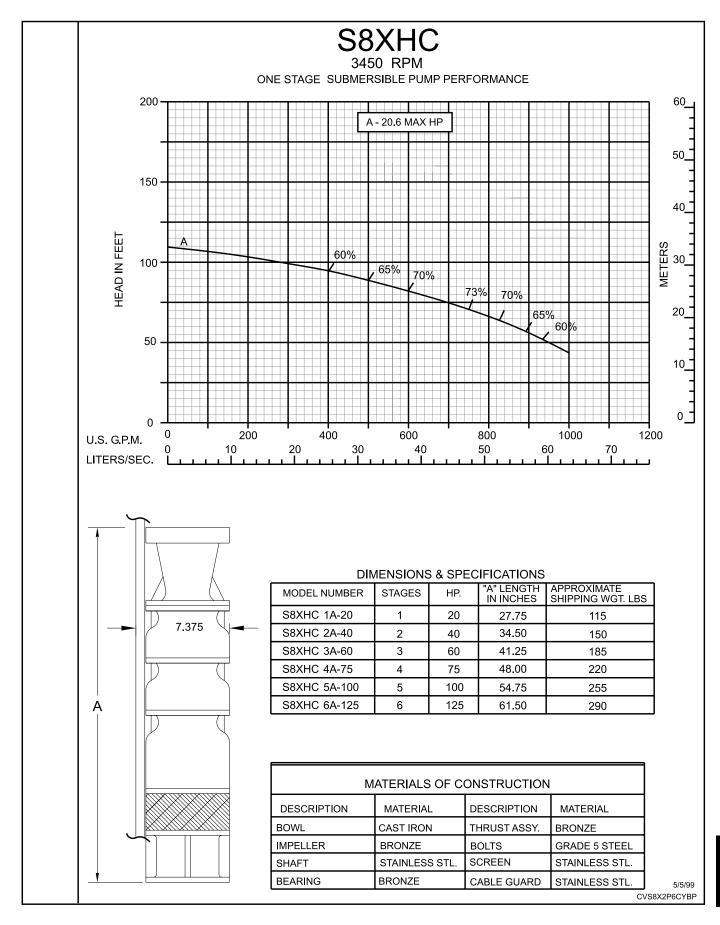


S8XHC

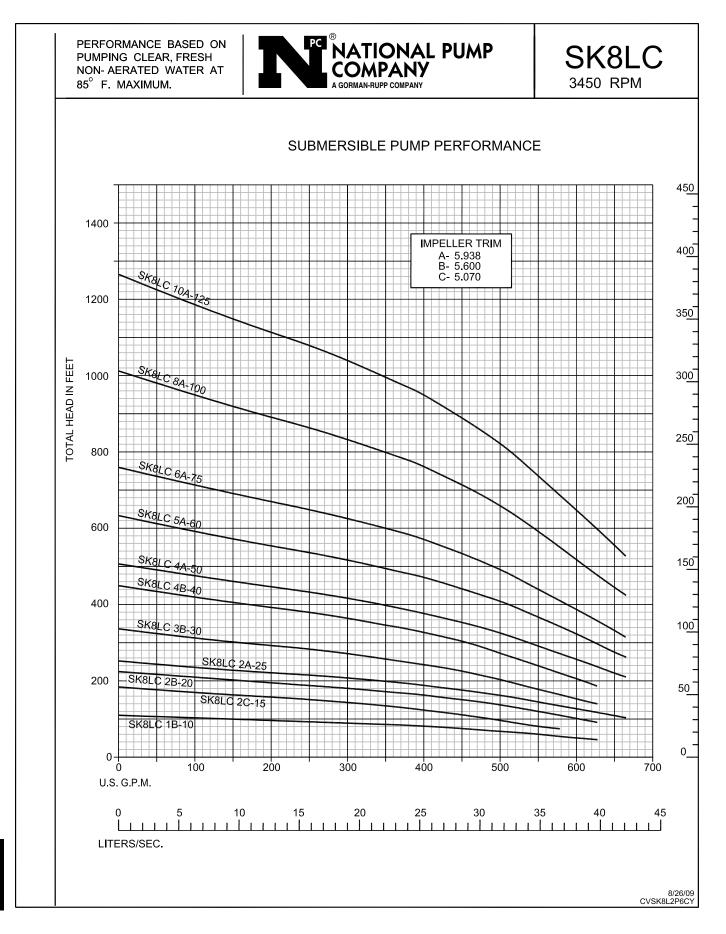
3450 RPM



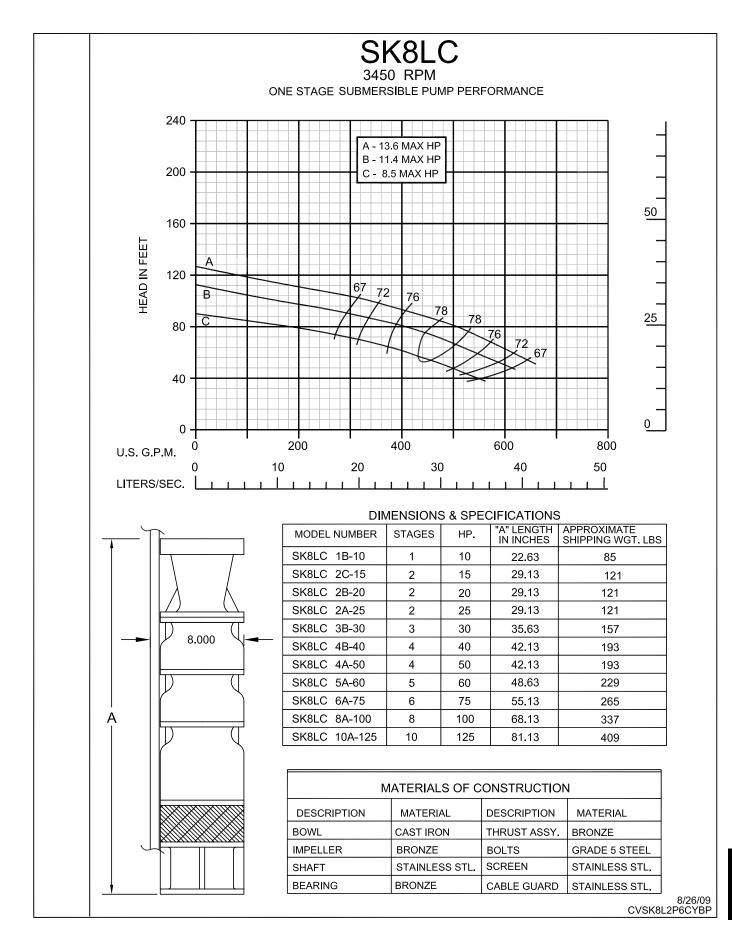
SUBMERSIBL CURVES



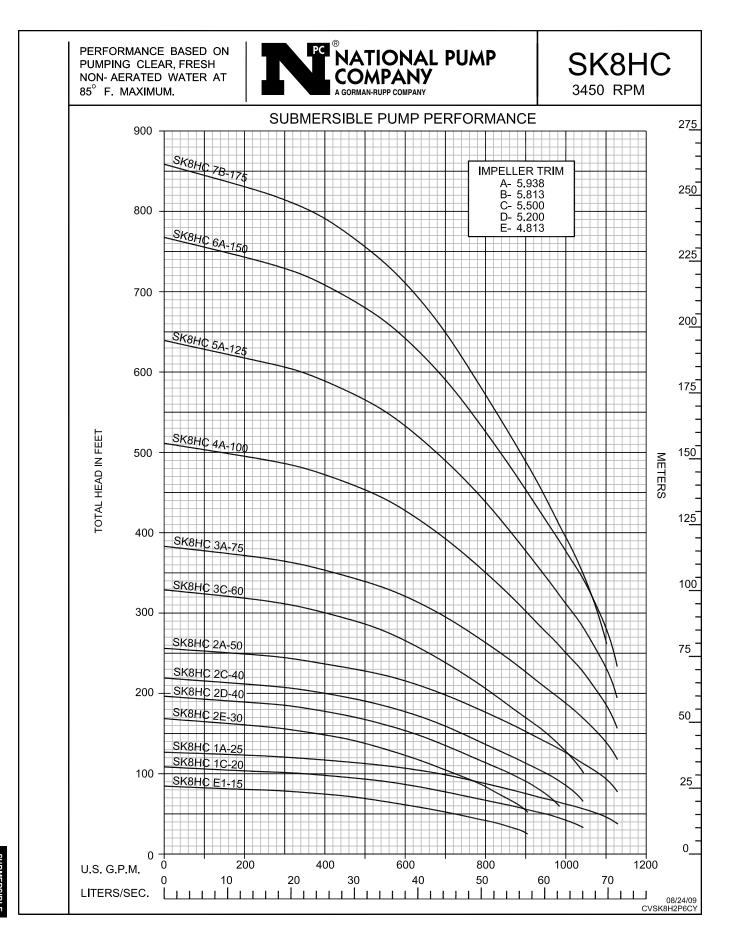
BMERSIBLE CURVES



N



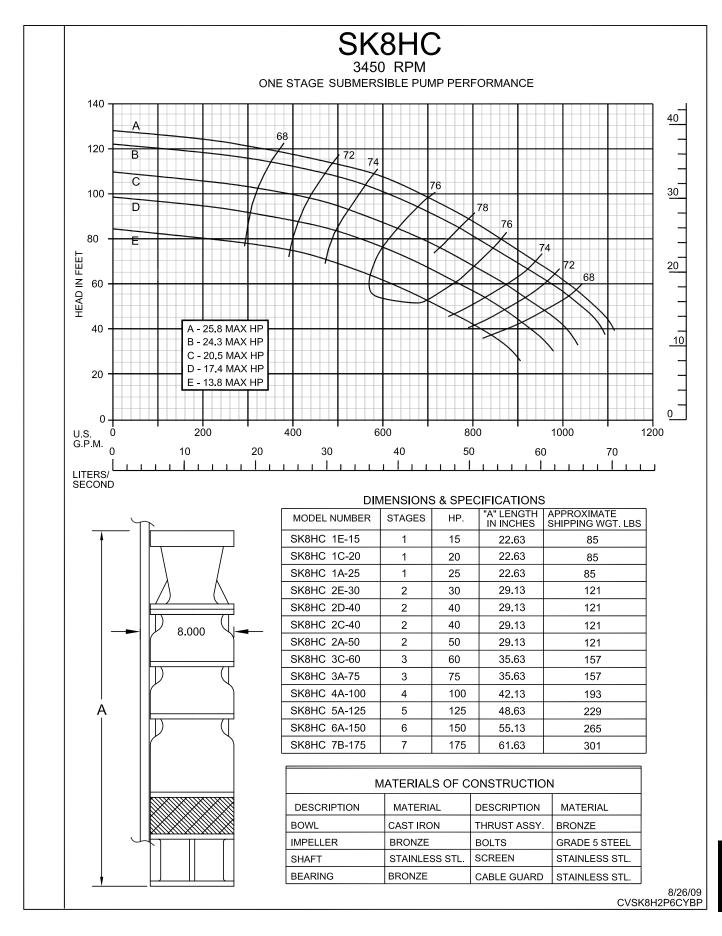
UBMERSIBLE



N

CURVES

300



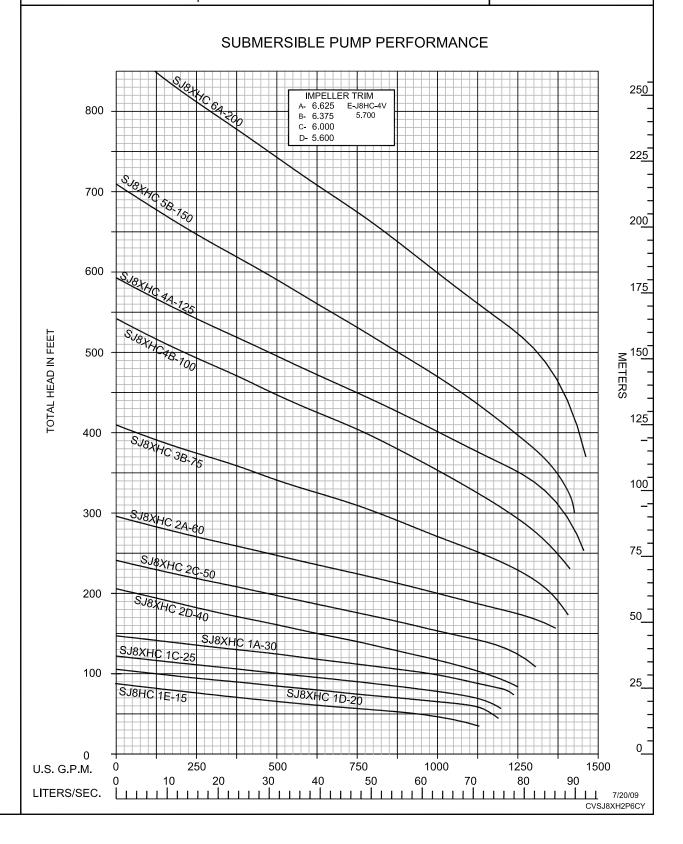


PERFORMANCE BASED ON PUMPING CLEAR, FRESH NON- AERATED WATER AT 85° F. MAXIMUM.



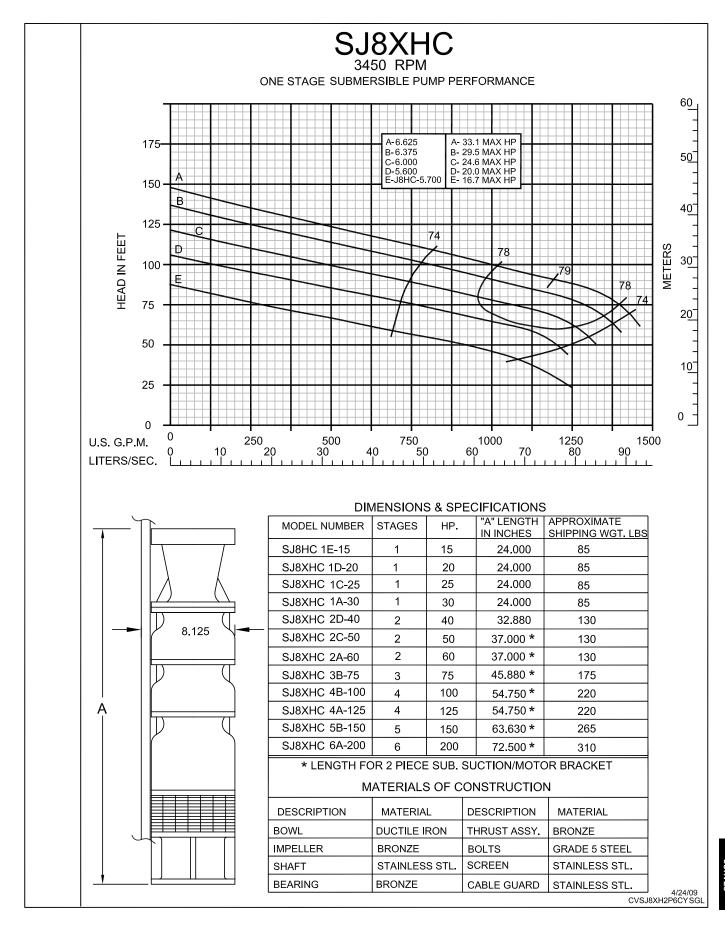
SJ8XHC

3450 RPM

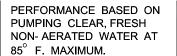


N

SUBMERSIBL CURVES



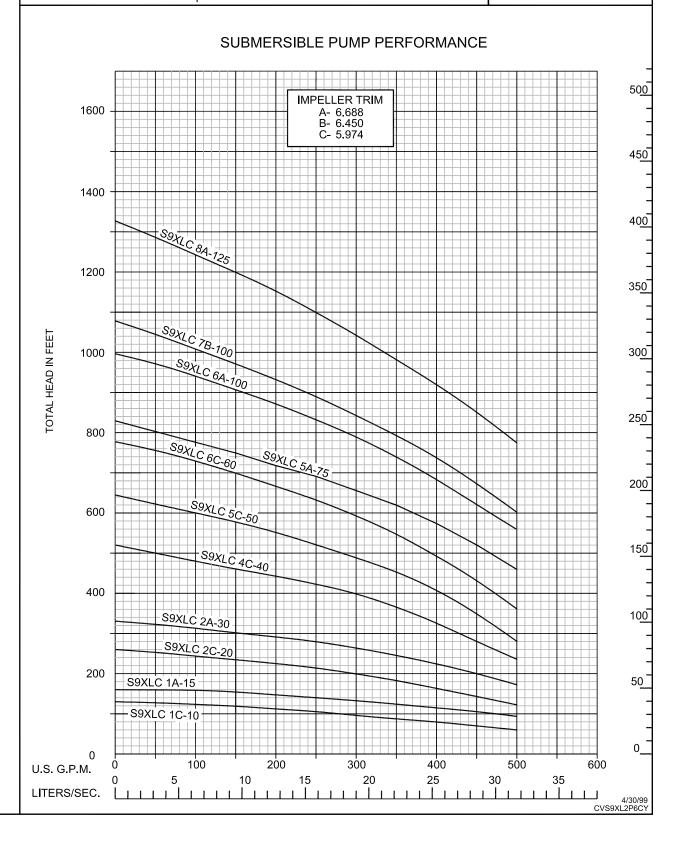




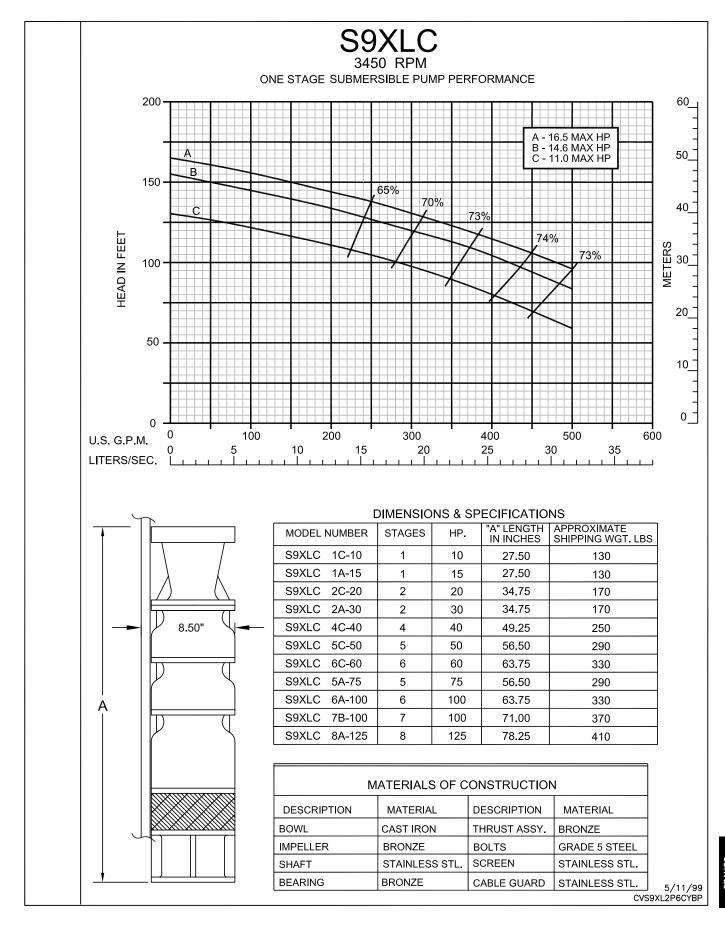




3450 RPM



CURVES

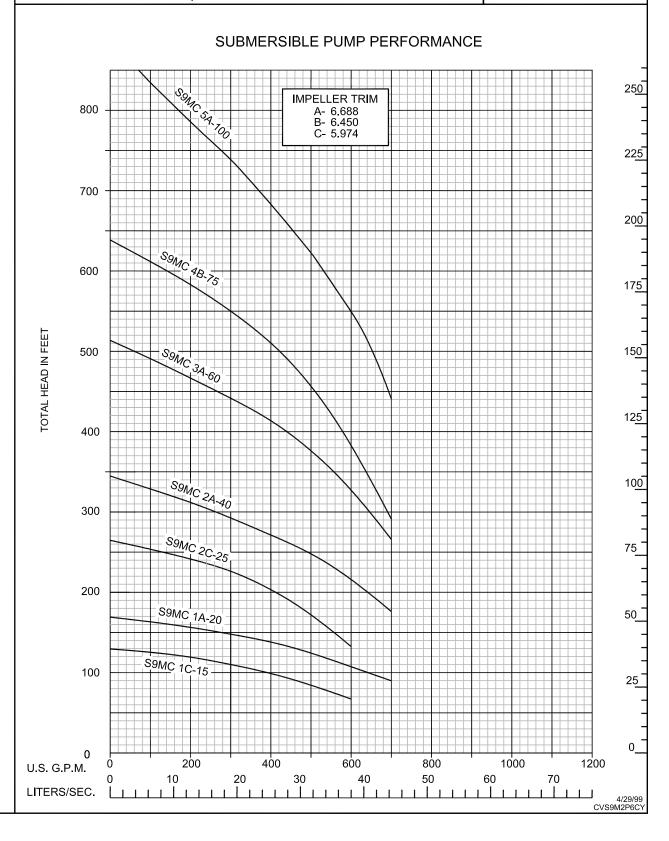


UBMERSIBLE

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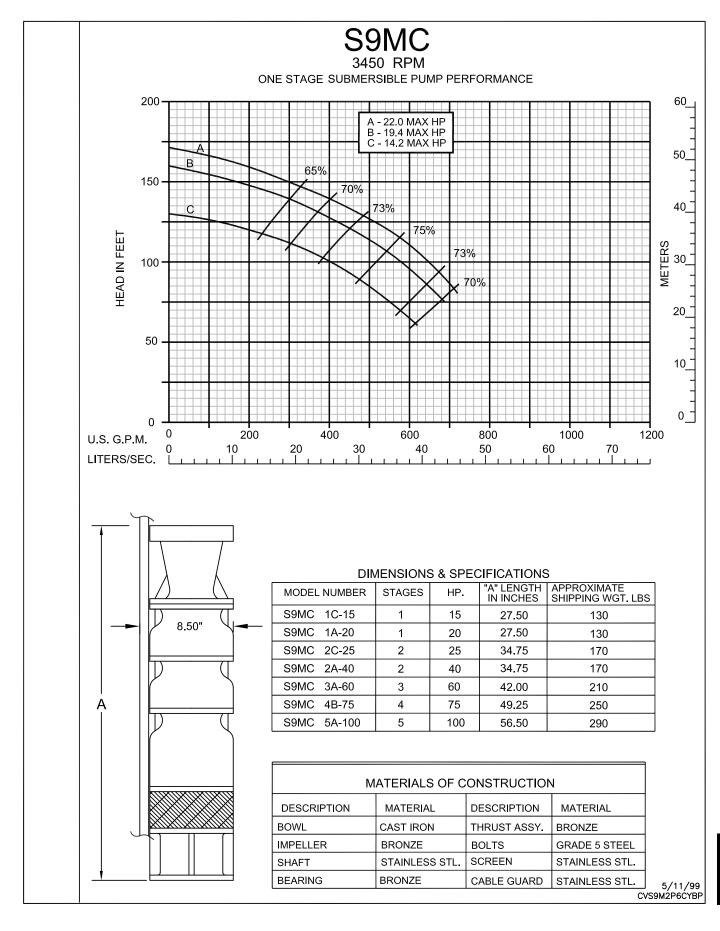






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SUBMERSIBI CURVES

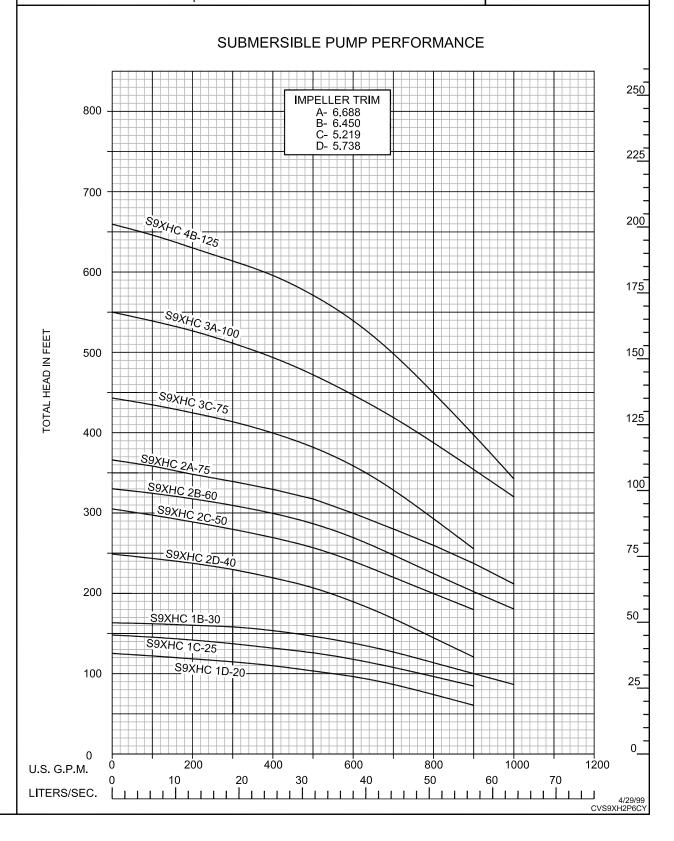


PERFORMANCE BASED ON PUMPING CLEAR, FRESH NON- AERATED WATER AT 85° F. MAXIMUM.



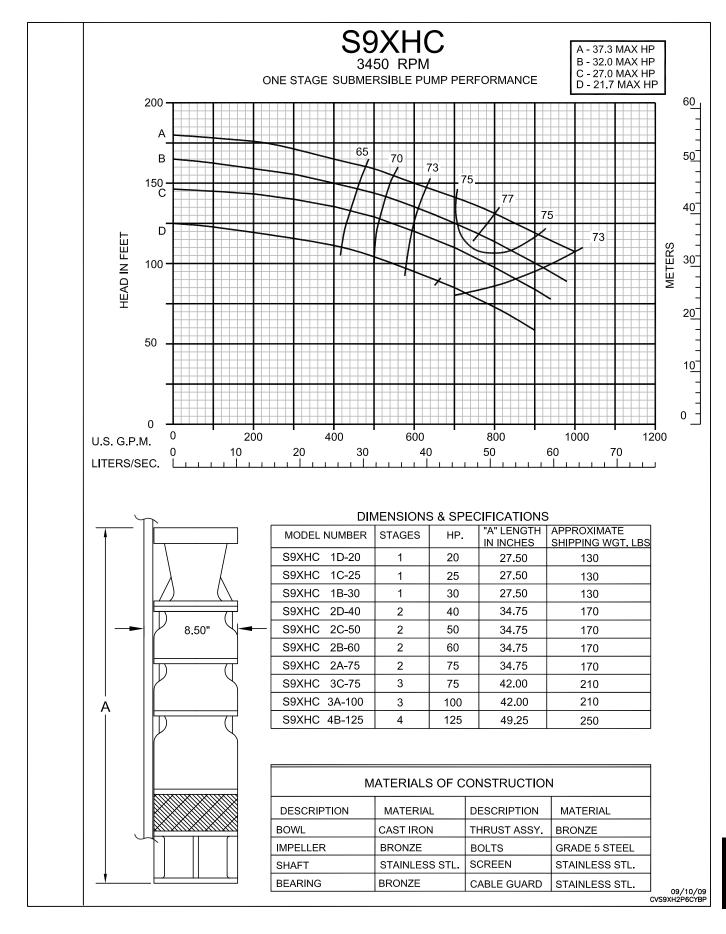
S9XHC

3450 RPM

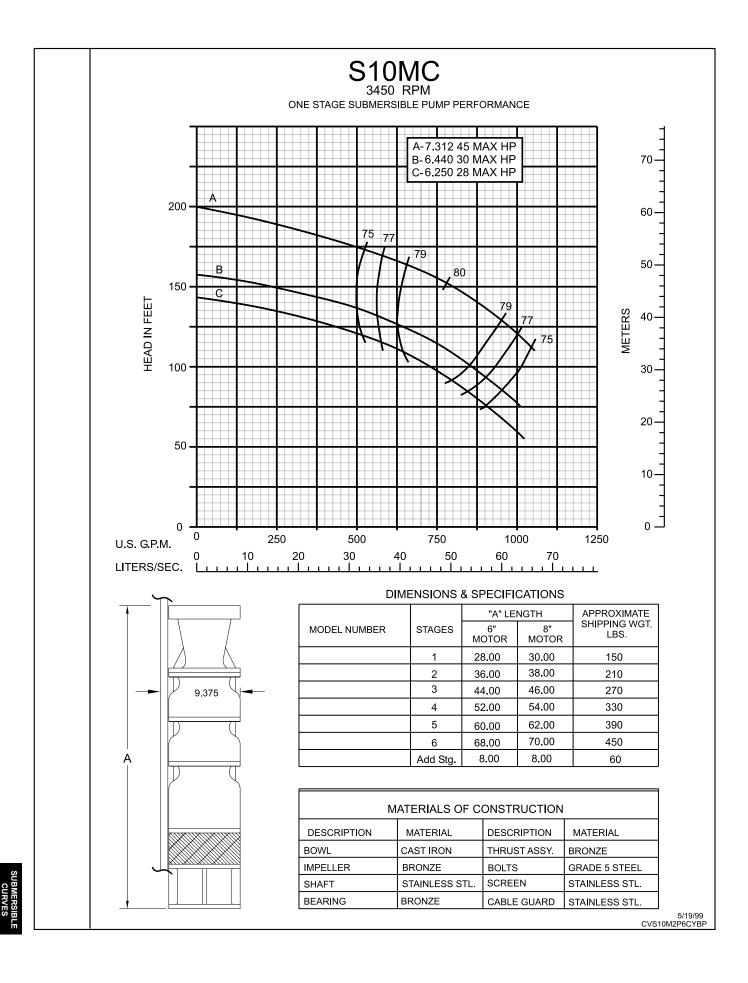


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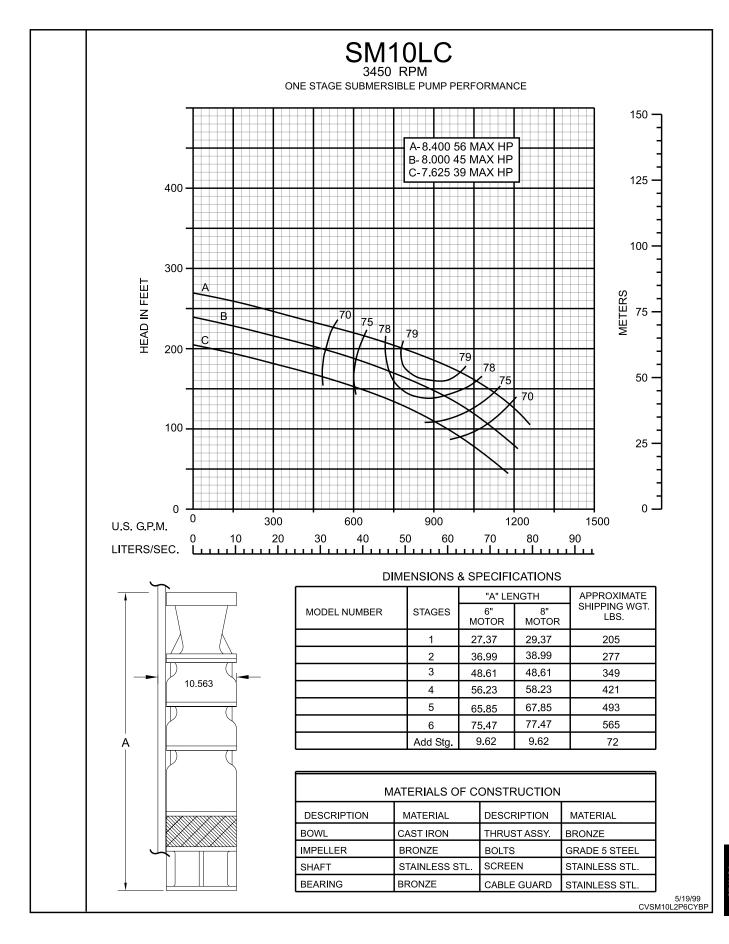
CURVES



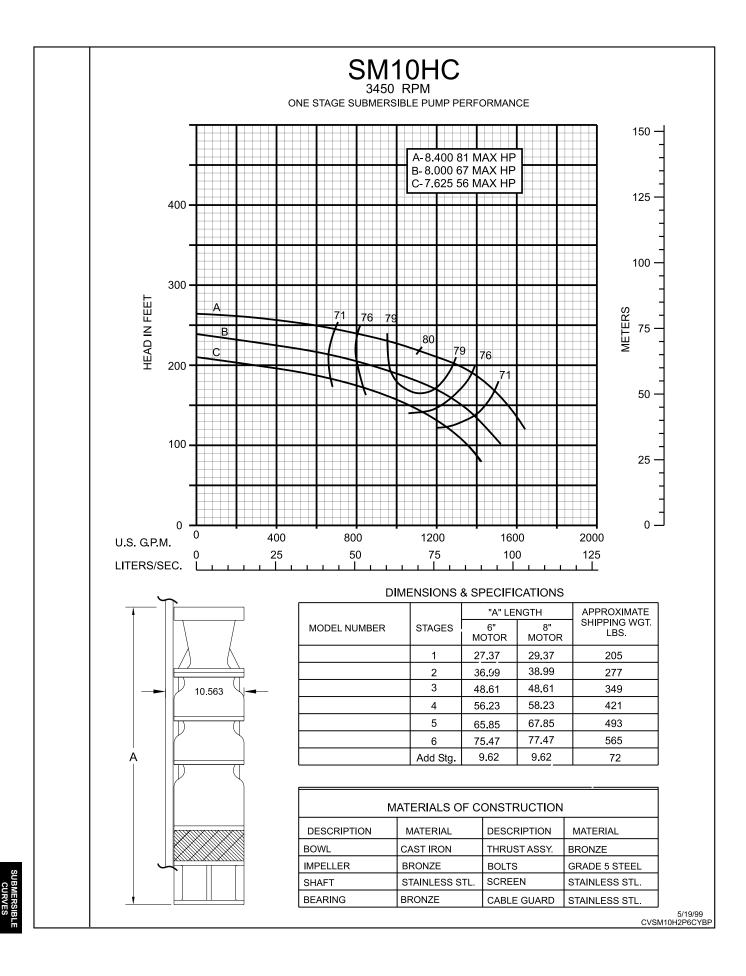
JBMERSIBLE CURVES



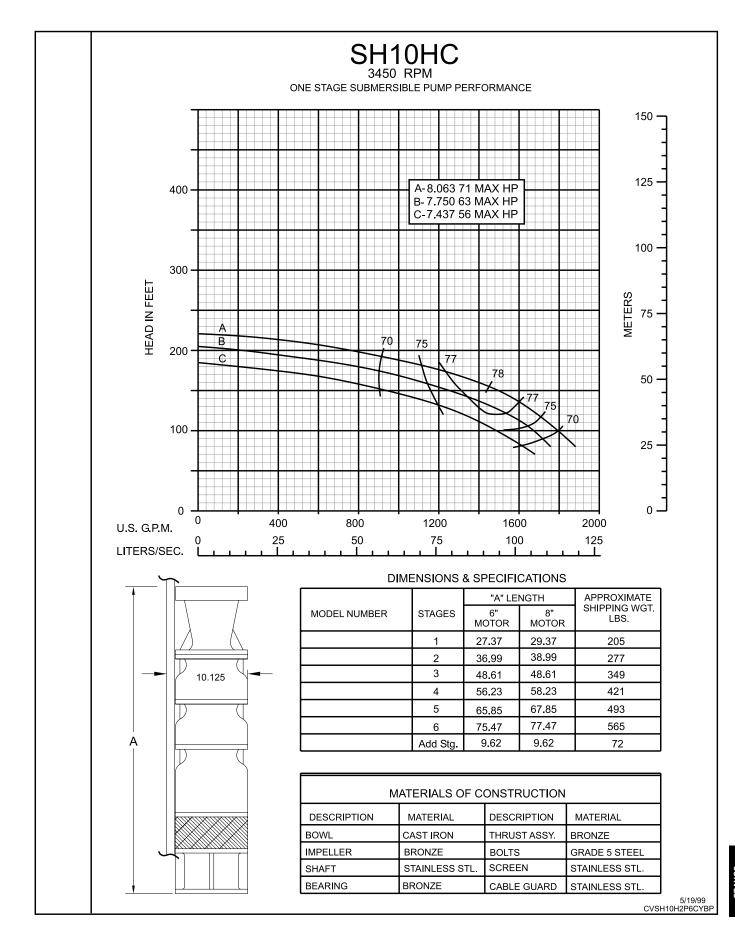








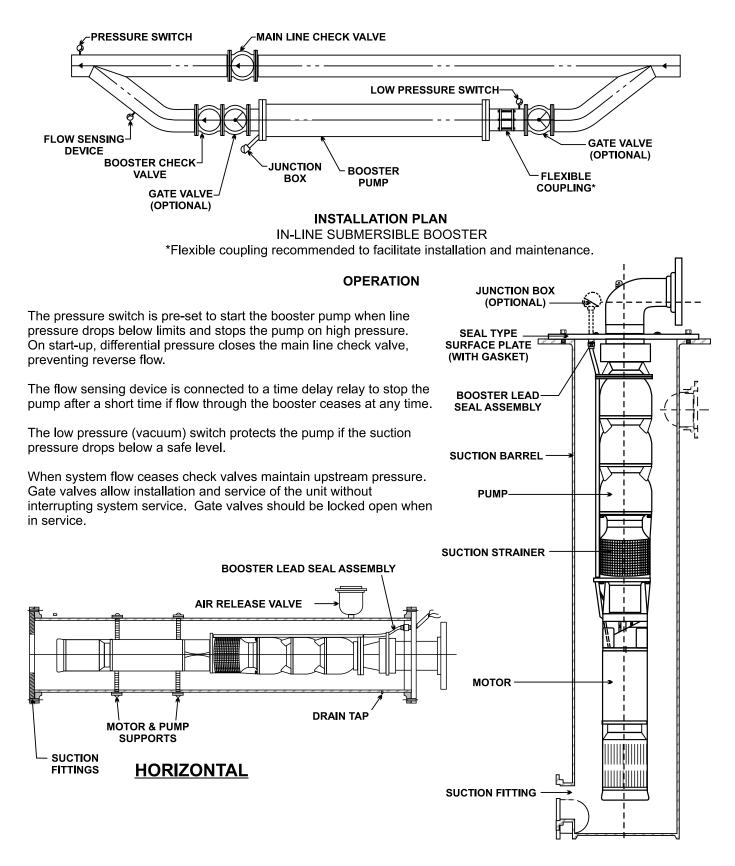






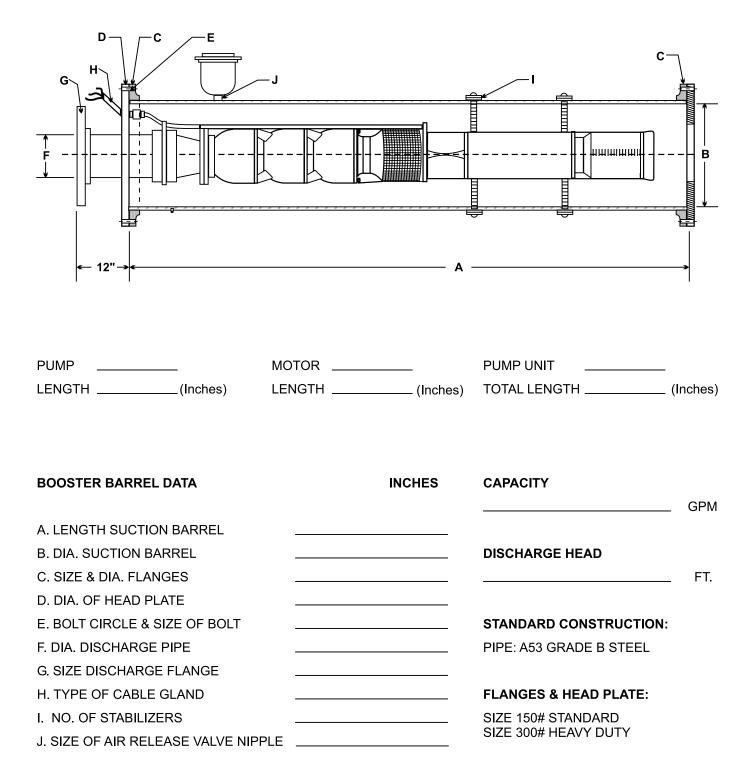


BOOSTER INSTALLATION PLAN, OPERATION & DESIGN





SUB HORIZONTAL BOOSTER ASSEMBLY







SUB VERTICAL BOOSTER ASSEMBLY

PUMP					PUMP UNIT	
LENGTH	Inches	LENGTH	In	ches	LENGTH	Inches
BOOSTER BARRE	EL DATA		INCHES			
A. LENGTH SUCTION	BARREL					
B. DIA. SUCTION BAR	REL			G—	┍═╴R╶┑ ╺╋╏╴╴┇╴	F
C. SIZE & DIA. FLANG	ES			<u> </u>	·	
D. DIA. OF HEAD PLA	TE					<u>у</u> Е
E. BOLT CIRCLE & SIZ	ZE OF BOLT					┶┊╴╺≝ ╴₿╶┟ ╝ ╶╌╴
F. DIA. DISCHARGE P	PIPE			C-7		
G. SIZE DISCHARGE	FLANGE					
H. SIZE SUCTION FLA	ANGE					
J. SIZE OF CABLE JU	NCTION					
K. SIZE OF AIR RELEA	ASE VALVE N	PPLE				
L. CENTER LINE TO F	ACE DIMENS	ION				
M. CENTER LINE TO	BARREL DIME	INSION				
N. CENTER LINE SUC	TION TO BOT	ТОМ		P		
P. DISCHARGE TO SU	JCTION					
R. CENTER LINE TO F	FACE					$\overline{\mathbf{M}}$
CAPACITY			GPM			
DISCHARGE HEAI	D		GPM		• B -	
STANDARD CONS SCHEDULE 40 STE		:	2			
FLANGES & HEAD SIZE 150# STANDA SIZE 300# HEAVY	ARD .			↓ H		
OPTIONS:				N ↓		
TEMPERATURE	PROBE			<u>,</u>	<u> </u>	ut
JUNCTION BOX						



IN-LINE BOOSTER DATA

The complete Booster Barrel Assembly consists of three basic sub assemblies: Barrel Assembly, Head Plate Assembly, and Pumping Unit. The pumping unit is secured to the head plate assembly and is centered in the barrel by means of brackets or stabilizers. Generally, two brackets are necessary and are positioned at top and bottom end of the submersible motor. However, in the case of an installation requiring a long pump end, it may be necessary to have a third bracket positioned around the pump at the halfway mark; i.e., between the pump outlet and the pump inlet. As the number of bowls in a given length differ, depending on the model of pump end use, it is suggested that you consult the factory when considering six (6) stages or over. The support brackets are necessary on both the Horizontal and the Vertical applications. However, on a Vertical Installation, the brackets can be eliminated if the pumping unit is installed in the barrel at the site. The main reason for support brackets in a Vertical Booster would be to support the pumping unit in transit. The dimensions of the Barrel and the Head Plate Assemblies are governed by the size of the Pump Assembly; and, in turn, the Pump Assembly is sized according to GPM and Head (psi) required.

The Pumping Unit installed in a booster barrel will operate satisfactorily if given the same basic care as a proper deep well installation. The following three rules, however, are of extreme importance. Otherwise, the end result will be the overheating of the motor windings without the necessary amperage draw to activate the circuit breakers in the pump control.

- 1. The barrel must be vented of all air on start-up.
- 2. There must be a larger flow (GPM) at the intake than the demand at the pump inlet at all times. This will ensure that the barrel is completely full and the pumping unit is operating under submerged conditions.
- 3. At no time should the pump be permitted to operate against a closed valve condition or against a pressure high enough to approach its closed valve condition as the proper cooling of the motor depends on a constant flow of liquid past its outer casing. The higher the H.P., the larger the flow necessary. The minimum flow for safe operation is generally considered to be one gallon per minute per H.P. of motor.



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SUBMERSIBLE BOOSTER





L COMPANY	321

322



	323

324

REVISED OCTOBER 2022



NATIONAL PUMP COMPANY'S CAPABILITIES

SALES AND SERVICE:

Putting the "customer first" is at the center of everything we do at National Pump. Our experienced sales, marketing, application engineers and branch managers offer many years of pump experience and are prepared to satisfy customer product and service needs. Challenge the National Pump team on your next API, agricultural, industrial and municipal application and discover how we can add value to your business.

PRODUCT & MANUFACTURING:

National Pump Company manufactures a complete line of vertical turbine pumps and pump systems from an extensive inventory located in six (6) USA build centers. Pump capabilities range from 50 through 20,000 GPM. NPC also manufactures and stocks a complete line of VTP accessories, including: column, tube and shaft, standard and custom discharge heads, gear drives and VHS motors, and offers custom pump design, fabrication work, sandblasting and powder coating capabilities.

ENGINEERING & TECHNOLOGY:

National Pump Company's Engineering Department is staffed with extremely experienced engineers and technicians. The team utilizes the latest technology for the design and application of pump products, which includes (CAD) computer aided design, 3D modeling, and realistic engineering programs. This technology and experience ensures that the final product is properly designed for optimum performance.

QUALITY CONTROL:

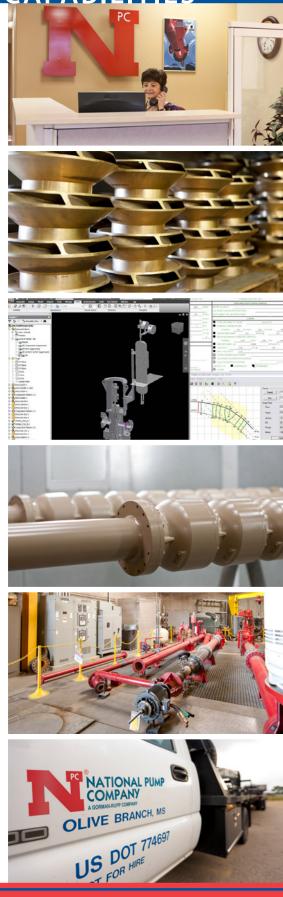
National Pump strives to deliver the highest quality products for complete customer satisfaction through continuous quality improvement initiatives. NPC is ISO 9001 Certified which integrates all facets of the business including: engineering, procurement, assembly, testing, shipping, receiving, and supplier inspections. Every employee at NPC understands they are responsible for the quality objectives of the organization but most importantly to our customers.

TESTING:

NPC offers full HYDRAULIC INSTITUTE certified pump testing, along with UL 508A electrical certification and custom panel building for our complete line of pumps and custom pump stations.

PRODUCT AVAILABILITY AND SUPPLY CHAIN:

National Pump markets it pumps and components in the USA and in over 40 countries globally. We operate six (6) Build and Service Centers in the USA in which we stock and utilize the best quality domestic and international components to insure a quality and reliable pump installation. Our forecasting tools and distribution system maintains thousands of pump parts to help achieve the best customer satisfaction with timely customer deliveries.



MEETING CUSTOMER NEEDS



Delivering Vertical Turbine Pump Reliability, Quality and Service Since 1969

Creating Quality Pump Systems and Satisfied Customers

Visit us on the web at: www.nationalpumpcompany.com

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